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Comparative Analysis of Annular Raft and Solid Raft

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Abstract: The goal of the study is annular mat foundation in various modern structures: Circular tower-shaped structures, like, microwave towers, TV tower, cooling towers, overhead water tanks, etc For this purpose, three raft cases are considered, which are mentioned below.

- (1) Intze overhead tank Annular raft with net SBC 24Kn/m2
- (2)Intze overhead tank Circular Solid raft

This study aims to evaluate these foundation systems' structural behavior and performance aft's outer radius is also taken as a variable for obtaining different results in our thesis work. An F.E.M.-based analysis is done to determine critical moments and deflections in both annular and circular rafts. Comparison of this base pressure critical moments, shear force, bending stress, and deflections are made based on the above-mentioned case, including the cost comparison foundation. The concrete grade is M-30, and HYSD FE 500 steel reinforcement is used in design calculation. The load combination is followed as IS 1893-2016 and IS 456-2000—seismic zone 3. The software package staad pro v8i and connect edition is used. To provide relevant calculations, Microsoft Excel is used.

Keywords: Staad pro v8i, FEM, Solid Raft, SBC

I. INTRODUCTION

The foundation is a mediator to effectively transfer the load from the superstructure to the soil, without any failure for both the structure and the soil. Annular Mat foundation is one of the effective types of shallow foundations, which carries the load to the soil without any differential settlement in the soil. Annular foundation may be used where the base soil has a low bearing capacity and/or the column loads are so large that more than 50 percent of the area is covered by conventional spread footings.

In the present era, factors like rapid urbanization and massive developments taking place at one place or the other have also given rise to instances of failure of the structures, which in turn, sometimes lead to colossal destruction and loss of lives. For this reason, the study of the bearing capacity of soil has attained paramount significance. On one hand, overestimation of the bearing capacity results in structures potentially prone to disastrous collapse, while its underestimation can make the foundation uneconomic.

There are various theories for the design of the Annular foundation. Those vary from conventional manual calculation methods to most modern computer-based methods. The finite element method is one of the effective and economical numerical methods for analyzing these foundations. For the Annular Mat foundation, advanced numerical modeling techniques are utilized by dividing the MAT into grid elements and predicting the behavior of the structure under loading for critical elements projects.

II. TYPE FOUNDATION

Following are the different types of Foundation.

- 1. Shallow Foundation
- Isolated footing
- Combined Footing
- Strip Foundation
- Raft Foundation

2. Deep Foundations

Pile Foundation

III. ANNULAR AND SOLID RAFT

The raft foundation is generally recommended in underground structure, or when the footing area exceeds 50% of the building than raft foundation is provided.

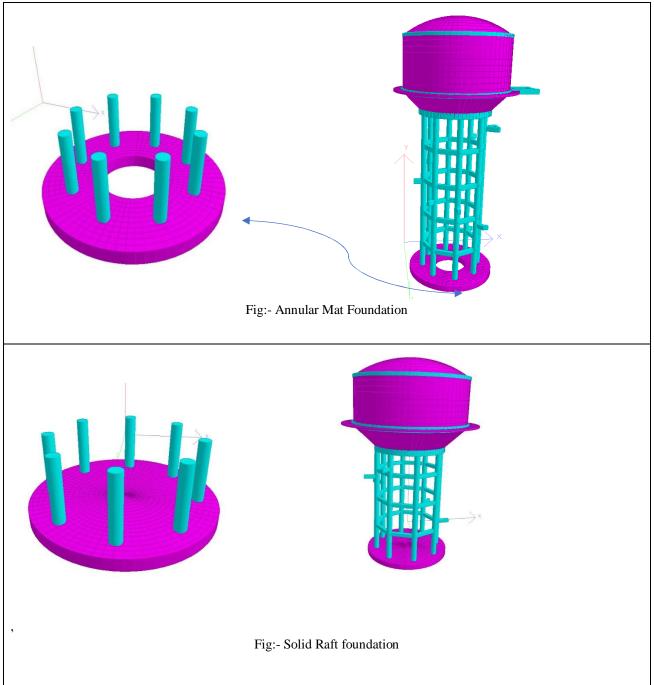
The Annular or raft foundation also supports the control the differential settlement.





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Annular raft foundation in various modern structures: Circular tower-shaped structures, like TV towers, microwave towers, chimneys, cooling towers, overhead water tanks, etc.



IV. NECESSARY INFORMATION REQUIRED FOR DESIGN A FOUNDATION

For satisfactory design and construction of the annular foundation, the following information a neighbouring structure.

