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# Investigation of Cementitious Material Oozing through Dams and Its Implications on Structural Health

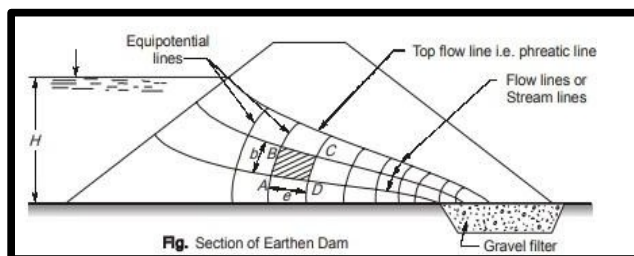
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**Abstract**—Concrete and masonry dams subjected to prolonged seepage undergo progressive physicochemical deterioration through calcium leaching, wherein calcium hydroxide ( $\text{Ca}(\text{OH})_2$ ) dissolves and migrates with seepage water, compromising cement paste integrity. This study investigates cementitious material collected from seepage-affected drainage galleries of two major Maharashtra dams—Upper Wardha Dam (Amravati) and Hatnur Dam (Jalgaon)—through systematic chemical analysis per IS 4032:1985. Seven parameters were determined: Loss on Ignition (LOI),  $\text{SiO}_2$ ,  $\text{R}_2\text{O}_3$ ,  $\text{CaO}$ ,  $\text{MgO}$ ,  $\text{SO}_3$ , and Insoluble Residue (IR). The CBIP methodology was applied to estimate cement loss per tonne of leached material. Results confirm significant  $\text{CaO}$  depletion (36–44% vs. 60–67% in fresh OPC) and extremely elevated LOI (>30%), confirming calcium leaching as the dominant deterioration mechanism. Estimated cement loss is 0.63t/t for Upper Wardha Dam and 0.67t/t for Hatnur Dam. Both dams are reclassified at moderate deterioration, requiring periodic monitoring rather than immediate structural intervention.

**Index Terms**—Calcium leaching, Cementitious material, Dam structural health, CBIP methodology, IS 4032, Seepage, Upper Wardha Dam, Hatnur Dam, Chemical deterioration, Efflorescence.

## I. INTRODUCTION

Dams are critical hydraulic structures serving irrigation, drinking water supply, hydropower, and flood control. In India, where rainfall is seasonal and unevenly distributed, dams are central to water resource management. However, long-term exposure to hydrostatic pressure and continuous seepage drives progressive structural deterioration that must be systematically monitored [2].



This paper presents a systematic chemical investigation of cementitious material oozing from the drainage galleries of Upper Wardha Dam (Amravati) and Hatnur Dam (Jalgaon), applying CBIP Miscellaneous Report No. 10 for cement loss estimation and IS 4032:1985 for chemical analysis. The quantitative, sensor-analogue data-collection philosophy mirrors automated precision monitoring systems in modern infrastructure [1].

### A. Motivation

Cementitious material oozing through dam faces signals active transport of cement paste and leachates along seepage paths. Persistent oozing indicates hydraulic connectivity and deterioration warranting structural health monitoring (SHM). Understanding this phenomenon is critical for early damage warning, evidence-based maintenance, and cost-effective rehabilitation planning.

### B. Paper Organization

Section II reviews literature; Section III describes the problem and dams studied; Section IV details methodology; Section V presents results; Section VI provides comparative analysis; Section VII discusses remedial measures; and Section VIII concludes with recommendations.

## II. LITERATURE REVIEW

### A. Calcium Leaching in Dam Concrete

Nie et al. [4] demonstrated that soft-water-induced calcium leaching causes measurable microstructural deterioration in dam concrete, combining SEM/ICP-MS microscopy with numerical modeling to predict long-term dissolution depth and mechanical property reduction. Guo et al. [5] developed a coupled seepage-dissolution numerical model, finding that dissolution increases porosity and permeability of anti-seepage walls—directly paralleling field observations at both dams studied here.

