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Strength Improvement of Black Cotton Soil by using Different Materials

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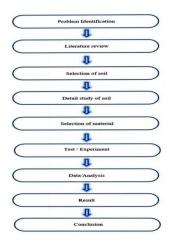
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Abstract: This study examines the effect of geotextiles, plastic rings, plastic shavings and fibres on soil California bearing capacity (CBR). The experiment evaluates the effectiveness of these additions to improve the bearing capacity and reduce the sedimentation of the soil samples. Geotextiles are introduced to improve soil compaction and reduce lateral movement. Plastic rings and chips are added to create voids and improve drainage, which can reduce water content and improve strength. Polypropylene Fibres were added to study their effect on soil reinforcement and stress distribution improvement. CBR tests are performed on soil samples with hand without these additives to quantify the improvement in strength and deformation properties. The results of this study should provide valuable information on the potential benefits of using geotextiles, plastic rings, plastic chips and polypropylene fibres in pavement construction to improve soil CBR of soils in pavement applications Keywords: CBR Test, Geotextiles, plastic chips, plastic rings, polypropylene fibres,

I. INTRODUCTION

- 1) Black Cotton Soil: Black cotton soil, also known as regur soil, is a type of soil found in the Deccan Plateau region of India. It is characterized by its brown-black color, high clay content, and high shrink-swell properties.
- 2) CBR Test: CBR (California Bearing Ratio) testing is performed primarily to provide information for pavement design. It was first developed by the California State Highway Department. It is a penetration or subsidence test under load, mainly used to evaluate the base strength of roads, pavements and foundations..
- 3) Geotextiles: Geotextiles are essentially strong fabrics used in construction projects. They are the most Versatile type of geosynthetic material, with a wide range of applications. Due to the variety of Geotextiles available, choosing the right one for a specific project is crucial.
- 4) Polypropylene Fibres: Experiments were conducted using different Percentages of polypropylene fibres mixed with compacted soil samples. The tests measured the Soil's strength, bearing capacity, and swelling behaviour. While the detailed results aren't provided. This research suggests that fibre reinforcement has promise for improving problematic soils.
- 5) Plastic bottle: The project involves mixing the soil with various percentages of these plastic strips. Tests like Compaction and California Bearing Ratio (CBR) will then be conducted to analyse the impact on Soil properties

II. METHODOLOGY





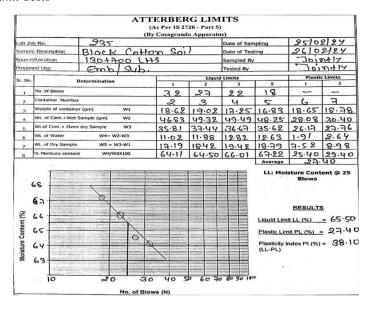
III. TESTS AND RESULTS

To determine the properties of soil tests we conducted on soil are:

1) Free Swell Index

			WELL IN				
Lab Jot	No.:	235	235		: 251	25/02/24	
Sample Description: Black Coffon		Soil Date of Testing:		26/02/24			
Source/Location:		180+700 LHS	Sampled By:	Jointy			
Proposo	od Use:	Embon kment	Subground	Tested By:	700	mais	
Sr. No		Determination	, ,	Test-1	Test-2	Average	
1		cirnen in Graduated Cylinder illed Water after 24 hrs = (ml)	Vd	20	21	/	
2		imen in Graduated Cylinder osene after 24 hrs = (ml)	Vk	13	13		
3	Difference of Vo	olume in Water & Kerosene (ml)	Vd-Vk	7	.8	/	
4	Free Swelling In	idex, [%] =	[(Vd-Vk)/Vk] x 100	53.85	61.54	57.70	