- 1) Site plan- a site plan showing the location of the proposed as well neighboring structures.
- 2) Building plan- showing the detail of height, staging column, etc.
- 3) Loading condition- dead load, wind or earthquake loads, shown on the schematic plan indicating the design combination of the load transmitted to the foundation.





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- 4) Environmental factor information relating to the geologic history of the area, seismicity of the region, hydrological, information indicating groundwater condition and its seasonal variation, climatic factor like the vulnerability of the site to sudden flooding by surface runoff, erosion, etc.
- 5) Geotechnical information subsurface profile with stratification details engineering properties of the founding, strata, index properties, effective shear parameters determined under appropriate drainage conditions, compressibility characteristics, swelling properties, results of field tests like static and dynamic penetration tests, pressure meter tests, etc.
- 6) Modulus of elasticity and modulus of subgrade reaction.
- 7) Limiting values of the angular distortion and differential settlement, the superstructure can withstand.

TABLE 01 – Properties of Annular Raft and solid Raft Foundation

Annular Raft									
Inner	Inner outer								
Dia	Dia	Thickness	Sbc	Conc.Grade	Steel				
3200	8700	600	240kn/m2	M-25	Fe-500				

	Solid Raft								
Inner	outer								
Dia	Dia	Thickness	Sbc	Conc.Grade	Steel				
-	8700	600	240kn/m2	M-25	Fe-500				
Density of	of Water (γw	<u>/) = </u>	10	kN/m3					
Elastic M	Iodulus of S	teel (Es) =	200000	N/mm2					
For calcu	ılations relat	ed to							
Strength	Calculations	s (IS:456)							
Per. Stres	ss in Concre	te							
	Bending, (σcl	oc) =	10	N/mm2					
	ss in Steel								
	irect tension		130	N/mm2					
1011.5010.	Per. Stress in Concrete								
	due to Direct tension (σ cc) =			N/mm2					
	For calculations related to								
	resistance to cracking (IS:3370)								
	ss in Concre		1.5	N/ O					
	irect tension	` '	1.5	N/mm2					
	ss in Concre	te	2	N/mm2					
	sending = Modulus of		2	IN/IIIIIZ					
	, Tank (Ec)		27386.1279	N/mm2					
Elastic M			27300.1277	14/IIIII2					
2140011	of Concrete, Staging (Ec) =		25000	N/mm2					
Modular	Modular Ratio (m) =		9.33333333						
Earthqua	ke Zone =		III						
Soil type	=		Hard	Soil					
Wind Sp	eed =		50	m/sec					

V. METHODOLOGY

The finite element analysis carried out staad pro connect edition, of solid and annular raft foundation, The sub grade modulus value is considering differential settlement 50mm.





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The comparative analysis of both case has been carried out. The different case study is carried it has been observed that if annular beam is provided the shear force and bending can be reduced. The oneway shear force is calculated at D distance. The punching shear force is calculated at D/2 distance. If the sbc is increased the raft inner /outer projection forces are reduced. Thus, the section can be economized.

To reach a certain conclusion, one of the variables should be taken as unknown, and the rest of the others should be made constant; therefore, in our research work, Dia of the raft and sbc variable. Other boundary conditions such as backfill soil characteristics, Grade of concrete and reinforcement, and designing methodology (Limit state method as per IS 456:2000) were kept constant during analysis and design work.

VI. RESULT

Load Combination

The structure shall be analysed for the following load combination and each structure element (wall, beam, column,etc.) shall be designed for the load combination producing most unfavourable effect on it.

- DL + LL
- DL + WL(+X)
- DL + WL(-X)
- DL + WL(+Z)
- DL + WL(-Z)
- DL + EQ(+X)
- DL + EQ(-X)
- DL + EQ(+Z)
- DL + EQ(-Z)
- DL + LL + WL(+X)
- DL + LL + WL(-X)
- DL + LL + WL(+Z)
- DL + LL + WL(-Z)
- DL + LL + EQ(+X)
 DL + LL + EQ(-X)
- DL + LL + EQ(+Z)
- DL + LL + EQ(-Z)A

Limit State	of Servivea			
LC	DL	WL	EQ	
1	1.0	1.0	-	-
2	1.0		1.0	-
3	1.0	-		1.0
4	1.0	1.0	1.0	-
5	1.0	1.0	-	1.0

Limit State of Collapse:

LC	DL	LL	WL	EQ
6	1.5	1.5	-	-
7	1.5	-	1.5	-
8	1.5	-	-	1.5
9	1.2	1.2	1.2	-
10	1.2	1.2	-	1.2
11	0.9	-	1.5	-
12	0.9	-	-	1.5

Note:

