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A Parametric Study on Composite G+8 Structure With Application of Damper on Different Locations Using Time History Analysis

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Abstract: The world's population has been growing quite quickly in recent years. Major cities, in particular, have relatively dense populations, which has increased demand for new homes. Because there isn't enough land for new construction in the majority of the old cities, high-rise buildings are moving into mountainous areas. These days, there is more competition to build high rise buildings all over the world as a result of certain developed nations building extremely tall skyscrapers to demonstrate their power and technology to the rest of the world. Buildings on sloping terrain, however, have different structural configurations than those on level terrain, which causes them to vibrate more during earthquake-induced ground motions, resulting in higher displacements and shears. Increased floor displacement results in damage to the structural components, rendering the structure unusable or, in the worst situation, collapsing as a whole. Reducing the amount of seismic energy that enters slanted ground buildings is essential to preventing damage. This can be done by absorbing the majority of the vibrations that an earthquake produces. There are numerous ways to lessen a structure's seismic reaction, including base isolation, shear walls, bracings, dampers, and more. Because of their effectiveness and simplicity of usage, damping devices are particularly well-liked among these methods. The eight-storey building model with four distinct cases—bare frame, bare frame with damper on corners, bare frame with damper on Central Bay, and bare frame with damper on Alternate Bay—is taken into consideration in this research examination. For modeling, use ETABS 2016 Ultimate programme. Utilize time history analysis as well to investigate how earthquake loading affects structures.

Keywords: Fluid Viscous damper, Time history Analysis, Bare Frame, High Rise Building, Vibration Intensities etc.

I. INTRODUCTION

To give dynamic protection to structural systems, vibration control methods in the form of shock and vibration isolators have been designed. Fluid-viscous dampers, for example, have been shown to have desirable performance in controlling shock loads. Fluid viscous dampers are appealing for improving performance since they minimize not only the deformation demand but also the force delivered to the structure as a result of energy dissipation.

Traditional linear fluid-viscous dampers can only dissipate a limited amount of energy and are not as effective for shock loads as nonlinear dampers (Narkhede, D. I., and R. Sinha. 2012)1. For reducing structural resonance, viscous damping is a beneficial energy dissipation technique. A "turbulent viscous damper" (damper) functions by forcing a low-viscosity fluid through microscopic pores, while a "lamellar viscosity unit" (damper) works by forcing a high-viscosity fluid between moving objects. This is accomplished through fluid transfer. Dilution The first is commonly utilized in the manufacture of shock absorbers for car suspensions. "Viscous turbulent dampers" (damper-type dampers) are multidirectional, have a complex mechanical design, and must be maintained on a regular basis, whereas "laminar viscous dampers" (dampers) are multidirectional, have a simple mechanical design, and must be maintained.

A. Application of Damper

Dampers are intelligently positioned in the structure of the building to regulate floor vibrations and building displacement, cater to occupant comfort and mitigate against significant seismic events. The dampers capture the energy produced by building displacement and floor vibration, and then release it as heat energy. Even during an earthquake, the building's inhabitants will suffer less floor vibration, smaller building displacements, and overall better occupancy comfort (Lee, David, and Martin Ng, 2010)16.



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B. Presently Fluid Viscous Damper Applied

The technology was first brought to China on the Chongqing Egongyan Yangtze River Bridge in 2000 and is now widely used in Yangtze River bridges. Viscous dampers have been used in the last 30 years in major civil structures to mitigate the effects of earthquakes.

Their use in high-rise buildings built in seismic areas is a challenge for the designers, since they should reduce the vibrations induced by both strong winds and earthquakes, and the optimal behaviour in these two situations is not usually the same. Consequently, the design requirement for viscous dampers to be used in high-rise buildings is often that they should have two different behaviour in the different range of velocities corresponding to wind and earthquake. Recently Viscous Damper with said behaviour has been applied in three high-rise buildings in Asia, the St. Francis Twin Towers in Manila, the Philippines, and Taipei 101 in Taipei, Taiwan.