### B. Mechanical Effects of Leaching

Huang et al. [6] confirmed that calcium leaching reduces compressive strength, increases porosity, and shortens service life. Zhang et al. [7] quantified increased porosity/permeability due to leaching and recommended minimizing  $\text{Ca}(\text{OH})_2$  content and adding SCM to slow deterioration rates. Wang et al. further showed lower cement content and high permeability increase leaching rates [8].

### C. Seepage Control and SHM

El-Molla [9] reviewed modern seepage detection and treatment methods including grouting and cutoff walls, highlighting gaps in continuous monitoring for material loss. Vigneswaran et al. [10] demonstrated field grouting strategies to arrest oozing in masonry dams. The analogy to automated sensor-driven irrigation control [1] is instructive: chemical markers in leached material serve as quantitative triggers for maintenance interventions, analogous to soil moisture thresholds triggering pump control.

### D. Research Gap

Integrated chemical characterization studies on Indian dams using the CBIP methodology—with comparative deterioration staging across multiple structures—remain limited. This work addresses that gap through field-collected sample analysis from two dams with differing construction periods and reservoir characteristics.

## III. PROBLEM STATEMENT AND STUDY DAMS

### A. Problem Statement

Progressive seepage through cracks, joints, and porous zones in concrete or masonry dams leads to dissolution and transport of cementitious material, precipitating efflorescence or ooze on dam surfaces and gallery floors. No IS standard specifies permissible limits for chemical constituents of dam leached material. Consequently, IS 4032:1985 (Methods for Chemical Analysis of Hydraulic Cement) is used as a reference baseline with CBIP Report No. 10 guidelines for cement loss estimation. Seven constituents are tested (all as % by dry weight):

- Loss on Ignition (LOI)
- Silicon Dioxide ( $\text{SiO}_2$ )
- Metal Oxide ( $\text{R}_2\text{O}_3 = \text{Fe}_2\text{O}_3 + \text{Al}_2\text{O}_3$ )
- Calcium Oxide ( $\text{CaO}$ )
- Magnesium Oxide ( $\text{MgO}$ )
- Sulphate ( $\text{SO}_3$ )
- Insoluble Residue (IR)

### B. Upper Wardha Dam

Upper Wardha Dam (D02982), also known as Nal Damayanti Sagar, is built on the Wardha River near Simbhora village, Morshitaluka, Amravati district. It is a composite dam: central masonry/gravity spillway (~331.50 m) with earthen embankment wings (~5,588.50 m), total length 5,920 m, masonry height 46.20 m. Gross storage capacity: 786.48 MCM (27.8 TMC); catchment area: 4,302  $\text{km}^2$ ; gross command area: 1,04,400 ha. Construction completed 1993; spillway has 13 radial gates.

**C. HatnurDam**

Hatnur Dam (D02977), also known as the Tapi Project, is constructed across the Tapi River near Hatnur village, Bhusawal taluka, Jalgaon district. Composite earthfill dam with masonry/gravity and spillway sections; total length 2,580 m; height 25.50 m. Gross storage: 388.00 MCM; catchment area: 29,430 km<sup>2</sup>. Completed 1982; 41 radial gates (12 m × 6.50 m); design discharge ~26,423 m<sup>3</sup>/s.

**IV. METHODOLOGY**

**A. SampleCollection**

Cementitious material (semi-solid/sludge) was collected from foundation galleries, drainage sumps, and downstream oozing locations at both dams. For Upper Wardha Dam, six samples were taken at chainages CH-893.5m, 778.5m, 715m, 682.5 m, 672 m, and 940.5 m. For Hatnur Dam, four samples were collected at RD-910, 945, 985, and CH-1045. Samples (~1 kg each) were sealed in polyethylene bags with identification marks per CBIP Report No. 10 guidelines.