DL Dead Load

LL Live Load

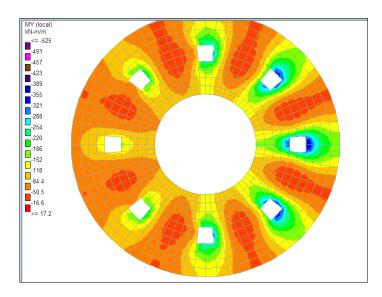


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VII. RESULTS AND COMPARISON

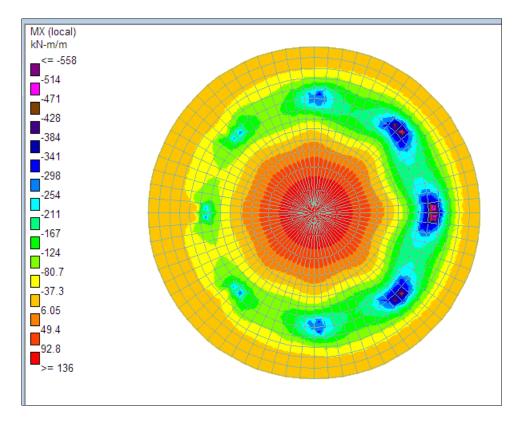
Annular Raft shear force and bending moment as per Staad result

			Sh	ear		Membrane		Bending Mom		ment	
	Plate	L/C	SQX (local)	SQY (local)	SX (local)	SY (local)	SXY (local)	Mx	Му	Mxy	
	1 1010	2.0	kN/m2	kN/m2	kN/m2	kN/m2	kN/m2	kN-m/m	kN-m/m	kN-m/m	
Max Qx	4431	102 TANK_FULL_ULS_1.5DL+1.5WRL+1.5WDL (+) X	1528.888	-251.597	0.000	0.000	0.000	-236.906	-331.664	-15.314	
Min Qx	3718	102 TANK_FULL_ULS_1.5DL+1.5WRL+1.5WDL (+) X	-924.949	38.142	0.000	0.000	0.000	-119.308	-295.151	-40.522	
Max Qy	3820	105 TANK_FULL_ULS_1.5DL+1.5WRL+1.5WDL (-) Z	274.389	1324.142	0.000	0.000	0.000	-279.346	-226.625	-2.003	
Min Qy	3790	102 TANK_FULL_ULS_1.5DL+1.5WRL+1.5WDL (+) X	388.543	-1287.138	0.000	0.000	0.000	-280.413	-225.186	1.724	
Max Sx	4434	101 TANK_FULL_ULS_1.5DL+1.5HT+1.5LL	89.688	-30.295	0.000	0.000	0.000	-0.514	-145.731	3.855	
Min Sx	4434	101 TANK_FULL_ULS_1.5DL+1.5HT+1.5LL	89.688	-30.295	0.000	0.000	0.000	-0.514	-145.731	3.855	
Max Sy	4434	101 TANK_FULL_ULS_1.5DL+1.5HT+1.5LL	89.688	-30.295	0.000	0.000	0.000	-0.514	-145.731	3.855	
Min Sy	4434	101 TANK_FULL_ULS_1.5DL+1.5HT+1.5LL	89.688	-30.295	0.000	0.000	0.000	-0.514	-145.731	3.855	
Max Sx	4434	101 TANK_FULL_ULS_1.5DL+1.5HT+1.5LL	89.688	-30.295	0.000	0.000	0.000	-0.514	-145.731	3.855	
Min Sxy	4434	101 TANK_FULL_ULS_1.5DL+1.5HT+1.5LL	89.688	-30.295	0.000	0.000	0.000	-0.514	-145.731	3.855	
Max Mx	4071	135 TANK_EMPTY_ULS_0.9DL+1.5WDL (+) X	-322.415	76.782	0.000	0.000	0.000	66.015	23.405	-0.589	
Min Mx	4419	102 TANK_FULL_ULS_1.5DL+1.5WRL+1.5WDL (+) X	-231.237	-1179.054	0.000	0.000	0.000	-336.201	-167.019	42.830	
Max My	4000	135 TANK_EMPTY_ULS_0.9DL+1.5WDL (+) X	-32.953	-227.575	0.000	0.000	0.000	16.380	34.286	25.760	
Min My	4431	102 TANK_FULL_ULS_1.5DL+1.5WRL+1.5WDL (+) X	1528.888	-251.597	0.000	0.000	0.000	-236.906	-331.664	-15.314	
Max Mx	3878	105 TANK_FULL_ULS_1.5DL+1.5WRL+1.5WDL (-) Z	-573.270	-521.499	0.000	0.000	0.000	-168.003	-141.337	95.727	
Min Mxy	4268	104 TANK_FULL_ULS_1.5DL+1.5WRL+1.5WDL (+) Z	-613.821	468.305	0.000	0.000	0.000	-149.172	-158.095	-96.778	
IIIII IIIAY	4200	104 TARRET DEE_DES_1.50E+1.5WRE+1.5WBE (1) Z	-010.021	400.000	0.000	0.000	0.000	-140.172	-100.000	-50.1	



