



iJRASET

International Journal For Research in
Applied Science and Engineering Technology



INTERNATIONAL JOURNAL FOR RESEARCH

IN APPLIED SCIENCE & ENGINEERING TECHNOLOGY

Volume: 11 Issue: VIII Month of publication: Aug 2023

DOI: <https://doi.org/10.22214/ijraset.2023.55137>

www.ijraset.com

Call:  08813907089

E-mail ID: ijraset@gmail.com

Numerical Investigations of Multilayered Sandwich Structures under Free Vibrations

Sandeep M Shiyekar

Department of Civil Engineering, D Y Patil College of Engineering, Akurdi, Pune

Abstract: Important structural properties of composite materials, such as high strength-to-weight and high stiffness-to-weight ratios, have resulted in a great need for these materials in various engineering industries, such as Mechanical, Civil, Automobile and Aerospace Engineering. This paper presents results from numerical investigations using software based on Finite Element Method (FEM) and its comparison with other theories from the literature under free vibrations of 5 and 7 layered sandwich plates. This study utilizes the finite element method to perform modal analysis of a sandwich composite plate with a honeycomb core. In this paper, the modal responses of a flat rectangular sandwich plate with a honeycomb core using FEM software are presented. To confirm the accuracy and reliability of the current model, validation with present literature is studied. In this study, aluminum honeycomb is used as the core materials, while glass fiber reinforced composite is used for the top and bottom of the plate to examine modal responses. Free vibration responses are investigated for the various boundary situations. The modal analysis of composite sandwich constructions was investigated, and the results were verified using available literature. The sandwich structure was solved using a finite element approach, which was modeled in ABAQUS software. The results indicated that frequencies by FEM software are in good agreement with other literature results.

Keywords: ABAQUS, Finite Element Method, Free Vibrations, Modal Analysis, Sandwich Plates .

I. INTRODUCTION

Sandwich structures are widely used in aerospace, automotive, and construction industries due to their lightweight and high stiffness properties. Free vibration analysis of sandwich structures is important for understanding their dynamic behavior, which is essential for design and optimization purposes. Free vibrations of sandwich structures can be analyzed using various methods, including analytical, numerical, and experimental techniques. Analytical methods, such as classical lamination theory and higher-order sandwich panel theories, provide closed-form solutions for simple sandwich structures. Numerical methods, such as finite element analysis, can handle more complex geometries and material properties, but require significant computational resources. Experimental methods, such as modal analysis, provide direct measurement of the natural frequencies and modes of vibration of the sandwich structures. The vibrational behavior of sandwich structures is affected by various factors, such as the geometry, material properties, boundary conditions, and loading conditions. The presence of core materials, such as foam or honeycomb, can significantly affect the vibration modes and frequencies of the sandwich structures. Delamination, which is a common failure mode in sandwich structures, can also affect the vibrational behavior by altering the stiffness and damping properties of the structure. Free vibration analysis of sandwich structures is essential for the design and optimization of structures that require high dynamic performance. By understanding the natural frequencies and modes of vibration of the sandwich structures, engineers can design structures that avoid resonance and reduce the risk of failure due to dynamic loads. Ahmed [1] used finite element displacement method to investigate the free vibration characteristics of curved sandwich beams under clamped-clamped boundary conditions. Goyal [2] studied the free vibrations of sandwich beams having a central mass. Shu [3] solved the free vibrations of sandwich beams with single and double delamination analytically. Frostig and Baruch [4] presented a free vibration analysis of sandwich beams under simply supported boundary conditions based on a higher-order beam theory for the skins and a two-dimensional elasticity solution for the core. By applying the discrete Green function, a free vibration analysis of a three-layer sandwich beam with an elastic or viscoelastic core and arbitrary boundary conditions was presented by Sakiyama et al. [5]. Furthermore, a related work about free vibration of stiffened rectangular plates using Green's functions was presented in [6]. Kameswara Rao et al. [7] used a fully third-order model of laminated composite and sandwich beams based on a higher-order mixed theory. Kapuria et al. [8] presented a third-order zig-zag theory for the static, free and forced vibration analysis of sandwich beams. Bhargale and Ganesan [9] studied the buckling and vibration behavior of a functionally graded material sandwich beam having constrained viscoelastic layer in thermal environment by using the finite element method. An assessment of higher-order and zig-zag displacement-based theories for the stability and free vibration of sandwich beams was proposed by Wu and Chen [10].