**B. ChemicalAnalysis(IS4032:1985)**

All tests were performed per IS 4032:1985. Key procedures:

- LOI: 1.00g sample heated at 900–1000°C for 15 min in muffle furnace; loss in weight recorded.
- SiO<sub>2</sub>: 0.5g dissolved in HCl, evaporated on steam bath, filtered (Whatman No. 40); residue weighed.
- R<sub>2</sub>O<sub>3</sub>: Combined hydroxides precipitated by NH<sub>4</sub>OH from SiO<sub>2</sub> filtrate; ignited at 1050–1100°C.
- CaO: Calcium oxalate gravimetric method; ignited at 1100–1200°C.
- MgO: Mg ammonium phosphate gravimetric method; MgO% = W × 72.4.
- SO<sub>3</sub>: BaSO<sub>4</sub> precipitation; ignited at 800–900°C; SO<sub>3</sub>% = W × 34.3.
- IR: HCl-insoluble residue digested in Na<sub>2</sub>CO<sub>3</sub>; ignited at 900–1000°C.

**C. CementLoss(CBIPMethodology)**

Per CBIP Report No. 10 (1986), OPC contains 44% calcium by mass; thus 1 tonne cement = 440 kg Ca = 814 kg Ca(OH)<sub>2</sub>. The CaO content of leached material is stoichiometrically converted to Ca(OH)<sub>2</sub> using the factor 74/56 = 1.321. Cement loss is then:

$$\text{Cement Loss} = [\text{CaO}_{\text{ma}} (\text{kg}) \times (74/56)] / 814$$

**V. OBSERVATIONS AND RESULTS**

**A. UpperWardhaDam—ChemicalResults**

Table I presents chemical test results for six samples from the Upper Wardha Dam foundation gallery.

Parameter	S-1	S-2	S-3	S-4	S-5	S-6
LOI(%)	37.00	36.00	36.70	31.00	37.83	37.83
SiO <sub>2</sub> (%)	7.02	8.00	6.00	4.04	4.86	6.66
R <sub>2</sub> O <sub>3</sub> (%)	7.60	5.74	5.10	4.80	3.14	5.14
CaO(%)	36.00	37.42	37.00	41.96	40.52	40.52
MgO(%)	5.07	3.63	4.31	4.87	4.65	3.20
SO <sub>3</sub> (%)	1.03	1.34	1.03	3.78	1.29	1.29
IR(%)	6.28	7.87	9.86	9.55	7.71	5.36

TABLE I. Chemical Test Results—Upper Wardha Dam (%)

**B. HatnurDam—ChemicalResults**

Table II presents chemical test results for four samples from Hatnur Dam drainage gallery.

Parameter	S-1RD910	S-2RD945	S-3RD985	S-4CH1045
LOI(%)	36.00	39.00	33.00	33.00
SiO <sub>2</sub> (%)	5.00	4.00	4.00	5.06
R <sub>2</sub> O <sub>3</sub> (%)	9.94	6.84	6.00	6.64

CaO(%)	41.20	36.00	43.00	43.92
MgO(%)	2.90	6.52	4.37	3.37
SO <sub>3</sub> (%)	1.72	1.34	4.96	3.15
IR(%)	3.24	6.30	4.67	4.86

TABLE II. Chemical Test Results—Hatnur Dam (%)

C. Cement Loss Estimation

Average CaO: Upper Wardha = 38.90%; Hatnur = 41.03%.

Applying CBIP methodology:

Dam	Avg CaO %	CaO kg/t	Ca(OH) <sub>2</sub> kg	Conv. Factor	Cement Loss t/t
Upper Wardha	38.90%	389	514	74/56	0.63
Hatnur Dam	41.03%	410	542	74/56	0.67

TABLE III. Cement Loss Estimation (CBIP Method)

VI. COMPARATIVE ANALYSIS AND ENGINEERING INTERPRETATION

A. Comparison with IS 269 Limits

IS 269 specifies limits for fresh OPC. These serve as a reference baseline for assessing chemical alteration in dam leached material, not as pass/fail criteria. Table IV presents the comparison.