C. Types of Fluid Viscous Damper

- 1) Turbulent Flow (Shock Absorber Type) Viscous Damping Devices
- 2) Laminar Flow Viscous Dampers (Dashpots)

D. Time History Analysis

A dynamic analysis technique is code time history analysis. It could be linear or not. This is a step-by-step investigation of the dynamic response of a structure to particular time-varying stresses (Patsialis et.al, 2022)1. Direct integration techniques or fast nonlinear (FNA) techniques can be used for this. The motion equations are integrated over a period of time using the direct integration method. A modal analysis technique is FNA.

E. Non-Linear Time History Analysis

The bridge is analyzed for actual ground vibrations in non-linear analysis. In this analysis, non-linarites in the member will be specifically described. Using this technique, it is possible to determine whether the structure's strength is sufficient to handle the anticipated inelastic deformation. The sub-structure has been subjected to a non-linear analysis using three time histories that are MCE-compliant.

II. PROBLEM STATEMENT

- 1) To get knowledge about effect of composite structure with application of damper on different locations using time history analysis consider as research problem.
- 2) A lot of work done with dampers but analysis of damper with time history not done yet. Also provide the most appropriate site damper in model based on the current conditions by comparing various seismic characteristics.
- *3)* Composite structure system which optimizes economy, serviceability, construction time and seismic performance may be considered as optimum structural system. Study dampers characteristics through the analysis of nine storey building.
- 4) Generally to achieve the objectives of constructions in economical way, composite structure design and construction technology plays enormous role.
- 5) Developing countries has to give especial attention to get its benefit. Specifically, the India is one of the developing countries, and its economy is developing rapidly. Thus, this construction technology contributes a lot in the current context of the country to answer the demand of economical designs.

III. OBJECTIVES

- 1) Due to the load combination of the dead load and seismic load, storey drift, drift ratio, and shear forces occur to limit joint displacement.
- 2) To study the damper & time history analysis using software.
- 3) Prepared different composite building models for different zone V and IV.
- 4) Compare the model parameters and discusses result like joint displacement, storey drift, drift ratio, shear force and bending moment.
- 5) To compare bracing's impact on composite structures.



IV. METHODOLOGY

In this section we study on 8 storey building model with four different cases like model with bare frame, bare frame with damper on corners, bare frame with damper on Central bay and bare frame with damper on Alternate Bay. We use ETABS 2016 Ultimate software for modeling.

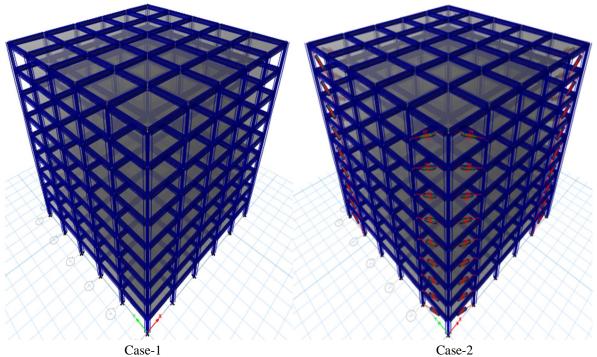
A. Model Geometry

Table 1	Specification	of G+8	building	Model
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Sr No.	Cases Description						
		-					
1	Case-1	G+8 Building model with bare frame					
2	Case-2	G+8 Building model with damper on Corner					
3	Case-3	+8 Building model with damper on Centre					
4	Case-4	G+8 Building model with damper on alternate bay					
Sr. No.	Building structure	Remark					
1	Height of building	27m					
2	No. of floors	9					
3	Floor height	3m					
4	Column	500x 500mm					
5	Beam	500x300mm					
6	Slab thickness	200mm					
Materials							
1	Grade of Concrete	M30					
2	Steel bars	HYSD500					
		Fe345					
3	Damper	Fluid Viscous damper (FVD)					
Loadings							
1	Seismic Zone	IS 1893:2002 (Zone-V)					
2	Time History	ASCE7-22					