Kulkarni and Kapuria [11] focuses on the development of an improved numerical method for analyzing the free vibration behavior of composite and sandwich plates. The authors introduce a discrete Kirchhoff quadrilateral element that incorporates the third-order zigzag theory. This approach allows for a more accurate representation of the displacement field and captures the shear deformation effects that are present in composite and sandwich plates. The element is formulated based on the variational principle and includes the effect of transverse shear stresses using the third-order zigzag theory. Wang et al. [12] addresses the analysis of the free vibration behavior of skew sandwich plates with laminated facings. Skew plates are structural elements with non-orthogonal angles between their principal axes and the plate boundaries. The authors present a comprehensive study on the free vibration characteristics of skew sandwich plates by employing a numerical approach. They developed a finite element model based on the Mindlin plate theory, which considers the effects of transverse shear deformation and rotary inertia. The laminated facings are modeled using the layer-wise theory, accounting for the individual stiffness and orientation of each layer. Chakrabarti and Sheikh [13] introduce a new refined element for analyzing the vibration of laminate-faced sandwich plates. Their study aims to enhance the accuracy of numerical simulations by considering higher-order effects and accurately capturing the behavior of these complex structures. Belarbi et al. [14] present a layerwise finite element formulation for the free vibration analysis of laminated composite and sandwich plates. Their work focuses on developing an accurate numerical model that accounts for the layer-wise variations in material properties, providing a reliable tool for predicting the dynamic behavior of these plates. Burlayenko et al. [15] evaluate displacement-based finite element models used for the free vibration analysis of homogeneous and composite plates. Their study compares different models and assesses their accuracy in predicting natural frequencies and mode shapes, highlighting the strengths and limitations of each approach. Rahmani et al. [16] investigate the free vibration response of a composite sandwich cylindrical shell with a flexible core. Their study focuses on the dynamic behavior of this specific configuration and explores the effects of core flexibility on the natural frequencies and mode shapes of the shell structure. Malekzadeh and Sayyidmousavi [17] analyze the free vibration of sandwich plates with a uniformly distributed attached mass, flexible core, and different boundary conditions. Their research explores the influence of various parameters on the vibration behavior and provides insights into the design and optimization of sandwich plate structures. Jam et al. [18] propose an improved high-order theory for the analysis of the free vibration of sandwich panels. Their study aims to overcome the limitations of existing theories and provide a more accurate prediction of natural frequencies and mode shapes for these structures. Meunier and Shenoi [19] investigate the free vibration analysis of composite sandwich plates. Their work focuses on analyzing the dynamic behavior of these plates and provides valuable insights into the effects of material properties, geometric parameters, and boundary conditions on the natural frequencies and mode shapes. Nayak et al. [20] study the free vibration analysis of composite sandwich plates based on Reddy's higher-order theory. Their research aims to improve the accuracy of numerical models by considering higher-order effects and providing more reliable predictions of the dynamic behavior of these plates. In summary, the reviewed papers contribute to the understanding of free vibration analysis in composite and sandwich plates. They introduce refined element formulations, layerwise finite element models, and improved theories to accurately predict natural frequencies and mode shapes. These studies provide valuable insights for the design, analysis, and optimization of composite and sandwich plate structures in various applications. In this paper free vibration analysis is presented using ABAQUS [21] FE tool.