2) Liquid Limit And Plastic Limit Tests



3) Grain Size Analysis

		GRAIN SIZE			
Lab Job No.	235	[AS per 13 27.	Date of Sampling	25/02/2	У
Sample Description	Black Ce	Hon Soil	Date of Testing	26/02/2	4
Source/Location	130+700		Sampled By	Toindly	
Proposed Use	Embl Sut		Tested By	Jointly	
Wt. of Sample (gm)	1000				
IS Sieve Size (mm)	Weight Retained (gm)	Cumulative Weight Retained (gm)	Cumulative Perentage Retained (%)	Cumulative Percentage Passing (%)	Remarks
100					
75					
. 19	0	0	0	100	
4.75	16	16	1.6	98.4	
2.0	9	25	2.50	97.5	
0.425	47	72	7.2	92.8	
0.075	53	125	12.5	87.5	
Pan					
DESCRIPTION C	F PARTICLE	SIEVE SIZE (mm)		PERCENT	TAGE
	Coarse .	75 - 19		-	
Gravel	Fine	19 - 4.75		1.60	1.60
	Coarse	4.75 - 2.00		0.90	
Sand	Medium	2.00 - 0.425		4.7	10.9
	Fine	0.425 - 0.075		5.3	
Silt & Clay		Passing through 0.07	5		87.5



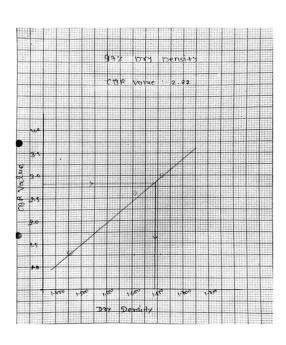


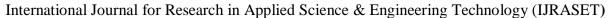
4) Modified Proctor Test

	N	IODIFIE		TOR COL	MPACTIO	ON TEST		
Lab Job No.	23	_	Asic		Date of Sample	ing	25/02	124
Sample Description	Black	Confly	on So	;)	Date of Testing		26/02	
Source/Location	100 +2	100 Lt	18	, ,	Sampled By			2417
Proposed Use	Empl		12		Tested By			ハナリケ
	00110	_				h		
Mould No % of Water	-	Wt. of N	Mould, W ₁ (gm)	399	227.	Volume of mou	26%	T
Wt. of Wet Sample +		f>	18%	20%		247		
		(gm)	2486	5979	6058	5956	5831	
Wt. of Wet Sample, V		(gm)	1996	1989	2068	1966	1881	
Wet density, Y _p = W ₃	N	(gm/cc)	1.796	1.989	2.068	1.966	1.881	
Container No.			56	57	58	59	60	
Wt. of container,W ₅		(gm)	40.30	46.4	43.57	48.25	48.15	
Wt. of wet soil + cont	. We	(gm)	146.99	161.89	166.61	170.47	171.92	
Wt. of dry soil + cont.	.w,	(gm)	130.60	142.80	145.14	146.5	146.3	
Wt. of water, W _s =(W _t	-W ₇)	(gm)	16.39	19.09	21.47	23.97	25.62	
Wt. of dry soil, W _e =(V	V-W5)	(gm)	90.30	96.40	99.57	98.25	98.15	
Moisture content w =1	W ₈ /W ₉ × 100	(%)	18.15	19.80	22.00	24.40	26.10	
Dry density Y = Yb/(1+ w/100)	(gm/cc)	1.520	1.660	1.695	1.580	1.492	
Sy Dy Dessity (grifter)			ζ)		D		Test Results MDD (gm/cc) = OMC (%) =	1.69 <i>5</i> 9 22.00
1.400		Co Mois	22 ture Conten	24		26	*	

