INTERNATIONAL JOURNAL
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IN APPLIED SCIENCE & ENGINEERING TECHNOLOGY

Finite Element Analysis of Connecting Rod using Composite Material

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Abstract: The connecting rod is the intermediate member between the piston and the Crankshaft. Its primary function is to transmit the push and pull from the piston pin to the crank pin, thus converting the reciprocating motion of the piston into rotary motion of the crank. This thesis describes designing and Analysis of connecting rod using composite materials. In this, drawing is drafted from the calculations. In this project connecting rod is replaced by aluminum based composite material reinforced with Boron carbide. And it also describes the modeling and analysis of connecting rod. NX solid modeling software is used to generate the 3-D solid model of Connecting rod. ANSYS software is used to analyze the connecting rod. The main aim of the project is to analysis the stress, strain, deformation of connecting rod by varying material with same geometry.
Keywords: Connecting Rod, Analysis of Connecting Rod, Aluminum Alloy Connecting Rod, Design and Analysis of Connecting Rod.

I. INTRODUCTION

Internal Combustion engine has many parts like cylinder, piston, connecting rod, crank and crank shaft. The connecting rod is very important part of an engine. A connecting rod is the part of a piston engine which connects the piston to the crankshaft. Together with the crank, the connecting rod converts the reciprocating motion of the piston into the rotation of the crankshaft. The connecting rod is required to transmit the compressive and tensile forces from the piston. The connecting rod consists of an I-beam cross-section and is made of forged steel. Aluminum alloy is also used for connecting rods. They are precisely matched in sets of similar weight in order to maintain engine balance. The lighter the connecting rod and piston, the greater the resulting in power and the lesser the vibration because the reciprocating weight is less. The connecting rod carries the power thrust from piston to the crankpin and hence it must be very strong, rigid and also as light as possible. There are two types of connecting rod: H-beam and I-beam or even a combination of the two. These connecting rods are utilized based on the area of application and usage. Figure 1 shows the parts of a connecting rod. The crank end is connected to the crank pin by a shaft. The pin and crank-end pinholes located at the top and bottom ends are machined to allow precise installation of bearings. These openings need to be identical and parallel. The top end of the connecting rod is attached to the piston by the piston pin. As the bottom end of the connecting rod rotates with the crankshaft, the top end is compelled to reverse on and forth on the piston pin. The bushing is essential due to the fact that of the high stress and temperature levels. The bottom hole in the connecting rod is divided to allow it to be secured around the crankshaft. The material is used for the rod is used for the cap which is then screwed by two screws. In the thesis by K. Sudershn Kumar, Dr. K. Tirupathi Reddy, Syed Altaf Hussain, for considering the parameters, the working factor of safety is nearer to theoretical factor of safety in aluminum boron carbide. Percentage of reduction in weight is same in Aluminum 360 and aluminum boron carbide. Percentage of increase in stiffness in aluminum boron carbide is more. Percentage of reducing in stress ALUMINIUM BORON CARBIDE and ALUMNUM is same than CARBON STEEL.

Fig. 1. Parts of Connecting Rod

II. HISTORY

The earliest evidence for a connecting rod appears in the late 3rd century AD Roman Hierapolis sawmill. It also appears in two 6th century Eastern Roman saw mills excavated at Ephesus respectively Gerasa. The crank and connecting rod mechanism of these Roman watermills converted the rotary motion of the waterwheel into the linear movement of the saw blades. Sometime between 1174 and 1206, the Arab inventor and engineer Al-Jazari described a machine which incorporated the connecting rod with a crankshaft to pump water as part of a water-raising machine, but the device was unnecessarily complex indicating that he still did not fully understand the concept of power conversion. In Renaissance Italy, the earliest evidence of a − albeit mechanically misunderstood–compound crank and connecting-rod is found in the sketch books of Taccola. A sound understanding of the motion involved displays the painter Pisanello (1455) who showed a piston-pump driven by a waterwheel and operated by two simple cranks and two connecting-rods.