II. FREE VIBRATION ANALYSIS OF SANDWICH PLATE

A. Example 1: Free Vibrations of five layered symmetric sandwich plate

In this example, a five-layer ($0^\circ/90^\circ/\text{CORE}/90^\circ/0^\circ$) symmetric sandwich plate is considered with each ply in the face sheets being of thickness $0.05h$, and core of thickness $0.8h$. The elastic material properties are taken from Table 1. Table 2 shows the comparison of first mode frequency of 5 layered symmetric cross ply sandwich plate with all sides simply supported. The comparison is made with analytical and numerical Finite Element Methods.

Table 1. Material Properties of 5 layered composite sandwich plate

| Quantity | Unit | Face Sheet | Core |
|------------|-------------------|------------|---------|
| E_1 | GPa | 276 | 0.5776 |
| E_2 | GPa | 6.9 | 0.5776 |
| E_3 | GPa | 6.9 | 0.5776 |
| G_{12} | GPa | 6.9 | 0.1079 |
| G_{23} | GPa | 6.9 | 0.22215 |
| G_{31} | GPa | 6.9 | 0.1079 |
| ν_{12} | 0.28 | 0.0025 | 0.3 |
| ν_{13} | 0.28 | 0.0025 | 0.3 |
| ν_{23} | 0.33 | 0.0025 | 0.3 |
| ρ | Kg/m ³ | 681.8 | 1,000 |

Table 2. Comparison of first mode frequency of 5 layered symmetric cross ply sandwich plate (SSSS)

| S | ABAQUS Present | Belarbi et al. [14] | Kulkarni and Kapurja [11] | Kulkarni and Kapurja [11] | Wang et al. [12] | Chakrabarti and Shaikh [13] | % error wrt [11] |
|------|-------------------|------------------------|------------------------------------|------------------------------------|---------------------|-----------------------------------|---------------------------|
| 6.67 | 10.44378 | 10.564 | 10.524 | 13.315 | 11.414 | 10.56 | -0.76 |
| 10 | 9.775746 | 9.871 | 9.828 | 12.088 | 10.555 | 10.051 | -0.53 |
| 20 | 7.640946 | 7.742 | 7.6880 | 8.721 | 8.029 | 7.927 | -0.61 |

The comparison of present ABAQUS with other theories of first mode natural frequency of five layered cross ply sandwich plate (SSSS) is presented in Table 2, Numerical results are in good agreement with 3D elasticity and FEM results. ABAQUS gives marginal 0.76 % error. Following Figs. 1-4 show frequencies for various plate boundary conditions, like SCSC and CCCC and for aspect ratios 5 and 10, ABAQUS shows satisfactory agreement with other theories reported in the literature.

B. Example 2: Free Vibrations of seven layered symmetric cross ply and angle ply laminated sandwich plate

In this example, a 7 layered symmetric cross and angle ply laminated composite sandwich plate is analyzed under free vibrations. ABAQUS modelling is carried out considering S4R: A 4-node doubly curved thin or thick shell, reduced integration, hourglass control, finite membrane strains element. The material properties are given in Table 3. Tables 4 and 5 present comparison of first 4 mode frequencies for cross ply and angle ply laminated sandwich plates.

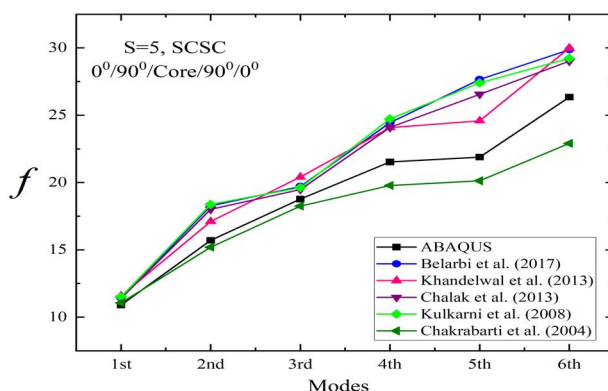


Fig. 1. Natural frequencies of 5 layered symmetric cross ply sandwich plate for S = 5, SCSC boundary condition.