- 5) California Bearing Ratio Test
- a) CBR Test With Noramal Black Soil

Laboratory Job		235			Sampling :	25/021	24	
Location/Soun	ce	130+10	30+ 100 LHS		by:	Teintly		
Type of Mater	ial :		Black	oil Tested by	y:	Jointly		
Proposed use:		The strict	United A	Date of Casting				
Period of Soal	kinn	00 11-		Date of T	Testing:	3/03/12		
	ONTENT AND UNIT W	96 Ho	us	position .		-1.03		
HOLSTONE CO	ONIENI AND ONLI W		Id No. a)4	Mos	Ad No. of 5	Mo	uld No. 46	
No. of layers		5	one. and	5	-	5	5	
No. of blows per	laver		- 5	30	30	65	65	
CONDITION OF		Before soaking	After soaking	Before soaking	After soaking	Before soaking	After soaking	
Wt. of Mould, W		6995	6995	7960	7960	6885	6885	
	ple + Mould, W ₂ (gm)		11122	123.90	12424	11441	11493	
	ple, W ₁ =(W ₂ -W ₁) (gm)	11072		4430	4464	4556	4608	
Volume of moule		4077	U127	350	4464	07.5%	2250	
	a, v (cc) = W ₃ /V (gm/cc)	2250	2250		1,984	2,025	2.048	
MOISTURE DET		1.812	After soaking	J. 969 Before soaking	After soaking	Before soaking	After soaking	
	EXPLINATION	Before soaking			Atter soaking	-	6	
Container No.	M (am)		110 0-	48.71	46,31	46.29	48.87	
Wt. of container		47.31	48, 90		350.34		312.33	
	ple +Cont., W ₆ (gm)	341.12	345.55	293,71	292,31	298.29	261.87	
	ple + Cont., W ₇ (gm)	489.31	287.90		(8,03	55.16	50.46	
Wt. of water, Wg=(Wg-Wy) (gm)		21.84	57.65	54.64		22.10	213.0	
	ple, W ₅ =(W ₇ -W ₅) (gm)	242.0	24.12	2420	246.0	21,69	23.69	
	t W = W ₈ /W ₅ (%) = Y ₆ /(1+ w/100) (gm/cc	1.492	1.418	1.610	1,605	1.661	1,656	
Proving rin		Provi	ng Ring Calibrat		Ad No. of 5	Mo	uld No. 46.	
Sr.No.	Penetration (mm)	Proving ring Reading		Proving ring Reading	Corrected load (Kg)	Proving ring Reading	Corrected load (Kg	
1	0.5	1	3.35	3	10.05	3	10.01	
2	1.0	2	6.70	5	16.75	6	20.10	
3	1.5	3	10.05	7	23.45	8	26,80	
4								
	2.0	4	13.40	8	26,80	10	33.50	
5	2.5	5	16.75	10	33.50	12	40.20	
6	2.5	5	20.10	10	33.50	12	40.20	
6	2.5 3.0 4.0	5	20.10	10	36.85 46.90	13	40.20 u3.55 53.60	
6 7 8	2.5 3.0 4.0 5.0	6 7 8	20.10	10	33.50 36.85 46.90 53.60	12 13 16 18	40.20 03.55 53.60 60.40	
6 7 8 9	2.5 3.0 4.0 5.0 7.5	6 7 8 10	20.10 23.45 26.80 33.50	10 11 14 16	33.60	12 13 16 18 21	40.20 03.55 53.60 60.30	
6 7 8 9	2.5 3.0 4.0 5.0 7.5	6 7 8	20.10 23.45 26.80 33.50 36.85	10 11 14 16 19	33.50 36.85 46.90 53.60	12 13 16 18 21	40.20 43.55 53.60 60.40 70.35 73.70	
6 7 8 9 10	2.5 3.0 4.0 5.0 7.5 10.0	6 7 8 10	20.10 23.45 26.80 33.50	10 11 14 16	33.60	12 13 16 18 21	40.20 03.55 53.60 60.30	
6 7 8 9	2.5 3.0 4.0 5.0 7.5 10.0 12.5 LATION Corrected Unit Load in Inform graph)	6 -7 -8 -10 -11 -11	20.10 23.45 26.80 33.50 36.85	10 11 14 16 19 20 22 Note:	33.50 36.85 46.90 53.60 63.65 67.0 73.7	12 13 16 18 21 21	40.20 43.55 53.60 60.30 70.35 73.40	
6 7 8 9 10 11 CBR CALCU	2.5 3.0 4.0 5.0 7.5 10.0 12.5 LATION Corrected Unit Load in significant graph. 5.0 mem.	6 -7 -8 -10 -11 -11 -11 -11 -11 -12 -13 -13 -13 -13 -13 -13 -13 -13 -13 -13	20.10 23.45 26.80 33.50 36.85	0 1 1 1 1 1 1 1 1 1 1	33.50 36.85 46.90 53.60 63.60 67.0 73.7 and vs penetration rected load/standa	12 13 16 18 21 21 21 21 21 21 21 21 21 21 21 21 21	10.20 U3.55 53.60 60.40 70.35 73.40	
6 7 8 9 10 11 CBR CALCU Mould No.	2.5 3.0 4.0 5.0 7.5 10.0 12.5 LATION Corrected Unit Load in significant graph (2.5 mm) 5.0 mm 1.7 (2.5 & 6.0	6 -7 -8 -10 -11 -11 -25 mm 5.0 mm -1.32 1-34	16:15 20:10 23:45 26:80 33:50 36:85	10 11 14 16 19 20 22 Note:	33.50 36.85 46.90 53.60 63.65 67.0 73.7 and vs penetration rected load/standa sit load :	12 16 18 21 21 21 23 attached rd losd) x 100 9 2.5mm Penetra	40.20 U3.55 53.60 60.40 70.35 73.70 77.05	
6 7 8 9 10 11 CBR CALCU	2.5 3.0 4.0 5.0 7.5 10.0 12.5 LATION Corrected Unit Load in significant graph. 5.0 mem.	6 -1 8 10 11 11 11 25 mm 5.0 mm 1 1.22 1.32 2.45 2.45	16:15 20:10 23:45 26:80 33:50 36:85	O I I I I I I I I I	33,50 36,85 46.90 53,60 67.0 73,7 and vs penetration rected load/standa it load	12 13 16 18 21 21 21 21 21 21 21 21 21 21 21 21 21	40.20 U3.55 S3.60 60.40 70.35 73.70 77.05 tion = 1370 Kg	