III. METHODOLOGY

A. Problem Statement

The objective of the present work is to design and analyses of connecting rod made of Aluminum Alloy. Steel materials are used to design the connecting rod. In this project the material (Forged steel) of connecting rod replaced with Aluminum Alloy. Connecting rod was created in SIEMENS NX SOFTWARE. Model is imported in ANSYS WORKBENCH 14.0 for analysis. After analysis a comparison is made between existing steel connecting rod viz., An Aluminum Alloy in terms of weight, factor of safety, stiffens, deformation and stress.

B. Mechanical Properties of Carbon Steel, Aluminum 6061, Aluminum Boron carbide

Table 1. Material Properties

Sr. No.	Parameters	Carbon Steel	Aluminum 6061	Aluminum 6061 BORON Carbide
1	Density	2.7	2.68	7.87
2	Young's modules	70-80	195	200
3	Poisson's ratio	0.33	0.32	0.29

C. Pressure Calculation For 150cc Engine

Suzuki GS 150 R Specifications

Engine type air cooled 4-stroke

Bore × Stroke (mm) = 57×58.6

Displacement= 149.5CC

Maximum Power = 13.8 bhp @ 8500 rpm

Maximum Torque = 13.4 Nm @ 6000 rpm

Compression Ratio= 9.35/1

Density of Petrol C8H18 = 737.22kg/m3 = 737.22E-9kg/mm3

Temperature = 60F = 288.855K

Mass = Density × Volume = 737.22E-9×149.5E3 = 0.11Kg

Molecular Weight of Petrol =114.228 g/mole

From Gas Equation,

PV = MRT,

R = R*/Mw = 8.3143/.114228 = 72.76

P = (0.11x72.786x288.85) / 149.5E3

P = 15.469Mpa =16Mpa
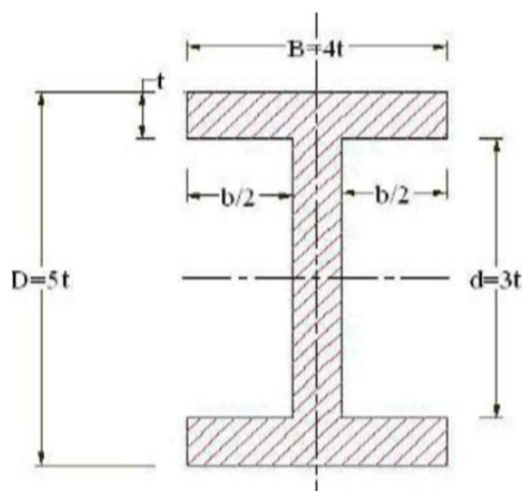
D. Design Calculations for Existing Connecting Rod

Fig. 2. Standard Dimension of I – Section

The standard dimension of I - SECTION

Thickness of flange & web of the section = t

Width of section B= 4t

Height of section H = 5t,

Area of section A=2(4t×t) +3t×t, A = 11t²

MI of section about x axis: $I_{xx} = 1/12 [4t \{5t\}^3 - 3t\{3t\}^3] = 419/12[t^4]$

MI of section about y axis: $I_{yy} = 2×1/12×t×\{4t\}^3 + 1/12\{3t\}t^3 = 131/12[t^4]$

$I_{xx}/I_{yy} = 3.2$

Length of connecting rod (L) = 2 times the stroke,

L = 117.2 mm

Buckling load Wb = maximum gas force × F.O.S Wb = 37663N,

Stroke length (l) = 117.2 mm

Diameter of a piston (D) = 57 mm

P=15.5 N/mm^2

Radius of crank (r) =stroke length /2 = 58.6/2 = 29.3 m

Maximum force on the piston due to pressure

FI = $\Pi/4*D^2*P = \Pi/4* (57)^2 *15.469 = 39473.16$N

Maximum angular speed $w_{max} = [2\Pi N_{MAX}]/60 = \{[2\Pi*8500]/60\}$,

$A = \pi r^2 = 768$ rad /sec

Ratio of length of connecting rod to radius of crank N = 1/r = 112/29.3 =3.8

Maximum inertia force of reciprocating parts F_{im} = Mr $(w_{max})^2$ r (cos ɵ +cos 2ɵ/n) (or)