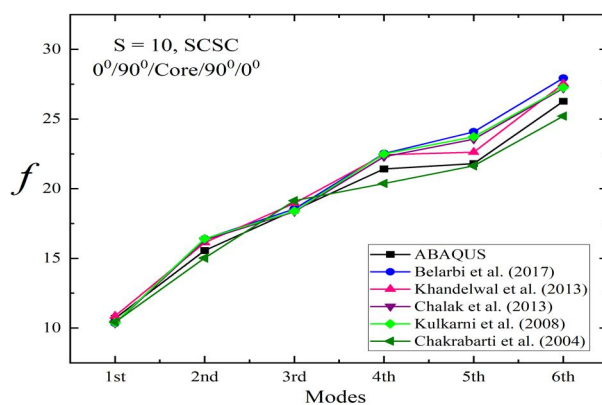


Fig. 2. Natural frequencies of 5 layered symmetric cross ply sandwich plate for S = 10, SCSC boundary condition.

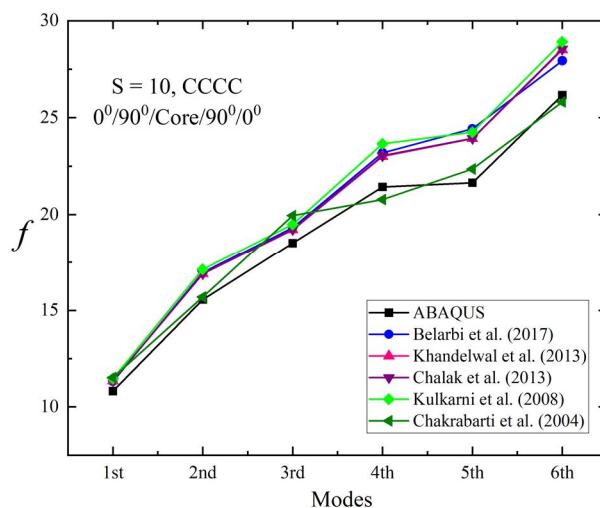


Fig. 3. Natural frequencies of 5 layered symmetric cross ply sandwich plate for $S = 10$, CCCC boundary condition.

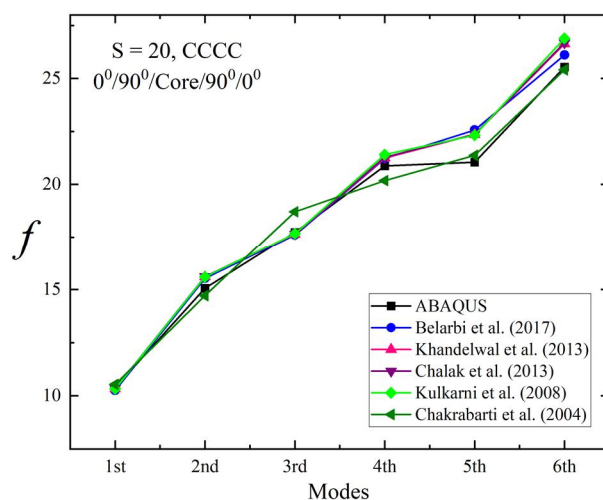


Fig. 4. Natural frequencies of 5 layered symmetric cross ply sandwich plate for $S = 20$, CCCC boundary condition.

Table 3. Material properties of 7 layered sandwich plate

| | E1 | E2 | E3 | G12 | G13 | G23 | ν | ρ |
|----------------|-------|-------|-------|-------|-------|-------|-------|-------------------|
| Material | (GPa) | (GPa) | (GPa) | (GPa) | (GPa) | (GPa) | | kg/m ³ |
| FRP | 24.51 | 7.77 | 7.77 | 3.34 | 3.34 | 1.34 | 0.25 | 1800 |
| Face Sheets | | | | | | | | |
| PVC | 0.103 | 0.103 | 0.103 | 0.05 | 0.05 | 0.05 | 0.32 | 130 |
| Core | 6 | 6 | 6 | | | | | |
| C70.130 | | | | | | | | |