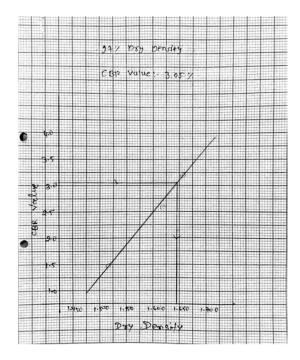






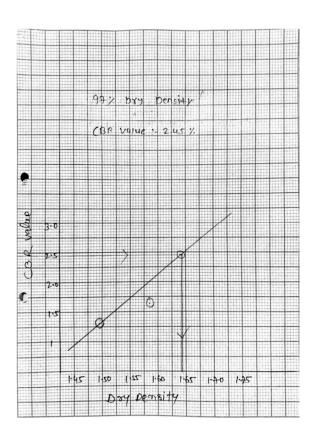
b) CBR Test with Geotextile

Laborator	Job No.	00-	[IS 2720 (PA	A BEARING F	931		T
Location/S		235			Sampling :	25/02/24	
Type of M		130 +	-100 LHS Sampl		by: Jointly		
		with	textile	Tested b	y: -	Jointly	
Proposed			,	Date of C		41031124	
Period of 5		96 1	lowes	Date of 1		1031'2	1
MOISTUR	E CONTENT AND UNIT	WEIGHT OF TEST	SAMPLES	Posts or .	· constant	51051 2	
No. of lavers			ould No. 25	Mou	ld No. 26	Mou	16 No. 34
		5	5	5	-		5
No. of blows		10	ID	3.0	30	65	65
CONDITION		Before soaking	After soaking	Before soaking	After soaking	Before soaking	After soaking
Wt. of Mould		6741	6741	6880	6880	7070	7070
	iample + Mould, W ₂ (gm)	10913	11016	11246	11403	11613	11620
	ample, W ₃ =(W ₂ -W ₁) (gm)	4172	4275	4466	4523	4543	4550
Volume of m		2250	2250	2250	2250	2250	2250
Wet Density,	$Y_b = W_y/V (gm/cc)$	1.854	1,900	1.985	2.010	2.109	2.022
	ETERMINATION	Before soaking	After soaking	Before soaking	After soaking	Before soaking	After soaking
Container No		5	6	22	26	25	22
Wt. of contain		45.30	46.80	43.61	48.70	48.71	46.23
Wt. of Wet S	ample +Cont., W ₄ (gm)	292.56	292.06	310.58	353.95	307.01	303.10
Wt. of Dry St	emple + Cont., W, (gm)	248.86	242.65	262.81	294.55	261.25	254.12
	W _s =(W _s -W _s) (gm)	42.70	49.41	47.71	59.40	45.76	46.67
Wt. of Dry Sample, W _s =(W ₂ -W ₃) (gm)		20356	195.85	216.56	245.85	212.54	210.89
Moisture cont	rent W = W ₈ /W ₄ (%)	21.47	25.23	22.03	24.16	21,53	22.13
Dry Density Y	e = Y _b /(1+ w/100) (gm/cc	1.534	1.517	1.627	1.619	1.661	1.656
	ETRATION TEST DATA :		1.311				
Proving ri			ing Ring Calibrat	ion Factor :			
Proving ri	ng No.:	Prov	ing Ring Calibrat	tion Factor :	1 No. 26	Moul	d No. 34
		Prov	uld No. 25			Moul Proving ring Reading	id No. 34 Corrected load (Kg)
Sr.No.	Penetration (mm)	Prov	Corrected load (Kg)	Moule	Corrected load (Kg)		Corrected load (Kg)
Sr.No.	Penetration (mm) 0.5 1.0	Prov	Corrected lead (Kg)	Moule	Corrected load (Kg)	Proving ring Reading	Corrected load (Kg)
Sr.No.	Penetration (mm) 0.5 1.0 1.5	Prov Mo Proving ring Reading	Corrected load (Kg)	Moule Proving ring Reading	[D.05]	Proving ring Reading	Corrected load (Kg)
Sr.No.	Penetration (mm) 0.5 1.0 1.5 2.0	Prov Mo Proving ring Reading 1 3	Corrected load (Kg)	Mouk Proving ring Reading	1D.05 13.45	Proving ring Reading	10.05 20.10 30.15
Sr.No.	Penetration (mm) 0.5 1.0 1.5 2.0 2.5	Prov Mo Proving ring Reading 1 3	20 No. 25 Corrected lead (Kg) 3.35 10.05 13.40	Proving ring Reading	[D.05]	Proving ring Reading 3 6 9	10.05 20.10