F_{im} = Mr $(w_{max})^2$ r (1+l/n) = 0.11* $(768)^2$ *(0.0293)*(1+ (1/3.8)), F_{im} = 2376.26 N

Inner diameter of the small end d1 = F_g /pb_1 * l_1 = 6277.167/12.5*1.5d1 = 17.94 mm

σ_c= compressive yield stress = 415 Mpa,

$K_{xx}= I_{xx}/A$, K_{xx} =1.78t,

a= $\sigma_c/\pi r^2$, a= 0.0002

By substituting σc, A, a, L, K_{xx} on Wb

Wb = 4565t^4 -37663t^2 - 81639.46=0

t^2 = 10.03, t = 3.167 mm, t = 3.2 mm

Width of section B = 4t =4*3.2 = 12.8 mm

Height of section H = 5t = 5*3.2 =16 mm

Area A = $11t^2$ = 11*3.22 = 112.64 mm^2

Height at the big end (crank end) = H_2 = 1.1H to 1.25 H = 1.1*16 = 17.6 mm

Height at the small end (piston end) = H_1 = 0.9H to 0.75 H =0.9*16 = 12 mm

Where,

Design bearing pressure for small end Pb_1 = 12.5 to 15.4 N/mm^2

Length of the piston pin l1 = (1.5 to 2) d_1

Outer diameter of small end = d_1+ $2t_b$ + $2t_m$ =17.94 + [2*2] + [2*5] = 31.94 mm

Where,

Thickness of the bush (t_b) = 2 to 5 mm

Marginal thickness (t_m) = 5 to 15 mm

Inner diameter of a big end d_2 = F_g /Pb_1 * l2 =6277.167/10.8*1.0d_1 = 23.88 mm

Where,

Design bearing pressure foe big end Pb_2 = 10.8 to 12.6 N/mm^2

Length of the crank pin l_2 = (1.0 to 1.25)d_2,

Root diameter of the bolt = $((2F_{im})/ (\pi * st))^{\frac{1}{2}}$ = $(2*6277.167\pi *56.667)^{\frac{1}{2}}$ = 4 mm

Outer diameter of a big end = d_2+$2t_b$+$2d_b$+$2t_m$ = 23.88+2*2+2*4+2*5 =47.72 mm

Where,

Thickness of the bush [t_b] = 2 to 5 mm

Marginal thickness [t_m] = 5 to 15 mm

Nominal diameter of bolt [d_b] = 1.2 * root diameter of the bolt = 1.2×4 = 4.8mm

Thickness of flange and web of the section = t = 2

Width of the section B = 4t= 4×2 = 8

Height of the section H = 5t = 5×2 = 10

Area of the section A = 11t² = 11×4 = 44

Moment of inertia about x axis Ixx = 34.91t4 = 34.91×16 = 558.56

Moment of inertia about y axis Iyy = 10.91t4 = 10.91×16 = 174.56

Therefore Ixx/Iyy = 558.56/174.56 = 3.2

IV. DESIGNING OF CONNECTING ROD

A. Designing Procedure of Connecting Rod in SIEMENS NX Software

The modeling of the connecting rod is done using NX software. Open NX interface. Initially the inner and outer end i.e. piston end and the crank end diameter are drawn. Draw smaller holes of connecting rod on bog end diameter side. Then the small end and the big end diameter circles are padded respectively. After completion of padding of both big and small the stem of the connecting rod is created. The constructed steam is padded. After finishing the padding of steam pocket is applied to one side of the steam, mirror extent pocket is given in order to pocket the other side of stem. Edge fillets are assigned at the desired locations. Thus the required connecting rod is modeled using NX software.

V. ANALYSIS OF CONNECTING ROD

A. Introduction of Finite Element Method

The basic idea in the Finite Element Method is to find the solution of complicated problems with relatively easy way. The Finite Element Method has been a powerful tool for the numerical solution of a wide range of engineering problems. Applications range from deformation and stress analysis of automotive, aircraft, building, defense, and missile and bridge structures to the field of analysis of dynamics, stability, fracture mechanics, heat flux, fluid flow, magnetic flux, seepage, and other flow problems. With the advances in computer technology and CAD systems, complex problems can be modelled with relative ease.