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 Cas-3
 Cas-4

Figure 1 3D view models in different cases



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TAYLOR DEVICES MODEL NUMBER	SPHERICAL BEARING BORE DIAMETER (mm)	MID- STROKE LENGTH (mm)	STROKE (mm)	CLEVIS THICKNESS (mm)	MAXIMUM CLEVIS WIDTH (mm)	CLEVIS DEPTH (mm)	BEARING THICKNESS (mm)	MAXIMUM CYLINDER DIAMETER (mm)	WEIGHT (kg)
17120	38.10	787	±75	43	100	83	33	114	44
17130	50.80	997	±100	55	127	102	44	150	98
17140	57.15	1016	±100	59	155	129	50	184	168
17150	69.85	1048	±100	71	185	150	61	210	254
17160	76.20	1105	±100	77	205	162	67	241	306
17170	88.90	1346	±125	91	230	191	78	286	500
17180	101.60	1441	±125	117	290	203	89	350	800
17190	127.00	1645	±125	142	325	273	111	425	1088
17200	152.40	1752	±125	154	350	305	121	515	1930
17210	177.80	1867	±125	178	415	317	135	565	2625
	DEVICES MODEL NUMBER 17120 17130 17140 17150 17160 17160 17180 17190 17200	TAYLOR DEVICES MODEL NUMBER BEARING BORE DIAMETER (mm) 17120 38.10 17130 50.80 17140 57.15 17150 69.85 17160 76.20 17170 88.90 17180 101.60 171200 152.40	TAYLOR DEVICES MODEL NUMBER BEARING BORE DIAMETER (mm) MID- STROKE LENGTH (mm) 17120 38.10 787 17130 50.80 997 17140 57.15 1016 17150 69.85 1048 17160 76.20 1105 17170 88.90 1346 17180 101.60 1441 17190 127.00 1645 17200 152.40 1752	TAYLOR DEVICES MODEL NUMBER BEARING BORE DIAMETER (mm) MID- STROKE LENGTH (mm) STROKE (mm) 17120 38.10 787 ±75 17130 50.80 997 ±100 17140 57.15 1016 ±100 17150 69.85 1048 ±100 17160 76.20 1105 ±100 17170 88.90 1346 ±125 17180 101.60 1441 ±125 17200 152.40 1752 ±125	TAYLOR DEVICES NODEL NUMBER BEARING BORE DAMETER (mm) MID- STROKE LENGTH (mm) STROKE (mm) CLEVIS THICKNESS (mm) 17120 38.10 787 ±75 43 17130 50.80 997 ±100 55 17140 57.15 1016 ±100 59 17150 69.85 1048 ±100 71 17160 76.20 1105 ±100 77 17170 88.90 1346 ±125 91 17180 101.60 1441 ±125 117 17200 152.40 1752 ±125 154	TAYLOR DEVICES MODEL NUMBER BEARING BORE DIAMETER (mm) MID- STROKE LENGTH (mm) STROKE (mm) CLEVIS THICKNESS MAXIMUM CLEVIS WIDTH (mm) 17120 38.10 787 ±75 43 100 17130 50.80 997 ±100 55 127 17140 57.15 1016 ±100 59 155 17150 69.85 1048 ±100 71 185 17160 76.20 1105 ±100 77 205 17170 88.90 1346 ±125 91 230 17180 101.60 1441 ±125 117 290 17190 127.00 1645 ±125 142 325 17200 152.40 1752 ±125 154 350	TAYLOR DEVICES MODEL NUMBER BEARING BORE DIAMETER (mm) MID- STROKE LENGTH (mm) STROKE (mm) CLEVIS THICKNESS (mm) MAXIMUM CLEVIS WIDTH (mm) CLEVIS DEPTH (mm) 17120 38.10 787 ±75 43 100 83 17130 50.80 997 ±100 55 127 102 17140 57.15 1016 ±100 59 155 129 17160 69.85 1048 ±100 71 185 150 17160 76.20 1105 ±100 777 205 162 17170 88.90 1346 ±125 91 230 191 17180 101.60 1441 ±125 117 290 203 17190 127.00 1645 ±125 142 325 273 17200 152.40 1752 ±125 154 350 305	TAYLOR DEVICES MODEL NUMBER BEARING BORE DIAMETER (mm) MID- STROKE LENGTH (mm) STROKE (mm) CLEVIS THICKNESS MAXIMUM CLEVIS WIDTH (mm) CLEVIS DEPTH (mm) BEARING DEPTH (mm) BEARING THICKNESS (mm) 17120 38.10 787 ±75 43 100 83 33 17130 50.80 997 ±100 55 127 102 44 17140 57.15 1016 ±100 59 155 129 50 17150 69.85 1048 ±100 71 185 150 61 17160 76.20 1105 ±100 77 205 162 67 17170 88.90 1346 ±125 91 230 191 78 17180 101.60 1441 ±125 117 290 203 89 17190 127.00 1645 ±125 142 325 273 1111 17200 152.40 1752 ±125 154 350	TAYLOR DEVICES NODEL NUMBER BEARING BORE DIAMETER (mm) MID- STROKE LENGTH (mm) STROKE (mm) STROKE (mm) CLEVIS THICKNESS MAXIMUM CLEVIS WIDTH (mm) CLEVIS DEPTH (mm) BEARING THICKNESS (mm) MAXIMUM CYLINDER DIAMETER (mm) 17120 38.10 787 ±75 43 100 83 33 114 17130 50.80 997 ±100 55 127 102 44 150 17140 57.15 1016 ±100 59 155 129 500 184 17160 69.85 1048 ±100 77 205 162 67 241 17170 88.90 1346 ±125 91 230 191 78 286 17180 101.60 1441 ±125 117 290 203 89 350 17190 127.00 1645 ±125 142 350 305 121 515