Sr.No. 1 2 3 4 5 6	ng No.: Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0	Proving ring Reading 1 3 41 5	25 (xg) (xg) (xg) (xg) (xg) (xg) (xg) (xg)	Proving ring Reading	10.05 13.40 16.75 23.45 30.15	Proving ring Reading 3 6 9	10.05 20.10 30.15 36.65
Sr.No. 1 2 3 4 5 6 7	ng No.: Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0	Proving ring Reading	Jo 05 13.40 16.75	Proving ring Reading	10.05 13.40 16.75 23.45	Proving ring Reading 3 6 9 11	10.05 20.10 30.15 36.85 43.53
Proving ri Sr.No. 1 2 3 4 5 6 7	ng No.: Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0	Proving ring Reading 1 3 41 6 7 8	10.05 13.40 16.15 20.1 23.45	Proving ring Reading	Corrected laad (Kg) 10.05 13.40 16.75 23.45 30.15	Proving ring Reading 3 6 9 11 13	Corrected load (Kg) 10:05 20:10 30:15 36:85 43.53
Sr.No. 1 2 3 4 5 6 7 8	ng No.: Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 7.5	Proving ring Reading 1 3 4 5 6 7 8 9 10	July No. 25 Corrected lead (Kg) 3.35 10.05 13.40 16.15 20.1 23.45	Proving ring Reading 1	Corrected load (Kg) 10.05 13.40 16.75 23.45 23.45 36.85 40.2	Proving ring Reading 3 6 9 11 13 ! LL	Corrected load (Kg 10.05 20.10 30.15 36.85 43.5 46.90 53.60
Proving ri Sr.No. 1 2 3 4 5 6 7 8 9 10	ng No.: Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 7.5	Proving ring Reading 1 3 4 5 6 7 8 9 10	dd No. 25 Corrected tod (Kg) 3.35 10.05 13.40 16.75 20.1 23.45 26.8 30.15 34.5	Moule Proving ring Reading	Corrected laad (Kg) 10.05 13.40 16.75 23.45 30.15 36.85 40.2 50.25 63.66	Proving ring Reading 3 6 9 11 13 14 16 18 21	Corrected load (Kg) 10:05 20:10 30:15 36:85 43:56 46:90 53:60 60:30
Sr.No. 1 2 3 4 5 6 7 8 9 10	Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 7.5 10.0 12.5	Proving ring Reading 1 3 4 5 6 7 8 9 10	dd No. 25 Corrected tod (4) 3, 35 10, 05 13, 40 16, 75 20, 1 23, 45 26, 8 30, 15 34,5	Moult Proving ring Reading 3 1 1 1 1 1 1 1 1 1	Corrected laud (Kg) 10.05 13.40 16.75 23.45 30.15 36.85 40.2 60.25	Proving ring Reading 3 6 9 11 13 14 16 18 21	Corrected load (Kg) 20-10 30-15 36-85 43-53 46-90 60-30
Sr.No. 1 2 3 4 5 6 7 8 9 10	Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 1.0 1.2.5 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	Proving ring Reading 1 3 41 5 6 7 8 9 10 11	dd No. 25 Corrected tod (Kg) 3.35 10.05 13.40 16.75 20.1 23.45 26.8 30.15 34.5	Moult Proving ring Reading T T T T T T T T T T T T T	Corrected bad (Kg) 10.05 13.40 16.75 23.415 36.85 40.2 50.25 63.65 67.0	Proving ring Reading 3 6 9 11 13 14 18 21 23 24	10:05 20:10 30:15 36:85 43.5 46:90 53.60 60:30