Table 4. Comparison of present ABAQUS FEM results of first natural frequency of 7 layered symmetrical cross ply laminated sandwich plate

| $0^0/90^0/0^0/\text{CORE}/0^0/90^0/0^0$ Plate | Theory | Mode 1 | Mode 2 | Mode 3 | Mode 4 |
|--|-----------------------|----------|----------|----------|----------|
| Present ABAQUS | 4 Noded Shell Element | 13.78835 | 26.18084 | 26.78262 | 34.90808 |
| Belarbi et al. [14] | QSFT52 (16x16) | 14.44 | 26.826 | 27.456 | 35.706 |
| Burlayenko et al. [15] | FEM-3D-LW | 14.62 | 26.8 | 27.4 | 35.55 |
| Rahmani et al. [16] | Analytical LW | 14.27 | 26.31 | 27.04 | 34.95 |
| Malekzadeh, K et al. [17] | FEM-3D-LW | 14.74 | 26.83 | 27.53 | 35.6 |
| Jam et al. [18] | Analytical-LW | 15.04 | 26.733 | 27.329 | 35.316 |
| Meunier and Shenoi [19] | Analytical-HSDT | 15.28 | 28.69 | 30.01 | 38.86 |
| Nayak et al. [20] | FEM-Q9-HSDT | 15.04 | 28.1 | 29.2 | 37.76 |
| Nayak et al. [20] | FEM-Q4-HSDT | 15.34 | 30.18 | 31.96 | 40.94 |

The example investigates the convergence of a ABAQUS FE modelling by examining a simply supported square sandwich plate consisting of seven layers. Two sandwich plates with different lay ups on the face sheets, namely $[0^0/90^0/0^0/\text{CORE}/0^0/90^0/0^0]$ and $[45^0/-45^0/45^0/\text{CORE}/-45^0/45^0/-45^0]$, are considered. The core material is HEREX-C70.130 PVC foam, while the face sheets are composed of glass polyester resin. The plate has the following geometric properties: $a/h = 10$, $a/b = 1$, and $h_c/h = 0.88$, where h represents the total plate thickness. The comparison involves analytical solutions based on the Layerwise (LW) approach by Jam et al. [18] and Rahmani et al. [16]. Three-dimensional (3D) finite element (FE) models also based on the LW approach (FEM-3D-LW) by Aalekzadeh and Sayyidmousavi [17] and Burlayenko et al. [15]. FEM-Q9 and Q4 solutions based on the Higher-Order Shear Deformation Theory (HSDT) by Nayak et al. [20], and another analytical solution based on HSDT by Meunier and Shenoi [19]. The comparison results demonstrate the performance and convergence of the current FE modelling.

Table 4 presents the initial four dimensionless natural frequencies of $0^0/90^0/0^0/\text{CORE}/0^0/90^0/0^0$ symmetric sandwich plate, which were calculated in this paper and compared by the work of other authors. The finite element (FE) and analytical models are compared by analyzing a thick sandwich plate with a soft foam core. The present ABAQUS uses 4 node shell element and gives the frequency slightly higher than other FE models for mode 1. In mode 2, the frequency predicted by ABAQUS is slightly less than other models. In mode 3 and 4, higher than other FE and analytical models as shown in Table 4. Table 5 demonstrates Comparison of present ABAQUS FEM results of first 4 natural frequencies of 7 layered symmetrical angle ply ($45^0/-45^0/45^0/\text{CORE}/45^0/-45^0/45^0$) laminated sandwich plates. Here ABAQUS underpredicts the frequencies as compared to other analytical and FE solutions.