To do the ANSYS we have chosen the workbench of 16 version. Then import the saved connecting rod model to the workbench by saving as part file, as it is easy to import easily for doing meshing and further process. Then go to static structural and insert the data and type of material used for analysis. Go to engineering data and give the density, Poisson's ratio and young's modules values.

Next go to geometry and import the part file of connecting which was save before in NX software. Then double click on the model now the actual workbench window opens.
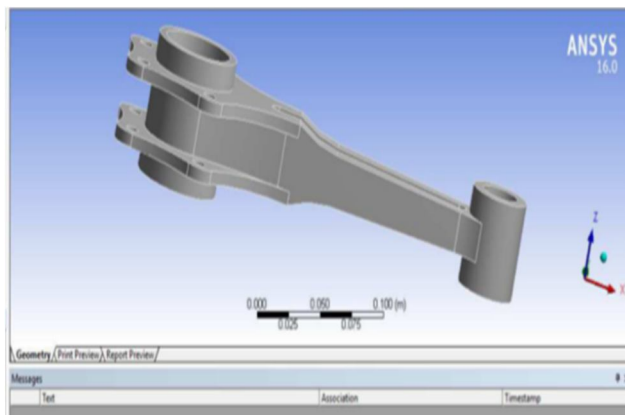
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ISSN: 2321-9653; IC Value: 45.98; SJ Impact Factor: 7.538
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Fig. 3. Connecting rod model in workbench
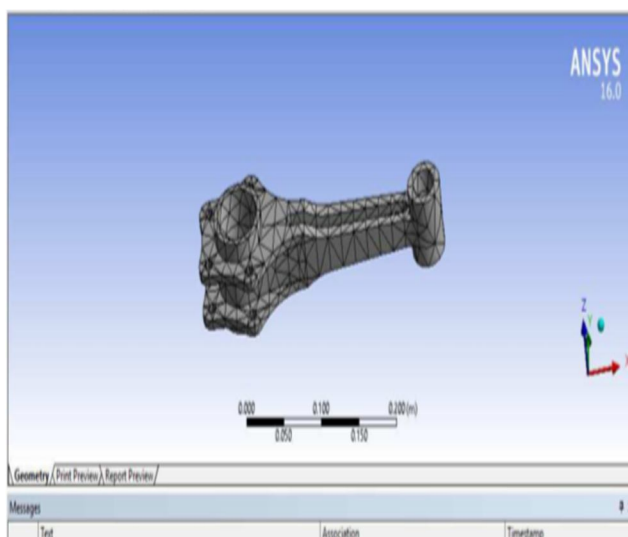
Fig. 4. Meshing of connecting rod
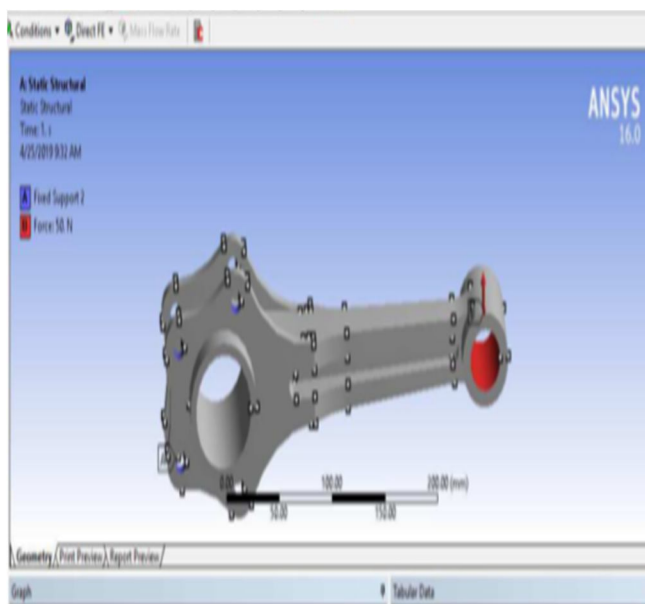
Fig. 5. Fixed supports and loads acting