Sr.No. 1 2 3 4 5 6 7 8 9 10	Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 7.5 10.0 11.5 10.0 11.5 10.0 11.5 10.0 11.5 Corrected the Load in self-ten geap)	Proving ring Reading 1 3 4 5 6 7 8 9 10	dd No. 25 Cometed kad (kg) 3, 25 10, 05 13, 40 16, 75 20, 1 23, 45 26, 8 3, 0, 15 3, 25 3, 25 3	Moult Proving ring Reading In The Proving ring Reading In The In	Corrected bad (Kg) 1D . 0 S 13 . 4 D 16 . 15 23 . 4 S 36 . 8 S 40 . 2 50 . 2 S 63 . 6 S 67 . 0 d vs penetration at	Proving ring Reading 3 6 9 11 13 14 16 18 21 23 24 ttached	10:05 20:10 30:15 36:85 43.5 46:90 53.60 60:30
Sr.No. 1 2 3 4 5 6 7 8 9 10 11 CCBR CALCU	Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 10.0 12.5 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10	Proving ring Reading 1 3 4 5 5 6 6 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	dd No. 25 Corrected tod (Kg) 3.35 10.05 13.40 16.75 20.1 23.45 26.8 30.15 34.5	Moult Proving ring Reading 3 1 1 1 1 1 1 1 1 1	Corrected load (Kg) 10.05 13.90 16.75 23.95 36.85 40.2 50.25 63.65 67.0 d vs penetration at teted load/standard	Proving ring Reading 3 6 9 11 13 14 16 18 21 23 24 ttached	10:05 20:10 30:15 36:85 43.5 46:90 53.60 60:30
Sr.No. 1 2 3 4 5 6 7 8 9 10 11 CCBR CALCU	Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 10.0 12.5 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10	Proving ring Reading 1 3 41 5 6 7 1 8 9 10 11	Add No. 25 Corrected lead (Kg) 3.35 10.05 13.440 16.75 20.1 23.45 26.8 30.15 36.85 36.85	Moult Proving ring Reading In The Proving ring Reading In The In	Corrected load (Kg) 10.05 13.40 16.75 23.45 30.45 36.65 40.2 50.25 60.3 64.0 divs penetration at ted load/standard	Proving ring Reading 3 6 9 11 13 14 16 18 21 23 24 ttached	Do O
Sr.No. 1 2 3 4 5 6 7 8 9 10 11 CBR CALCU	Penetration (mm)	Proving ring Reading 1 3 4 5 5 6 7 7 6 9 1 1 1 1 1 1 1 1 1	dd No. 25 Cometed kad (kg) 3, 25 10, 05 13, 40 16, 75 20, 1 23, 45 26, 8 3, 0, 15 3, 25 3, 25 3	Moult Proving ring Reading 3 1 1 1 1 1 1 1 1 1	Corrected lad (Kg) 1D . 05 13 . 4D 16 . T5 23 . 45 36 . 85 40 . 2 50 . 25 67 . 0 d vs penetration at teted load/standard load: 10 . 05	Proving ring Reading 3 6 9 11 13 14 16 18 21 23 24 tached load) x 100 80 25 Smm Penetratis 5.0 mm Penetratis	DD - O Corrected load (fg) DD - O Corrected load (fg)
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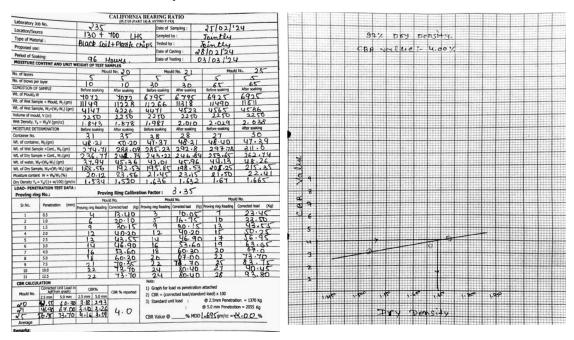