Table 5. Comparison of present ABAQUS FEM results of first natural frequency of 7 layered symmetrical angle ply laminated sandwich plate

| $45^0/-45^0/45^0/\text{CORE}/45^0/-45^0/45^0$ Plate | Theory | Mode 1 | Mode 2 | Mode 3 | Mode 4 |
|--|-----------------------|----------|----------|----------|----------|
| Present ABAQUS | 4 Noded Shell Element | 13.94671 | 26.24666 | 26.53882 | 35.13882 |
| Belarbi et al. [14] | QSFT52 | 15.419 | 28.756 | 27.456 | 35.706 |
| Burlayenko et al. [15] | FEM-3D-LW | 15.405 | 26.8 | 27.4 | 35.55 |
| Rahmani et al. [16] | Analytical LW | 15.42 | 26.31 | 27.04 | 34.95 |
| Malekzadeh, K et al. [17] | FEM-3D-LW | 14.74 | 26.83 | 27.53 | 35.6 |
| Jam et al. [18] | Analytical-LW | 15.81 | 26.733 | 27.329 | 35.316 |
| Meunier and Shenoi [19] | Analytical-HSDT | 16.38 | 28.69 | 30.01 | 38.86 |
| Nayak et al. [20] | FEM-Q9-HSDT | 16.09 | 28.1 | 29.2 | 37.76 |
| Nayak et al. [20] | FEM-Q4-HSDT | 16.43 | 30.18 | 31.96 | 40.94 |

Following Fig. 5 shows the first 8 frequencies from present ABAQUS.

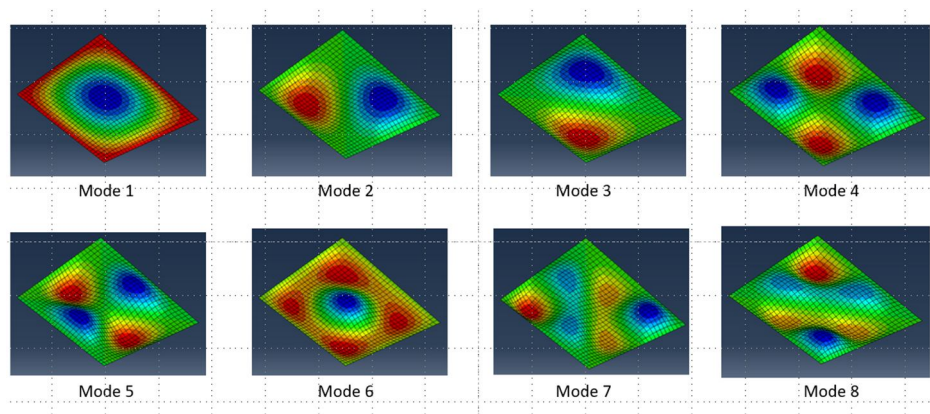


Fig. 5. First 8 frequencies modes from present ABAQUS

III. CONCLUSION

This paper presents an investigation into the modal responses of a flat rectangular sandwich plate with a honeycomb core using finite element method (FEM) software. The accuracy and reliability of the proposed model are validated through comparisons with existing literature. The study focuses on using aluminum honeycomb as the core material and glass fiber reinforced composite for the top and bottom layers of the plate to analyze the modal responses. Various boundary conditions are considered to examine the free vibration behavior. Modal analysis of composite sandwich structures is conducted, and the obtained results are compared with those available in the literature. The sandwich structure is solved using the ABAQUS software through a finite element approach. The findings reveal that the frequencies obtained from the FEM software align well with the results reported in other literature, affirming the accuracy of the current model.

IV. ACKNOWLEDGEMENTS

This work is supported by ISRO-Savitribai Phule Pune University (SPPU), Pune research grant project No 188. Author is thankful to ISRO-SPPU cell.