B.   Carbon Steel Results

Model (A4) - Geometry - Parts	
Object Name	*ram u. stp*
State	Meshed
Graphics Properties	
Visible	Yes
Transparency	1
Definition	
Suppressed	No
Stiffness Behavior	Flexible
Coordinate System	Default Coordinate System
Reference Temperature	By Environment
Material	
Assignment	cc
Nonlinear Effects	Yes
Thermal Strain Effects	Yes
Bounding Box	
Length X	324.59 mm
Length Y	112. mm
Length Z	70. mm
Properties	
Volume	3.5248e+005 mm³
Mass	0. dat
Centroid X	79.211 mm
Centroid Y	-2.8771e-003 mm
Centroid Z	5.9689e-009 mm
Moment of Inertia Ip1	0. dat·mm²
Moment of Inertia Ip2	0. dat·mm²
Moment of Inertia Ip3	0. dat·mm²
Statistics	
Nodes	44167
Elements	26607
Mesh Metric	None

Fig. 6. Part Details

Model (A4) > Static Structural (A5) > Loads

Object Name	Fixed Support 2	Force
State	Fully Defined	
Scope		
Scoping Method	Geometry Selection	
Geometry	8 Faces	1 Face
Definition		
Type	Fixed Support	Force
Suppressed	No	
Define By		Components
Coordinate System		Global Coordinate System
X Component		0. N (ramped)
Y Component		-50. N (ramped)
Z Component		0. N (ramped)

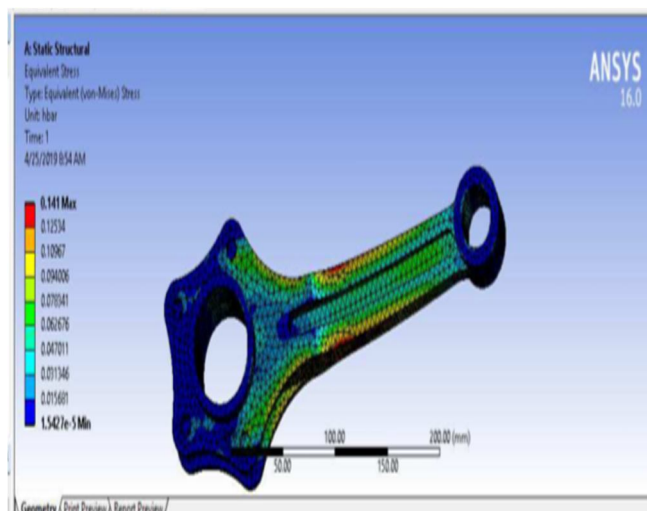Fig. 7. Loads Applied
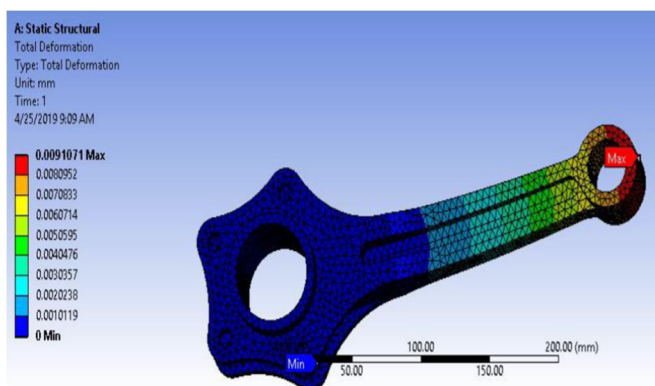
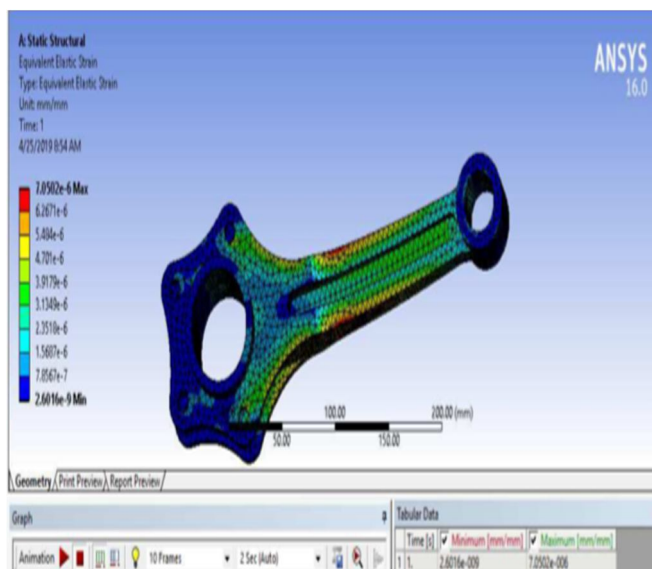Fig. 8. Total deformation of Connecting Rod