c) CBR Test with Fibre

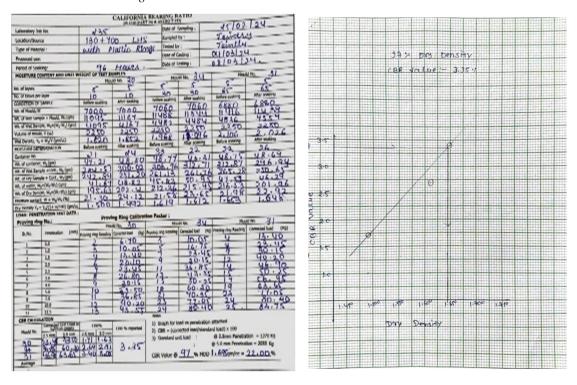
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110421010	CONTENT AND ONLY		d No. 32	Moul	6 No. 3	Moule	1 No. 35	
No. of layers		5	5	5	1	5		
No. of blows per layer		10	10	30	30	- 28	After soaking	
CONDITION		Before soaking	After soaking	Before soaking	After soaking	Before soaking	200F	
Wt. of Mould,		6959	6959	19 10	7910	7005	115 13	
	ample + Mould, W ₂ (gm)	11097	11164	12217	12334	11531	4568	
	ample, W ₃ =(W ₂ -W ₁) (gm)	4138	4205	4364	4424	4516	2250	
Volume of mo		2250	2250	2250	7250	2250	2.030	
	Y ₂ = W ₃ V (gm/cc)	1.839	1.869	1.941	After soaking	2.00 Y Before soaking	After soaking	
	ETERMINATION	Before scaking	After soaking	Before soaking		2 C)	38	
Container No.		28	44	26 UR. 87	33 48.69	47.37	u7.37	
Wt. of contain		U4-80	48.15	334.15	317.36	968.67	352.28	
	mple +Cont., W _s (gm) mple + Cont., W _r (gm)	330.34	316.85	282.49	365.27	310.62	293.88	
	mple + Cont., W ₇ (gm) W ₈ =(W ₈ -W ₇) (gm)	279.94	263.2	51.16	52,09	58.05	18.40	
	mple, W _s =(W _r -W _s) (gm)	230.14	215.05	234.12	216.58	263.25	246.5	
	ent W = W _a /W ₄ (%)	21.90	24.95	21.85	04.05	22.05	23.69	
	= Y _b /(1+ w/100) (gm/cc		1, 496	1.593	1.785	1.644	1.64	
	ETRATION TEST DATA:		11419		1.100			
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Proving ri	ng No.:	Provi	ng Ring Calibrat Id No. 32		Ad No. 3.1	Mo	M No. 35	
		Provi	ld No. 32			Mor Proving ring Reading	Corrected load (Kg	
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Proving ri Sr.No. 1 2 3 4 5 6 7 8	Peretation (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 7.5	Proving Moul Moul Proving ring Reading	10.05 10.05 10.05 13.45 10.05 13.40 16.75 20.10 23.45 26.80 30.15 33.50	Proving ring Reading 1 3 4 5 6 7 9 10	Corrected base (Ng 3, 3, 5 10, 0, 5 13, 40 16, 15 20, 10 23, 45 30, 15 43, 50 43, 73	Proving ring Reading T Reading 10 11 14 19 18 19	Corrected load (19 10.05 16.15 23.45 26.80 33.55 46.90 50.25 60.30	
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Proving ri Sr.No. 1 2 3 4 5 6 7 8 9 10 11 CBR CALCU	Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 7.5 10.0 12.5 10.0 10.	Proving Proving Reading III	3.35 A. 70 10. 05 13. 45 20.10 23. 45 20. 10 23. 45 20. 10 23. 45 20. 10 23. 45 20. 10 23. 45 20. 10 20.	Proving ring Reading 1 3 4 5 6 7 9 10 13 14 Note: 1) Graph for Is	Corrected toal (%) 3, 2, 5 10, 0, 5 13, 4, 10 16, 7, 5 20, 10 23, 4, 5 30, 15 43, 7, 5 46, 9, 0 46, 9,	Proving ring Reading 3 1 1 8 10 11 11 11 11 11 12 18 19 20 n attached	Corrected tool (%) 10 · OS 16 · TS 23 · Y 26 · 80 33 · SS 46 · 90 50 · 26 63 · 65	
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d) CBR Test Black with Plastic Bottle Chips