REFERENCES

- [1] Ahmed KM. Free vibration of curved sandwich beams by the method of finite elements. *J Sound Vib.* 1971;18(1):61–74.
- [2] Goyal SK, Sinha PK. A note on free vibration of sandwich beams with central mass. *J Sound Vib.* 1976;49(3):437–441.
- [3] Shu D. Vibration of sandwich beams with double delaminations. *Compos Sci Technol.* 1995;54(1):101–109.
- [4] Frostig Y, Baruch M. Free vibrations of sandwich beams with a transversely flexible core: a high order approach. *J Sound Vib.* 1994;176(2):195–208.
- [5] Sakiyama T, Matsuda H, Morita C. Free vibration analysis of sandwich beams with elastic or viscoelastic core by applying the discrete Green function. *J Sound Vib.* 1996;191(2):189–206.
- [6] Nicholson JW. Free vibration of stiffened rectangular plates using Green's functions and integral equations. 1986; 24(3): 485.
- [7] Rao MK, Desai YM, Chitnis MR. Free vibrations of laminated beams using mixed theory. *Composite Structures.* 2001;52(2):149–160.
- [8] Kapuria S, Dumir PC, Jain NK. Assessment of zigzag theory for static loading, buckling, free and forced response of composite and sandwich beams. *Composite Structures.* 2004;64(3):317–327.
- [9] Bhangale RK, Ganesan N. Thermoelastic buckling and vibration behavior of a functionally graded sandwich beam with constrained viscoelastic core. *Journal of Sound and Vibration.* 2006;295(1):294–316.
- [10] Wu Z, Chen W. An assessment of several displacement-based theories for the vibration and stability analysis of laminated composite and sandwich beams. *Composite Structures.* 2008;84(4):337–349.
- [11] Kulkarni S, Kapuria S. Free vibration analysis of composite and sandwich plates using an improved discrete Kirchhoff quadrilateral element based on third-order zigzag theory. *Computational Mechanics.* 2008;42(6):803–824.
- [12] Wang C, Ang K, Yang L, Watanabe E. Free vibration of skew sandwich plates with laminated facings. *Journal of Sound and Vibration.* 2000;235(2):317–340.
- [13] Chakrabarti A, Sheikh AH. Vibration of laminate-faced sandwich plate by a new refined element. *Journal of Aerospace Engineering.* 2004;17(3):123–134.
- [14] Belarbi MO, Tati A, Ounis H, Khechai A. On the Free Vibration Analysis of Laminated Composite and Sandwich Plates: A Layerwise Finite Element Formulation. *Latin American Journal of Solids and Structures.* December 2017.
- [15] Burlayenko V, Altenbach H, Sadowski T. An evaluation of displacement-based finite element models used for free vibration analysis of homogeneous and composite plates. *Journal of Sound and Vibration.* 2015;358:152–175.
- [16] Rahmani O, Khalili S, Malekzadeh K. Free vibration response of composite sandwich cylindrical shell with flexible core. *Composite Structures.* 2010;92(5):1269–1281.
- [17] Malekzadeh K, Sayyidmousavi A. Free Vibration Analysis of Sandwich Plates with A Uniformly Distributed Attached Mass, Flexible Core and Different Boundary Conditions. *Journal of Sandwich Structures and Materials.* 2010;12(6):709–732.



- [18] Jam JE, Eftari B, Taghavian SH. A new improved high-order theory for analysis of free vibration of sandwich panels. *Polymer Composites*. 2010;31(12):2042-2048.
- [19] Meunier M, Sheno R. Free vibration analysis of composite sandwich plates. *Proceedings of the Institution of Mechanical Engineers, Part C: Journal of Mechanical Engineering Science*. 1999;213(7):715-727.
- [20] Nayak A, Moy S, Sheno R. Free vibration analysis of composite sandwich plates based on Reddy's higher-order theory. *Composites Part B: Engineering*. 2002;33(7):505-519.
- [21] ABAQUS. *Abaqus Analysis User's Manual*: 2022.



10.22214/IJRASET



45.98



IMPACT FACTOR:
7.129



IMPACT FACTOR:
7.429



INTERNATIONAL JOURNAL FOR RESEARCH

IN APPLIED SCIENCE & ENGINEERING TECHNOLOGY

Call : 08813907089  (24*7 Support on Whatsapp)