Fig. 9. Equivalent Stress

Fig. 10. Equivalent Elastic Strain

International Journal for Research in Applied Science & Engineering Technology (IJRASET)
ISSN: 2321-9653; IC Value: 45.98; SJ Impact Factor: 7.538
Volume 10 Issue V May 2022- Available at www.ijraset.com

C. Aluminum 6061

Model (A4) > Geometry > Parts	
Object Name	*ramu.stp*
State	Meshed
Graphics Properties	
Visible	Yes
Transparency	1
Definition	
Suppressed	No
Stiffness Behavior	Flexible
Coordinate System	Default Coordinate System
Reference Temperature	By Environment
Material	
Assignment	al 606
Nonlinear Effects	Yes
Thermal Strain Effects	Yes
Bounding Box	
Length X	324.59 mm
Length Y	112. mm
Length Z	70. mm
Properties	
Volume	3.5248e+005 mm³
Mass	0. dat
Centroid X	79.211 mm
Centroid Y	-2.8771e-003 mm
Centroid Z	5.9689e-009 mm
Moment of Inertia Ip1	0. dat·mm²
Moment of Inertia Ip2	0. dat·mm²
Moment of Inertia Ip3	0. dat·mm²
Statistics	
Nodes	44167
Elements	26607
Mesh Metric	None

Fig. 11. Part Details

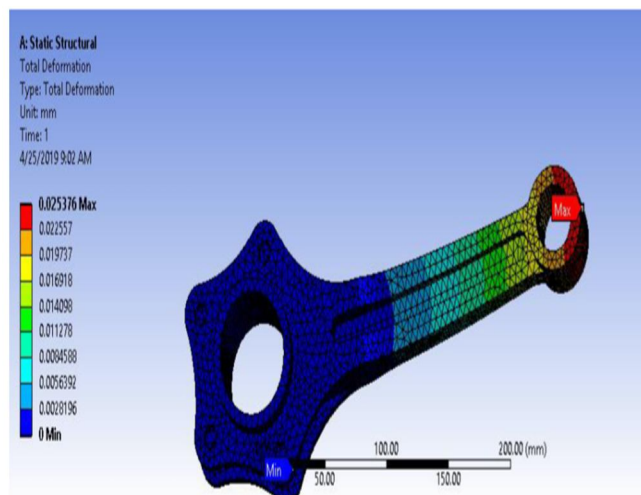| Model (A4)> Static Structural (A5) > Loads		
Object Name	*Fixed Support 2*	Force
State	Fully Defined	
Scope		
Scoping Method	Geometry Selection	
Geometry	8 Faces	1 Face
Definition		
Type	Fixed Support	Force
Suppressed	No	
Define By		Components
Coordinate System		Global Coordinate System
X Component		0. N (ramped)
Y Component		-50. N (ramped)
Z Component		0. N (ramped)