Param	IS 269 Limit	Upper Wardha	Hatnur	Trend
LOI	≤ 5%	31–38%	33–39%	Very High
CaO	60–67%	36–42%	36–44%	Depleted
IR	≤ 2%	5.4–9.9%	3.2–6.3%	Elevated
SO <sub>3</sub>	≤ 3.5%	1.0–3.8%	1.3–5.0%	Mostly OK
MgO	≤ 6%	3.2–5.1%	2.9–6.5%	Normal
SiO <sub>2</sub>	18–25%	4.0–8.0%	4.0–5.1%	Depleted

TABLE IV. Comparison with IS 269 Reference Limits

B. Key Observations

- CaO ↓ (36–44% vs. 60–67% fresh): Confirms calcium leaching.
- LOI ↑ (>30% vs. ≤5% limit): Advanced carbonation and ageing of hydrated cement phases.
- IR ↑ (5–10% vs. ≤2%): Cement paste removal; Upper Wardha more affected.
- SO<sub>3</sub>: Mostly within limits; one localized high value at Upper Wardha (3.78%).
- MgO: Within permissible limits at both dams; no magnesium attack.
- SiO<sub>2</sub>: Greatly reduced from fresh cement range (18–25%), consistent with silica dissolution.

C. Deterioration Staging

The convergence of CaO ↓ + LOI ↑ + IR ↑ unambiguously identifies calcium leaching as the primary deterioration mode, consistent with the self-reinforcing cycle: Ca(OH)<sub>2</sub> dissolution → porosity increase → greater seepage → further leaching [4,5,6].

- Upper Wardha Dam: CaO 36–42%, LOI >30%, IR 5–10% → Moderate to Active Deterioration.
- Hatnur Dam: CaO 36–44%, lower IR, normal SO<sub>3</sub> → Early to Moderate Deterioration.

No evidence of severe sulphate attack or magnesium-induced deterioration was found at either dam. Structural integrity is not immediately threatened; deterioration is progressive and manageable.

## VII. REMEDIAL MEASURES AND RECOMMENDATIONS

### A. Preventive Measures

- Dense, low water-cement ratio concrete to minimize seepage pathways.
- Use of SCMs (flyash, GGBS, silica fume) to consume free  $\text{Ca}(\text{OH})_2$ .
- Upstream face treatment with rich mortar masonry, Khanki facing, or gunite lining.
- Proper aggregate selection to avoid alkali-aggregate reaction.
- Pressure grouting in localized gallery zones showing elevated oozing.

### B. Monitoring Recommendations

- Chemical testing of cementitious deposit every 2–3 years.
- Trend analysis of CaO, LOI, and IR over time.
- Seasonal monitoring of seepage discharge quantity and calcium concentration.
- 20–30 year chemical deterioration tracking program.
- Initiate detailed structural review if CaO falls below 35%.
- Risk classification update every 5 years.

### C. Future Scope

Future work should include: (i) SEM/XRD microstructural analysis of leached material; (ii) long-term seepage water chemistry trend analysis; (iii) IoT/sensor-based remote gallery monitoring analogous to automated sensor-driven infrastructure systems [1]; (iv) seepage-dissolution coupled numerical modelling; and (v) evaluation of SCM-based repair grouts for improved leaching resistance [7].

## VIII. CONCLUSIONS

This paper presented a systematic chemical investigation of cementitious material oozing from two major Maharashtra dams. Key conclusions are:

- 1) Both dams exhibit calcium leaching as the primary deterioration mechanism, confirmed by CaO depletion, elevated LOI, and increased insoluble residue.
- 2) Estimated cement loss is 0.63t/t (Upper Wardha Dam) and
- 3) 0.67t/t (Hatnur Dam) per the CBIP methodology.
- 4) Upper Wardha Dam: Moderate to Active Deterioration. Hatnur Dam: Early to Moderate Deterioration.
- 5) No evidence of severe sulphate or magnesium attack at either dam.
- 6) Chemical ageing (LOI >30%) is significant at both dams, reflecting long-term carbonation of hydrated cement phases.
- 7) Periodic chemical monitoring every 2–3 years is recommended; immediate structural intervention is not warranted.
- 8) The quantitative, data-driven monitoring approach parallels precision sensor-based infrastructure management philosophies [1,2].

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