			Sh	Shear		Membrane			Bending Moment		
	Plate	L/C	SQX (local) kN/m2	SQY (local) kN/m2	SX (local) kN/m2	SY (local) kN/m2	SXY (local) kN/m2	Mx kN-m/m	My kN-m/m	Mxy kN-m/m	
Max Qx	4431	102 TANK_FULL_ULS_1.5DL+1.5WRL+1.5WDL (+) X	1412.011	-226.831	0.000	0.000	0.000	-228.233	-242.114	-21.671	
Min Qx	3718	102 TANK_FULL_ULS_1.5DL+1.5WRL+1.5WDL (+) X	-1126.439	54.741	0.000	0.000	0.000	-149.576	-172.183	-43.895	
Max Qy	3820	105 TANK_FULL_ULS_1.5DL+1.5WRL+1.5WDL (-) Z	246.878	1302.889	0.000	0.000	0.000	-293.261	-131.103	-1.835	
Min Qy	3789	102 TANK_FULL_ULS_1.5DL+1.5WRL+1.5WDL (+) X	-306.684	-1279.846	0.000	0.000	0.000	-324.768	-102.252	34.675	
Max Sx	4724	101 TANK_FULL_ULS_1.5DL+1.5HT+1.5LL	-73.572	-5.116	0.000	0.000	0.000	146.184	144.949	0.443	
Min Sx	4724	101 TANK_FULL_ULS_1.5DL+1.5HT+1.5LL	-73.572	-5.116	0.000	0.000	0.000	146.184	144.949	0.443	
Max Sy	4724	101 TANK_FULL_ULS_1.5DL+1.5HT+1.5LL	-73.572	-5.116	0.000	0.000	0.000	146.184	144.949	0.443	
Min Sy	4724	101 TANK_FULL_ULS_1.5DL+1.5HT+1.5LL	-73.572	-5.116	0.000	0.000	0.000	146.184	144.949	0.443	
Max Sx	4724	101 TANK_FULL_ULS_1.5DL+1.5HT+1.5LL	-73.572	-5.116	0.000	0.000	0.000	146.184	144.949	0.443	
Min Sxy	4724	101 TANK_FULL_ULS_1.5DL+1.5HT+1.5LL	-73.572	-5.116	0.000	0.000	0.000	146.184	144.949	0.443	
Max Mx	4517	101 TANK_FULL_ULS_1.5DL+1.5HT+1.5LL	-73.601	-5.675	0.000	0.000	0.000	146.296	144.674	0.005	
Min Mx	4419	102 TANK_FULL_ULS_1.5DL+1.5WRL+1.5WDL (+) X	-285.028	-1208.096	0.000	0.000	0.000	-346.529	-62.752	35.433	
Max My	4688	101 TANK_FULL_ULS_1.5DL+1.5HT+1.5LL	-74.395	-2.734	0.000	0.000	0.000	144.735	146.108	0.408	
Min My	4431	102 TANK_FULL_ULS_1.5DL+1.5WRL+1.5WDL (+) X	1412.011	-226.831	0.000	0.000	0.000	-228.233	-242.114	-21.671	
Max Mx	4418	102 TANK_FULL_ULS_1.5DL+1.5WRL+1.5WDL (+) X	-755.321	-623.784	0.000	0.000	0.000	-195.814	-32.327	83.621	
Min Mxy	3728	102 TANK_FULL_ULS_1.5DL+1.5WRL+1.5WDL (+) X	-807.403	554.007	0.000	0.000	0.000	-179.564	-48.975	-96,343	

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VIII. CONCLUSIONS

Based on the study carried out, the following conclusions are drawn:.

- 1) The distribution of pressure below the foundation is very with the change subgrade modulus.
- 2) Maximum reduction in the negative moment along the MY and MX is more at top solid raft
- 3) The overturning resisting moment is increased in case soild raft
- 4) The steel is reduced by providing ring Beam system to the annular foundation.
- 5) During the analysis it has been observed that moments of the raft changes with respect to SBC.
- 6) The variation in ring beam size effect moment and shear force annular raft foundation.
- 7) It is also observed that the saving in cost of construction is 12% by the provision of Beam over the annular raft. There is about 10% saving in steel.

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