Fig. 12. Loads Applied
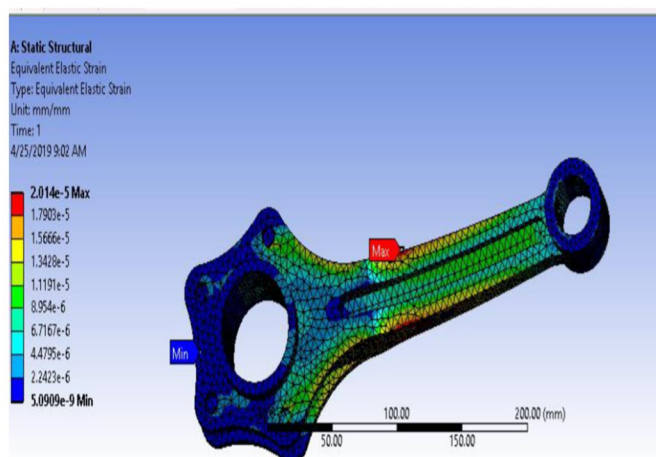
Fig. 13. Total Deformation
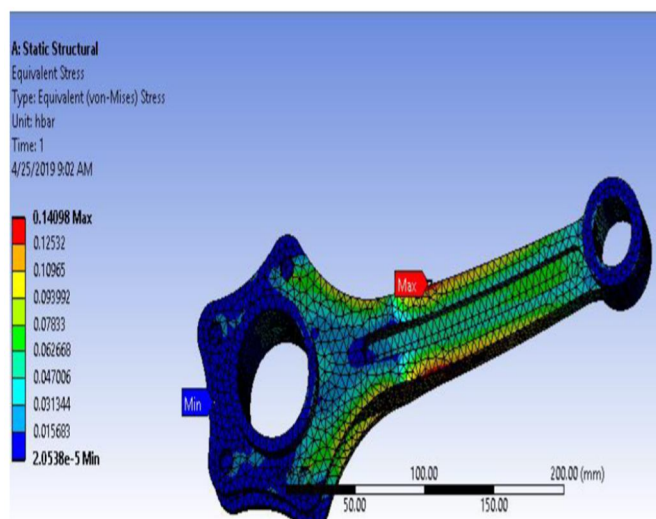

Fig. 14. Equivalent Elastic Strain

Fig. 15. Equivalent Stress

D. Aluminum 6061 Boron Carbide

Model (A4) > Geometry > Parts

Object Name	ram u. stp
State	Meshed
Graphics Properties	
Visible	Yes
Transparency	1
Definition	
Suppressed	No
Stiffness Behavior	Flexible
Coordinate System	Default Coordinate System
Reference Temperature	By Environment
Material	
Assignment	al b4+c
Nonlinear Effects	Yes
Thermal Strain Effects	Yes
Bounding Box	
Length X	324.59 mm
Length Y	112. mm
Length Z	70. mm
Properties	
Volume	3.5248e+005 mm³
Mass	0. dat
Centroid X	79.211 mm
Centroid Y	-2.8771e-003 mm
Centroid Z	5.9889e-009 mm
Moment of Inertia Ip1	0. dat·mm²
Moment of Inertia Ip2	0. dat·mm²
Moment of Inertia Ip3	0. dat·mm²
Statistics	
Nodes	44167
Elements	26607
Mesh Metric	None

Fig. 16. Part Details

Model (A4) > Static Structural (A5) > Loads

Object Name	Fixed Support 2	Force
State	Fully Defined	
Scope		
Scoping Method	Geometry Selection	
Geometry	8 Faces	1 Face
Definition		
Type	Fixed Support	Force
Suppressed	No	
Define By		Components
Coordinate System		Global Coordinate System
X Component		0. N (ramped)
Y Component		-50. N (ramped)
Z Component		0. N (ramped)