Table 2 FVD with different Capacities Forces (kN)

V. RESULTS AND DISCUSSION

A. Results of Joint Displacement (mm)

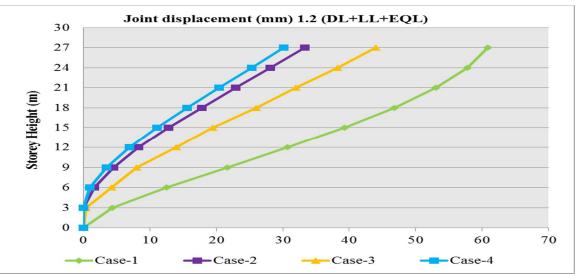


Figure 2 Joint displacement in G+8 storey structure different cases cause from load combination 1.2 (DL+LL+EQL)

B. Results of Storey Drift

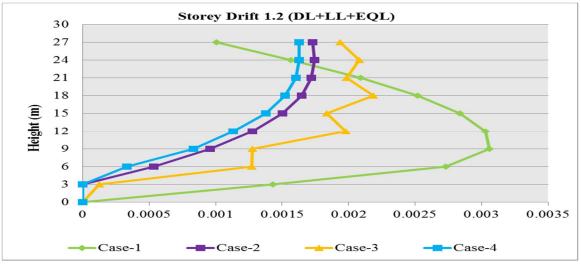


Figure 3 Storey Drift in G+8 storey structure different cases cause from load combination 1.2 (DL+LL+EQL)



C. Results of Stiffness (kN/m)

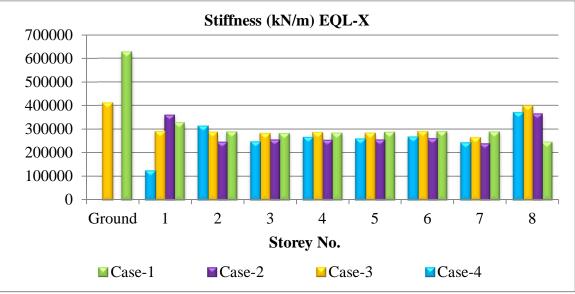
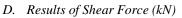


Figure 4 Stiffness of G+8 storey structure different cases cause from earthquake load



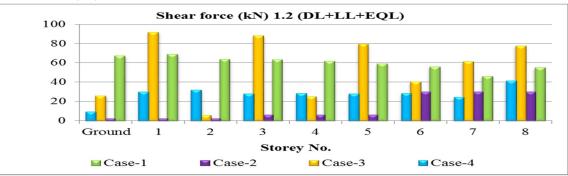
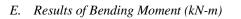