Fig. 17. Loads Applied
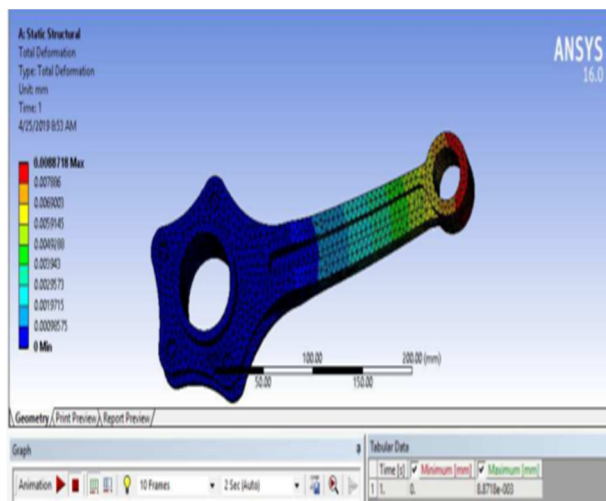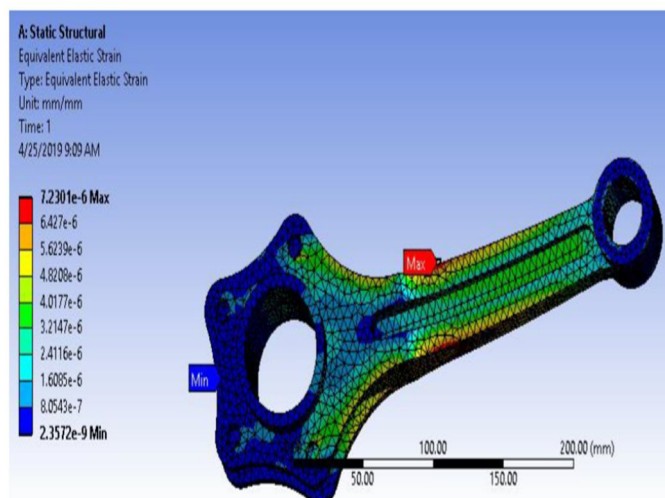
Fig. 12. Total Deformation
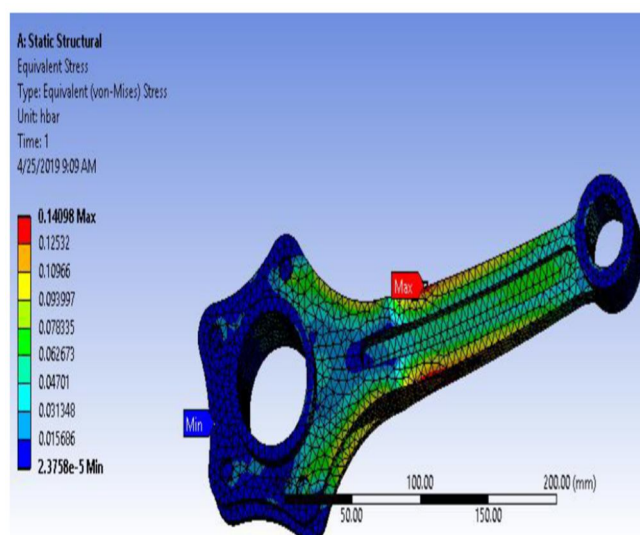

Fig. 13. Equivalent Elastic Strain

Fig. 14. Equivalent Stress

International Journal for Research in Applied Science & Engineering Technology (IJRASET)
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VI. CONCLUSION

In automotive industries, to achieve reduced fuel consumption as well as greenhouse gas emission is a current issue of utmost importance. To reduce automobile weight and improve fuel efficiency, the auto industry has dramatically increased the use of aluminum in light vehicles in recent years. Aluminum alloy based metal matrix composites (MMCs) with ceramic particulate reinforcement have shown great promise for such applications. These materials having a lower density and higher thermal conductivity as compared to the conventionally used.

Weight reduction of up to 50 – 60 % in the systems. Moreover, these advanced materials have the potential to perform better under severe service conditions like higher speed, higher load etc. The objective of the present work is to design and analysis of connecting rod made of Aluminum Alloy. Steel materials are used to design the connecting rod. In this project the material (Forged steel) of connecting rod replaced with Aluminum Alloy. Connecting rod was created in NX 11.0. Model is imported in ANSYS 16.0 for analysis. After analysis a comparison is made between existing steel connecting rod viz., An Aluminum Alloy in terms of weight, factor of safety, stiffens, deformation and stress. The present work aimed at evaluating alternate material for connecting rod with lesser stresses and lighter weight. This work found alternate material for minimizing stresses in connecting rod. FEA analysis performed using ANSYS WORKBENCH 16.0 software for determining stresses & deformation.

VII. FUTURE SCOPE

From analysis it is observed that the minimum stresses among all loading conditions, were found at crank end cap as well as at piston end. So the material can be reduced from those portions, thereby reducing material cost. For further optimization of material dynamic analysis of connecting rod is needed. After considering dynamic load conditions once again finite element analysis will have to be performed. It will give more accurate results than existing. Design modifications can be done to minimize the weight of the connecting rod and inertia force.

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