Figure 5 Shear Force on G+8 storey structure different cases cause from load combination 1.2 (DL+LL+EQL)



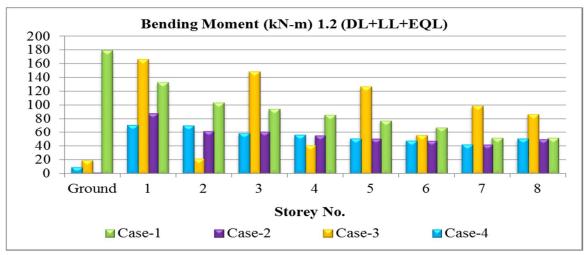


Figure 6 Bending Moment of G+8 storey structure different cases cause from load combination 1.2 (DL+LL+EQL)



F. Base Reaction (kN)

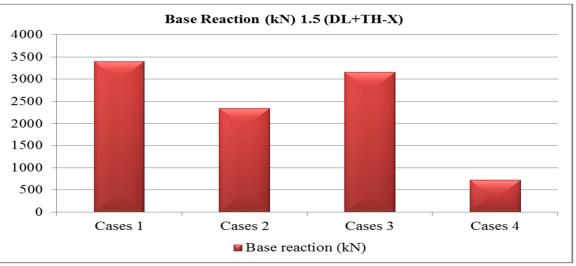


Figure 8 Base Reaction in G+8 storey structure different cases cause from load combination 1.5 (DL+TH-X)

VI. CONCLUSION

- In the bare frame value of joint displacement was 60.83mm at top floor. When damper applied on corner this joint displacement was 33.35mm decreased. Location of damper was at centre then joint displacement was 44.04mm. And finally location of damper placed at alternate bays then joint displacement was 30.18mm.
- 2) It is noticed that maximum change in joint displacement happen in case-4 when dampers were placed at alternate bays and minimum reduction happen in case-3 when damper were placed at centre.
- *3)* In the bare frame value of storey drift was 0.001009 at top floor. When damper applied on corner this storey drift was 0.00173 increased. Location of damper was at centre then storey drift was 0.001935. And finally location of damper placed at alternate bays then storey drift was 0.001626.
- *4)* It is noticed that maximum change in storey drift happen in case-3 when dampers were placed at centre and minimum reduction happen in case-4 when damper were placed at alternate bay.
- 5) In the bare frame value of stiffness was 243861.96kN/m at top floor. When damper applied on corner this stiffness was 362349.59kN/m increased. Location of damper was at centre then bending moment was 397611.43kN/m. And finally location of damper placed at alternate bays then stiffness was 367889.78kN/m.
- 6) It is noticed that maximum change in stiffness happen in case-3 when dampers were placed at centre and minimum reduction happen in case-2 when damper were placed at centre.
- 7) In the bare frame value of shear force was 54.441kN at top floor. When damper applied on corner this shear force was 29.3043kN decreased. Location of damper was at centre then shear force was 76.926kN. And finally location of damper placed at alternate bays then shear force was 40.538kN.
- 8) It is noticed that maximum change in shear force happen in case-3 when dampers were placed at centre and minimum reduction happen in case-4 when damper were placed at alternate bay.
- 9) In the bare frame value of bending moment was 50.77kN-m at top floor. When damper applied on corner this bending moment was 49.05kN-m decreased. Location of damper was at centre then bending moment was 85.98kN-m. And finally location of damper placed at alternate bays then bending moment was 49.75kN-m.
- 10) It is noticed that maximum change in bending moment happen in case-3 when dampers were placed at centre and minimum reduction happen in case-4 when damper were placed at alternate bay.
- 11) In the bare frame value of base reaction was 3400.9667kN. When damper applied on corner this bending moment was 2340.9323decreased. Location of damper was at centre then bending moment was 3161.7707kN. And finally location of damper placed at alternate bays then bending moment was 716.8096kN.
- 12) It is noticed that maximum change in bending moment happen in case-3 when dampers were placed at centre and minimum reduction happen in case-4 when damper were placed at alternate bay.

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