e) CBR test with Plastic Bottle Ring



IV. RESULT ANALYSIS

A. Free Swell Index Result Analysis

Here's an analysis of the Free Swell Index test results:

- Free Swell Index: The Free Swell Index of the soil sample is 57.70%. A free swell index greater than 30% indicates a high swelling potential
- Interpretation:



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The high Free Swell Index suggests that the soil sample has a high potential to swell when saturated with water. This can cause problems with foundations and other structures built on this soil, as the swelling soil can cause cracking and movement.

B. Liquid Limit Result Analysis

Atterberg Limits

- Liquid Limit (LL): The Liquid Limit is 65.50%. This is the moisture content at which the soil changes from a liquid state to a plastic state
- Plastic Limit (PL): The Plastic Limit is 27.40%. This is the moisture content at which the Soil changes from a plastic state to a brittle state.
- Plasticity Index (PI): The Plasticity Index (PI) is calculated as the difference between the
- Liquid Limit (LL) and the Plastic Limit (PL). In this case, the PI is 65.50% 27.40% = 38.10%. A higher PI value indicates a more plastic soil.

C. Grain Size Analysis Result Analysis

Here's an analysis of the grain size distribution:

- Gravel(75-19 mm): 1.60% of the sample falls into the gravel size category.
- Sand (4.75-0.075 mm): 10.9% of the sample falls into the sand size category. This can be Further broken down into: Coarse sand (4.75-2.00 mm): 0.90%, Medium sand (2.00-0.425 mm): 4.7% &Fine sand (0.425-0.075 mm): 5.3%
- Silt and Clay (particles smaller than 0.075 mm): 87.5% of the sample falls into the silt And clay size category.

D. Modified Proctor Test Result Analysis

- Dry Density (g/cm³): The data sheet shows the Dry Density for five different moisture Content values. The Dry Density increases as the moisture content increases up to a certain Point, and then starts to decrease. The highest Dry Density is 1.695 g/cm³ at a moisture Content of 22.00%, which is considered the Maximum Dry Density (MDD).
- Optimum Moisture Content (OMC): The Optimum Moisture Content (OMC) is the Moisture content at which the Maximum Dry Density (MDD) is achieved. In this case, the OMC is 22.00%

E. Cbr Test Result Analysis Noramal Black Soil

The report shows the results of the CBR test for three soil samples (moulds 24, 25, and 26).

The CBR values for the three samples are:

- Mould 24: 16.75 corrected load at 2.5 mm penetration, 26.80 corrected load at 5.0 mm Penetration
- Mould 25: 33.50 corrected load at 2.5 mm penetration, 53.60 corrected load at 5.0mm penetration
- Mould 26: 40.20 corrected load at 2.5 mm penetration, 60.30 corrected load at 5.0 mm penetration
- The CBR values are all relatively low, which indicates that the soils are weak and may not be Suitable for use in pavements without additional treatment. The report does not specify what The soils will be used for, but the CBR values are typically used to design the thickness of Pavement layers.
- CBR VALUE IS :- 2.82%

F. CBR Test Result Analysis Black Soil + Geotextile

The report shows the results of the CBR test for three soil samples (moulds, 25, 26, and 34). The CBR values for the three samples are:

- Penetration Mould 25: 20.10corrected load at 2.5 mm penetration, 30.15 corrected Load at 5.0 mm
- Penetration Mould 26: 30.15 corrected load at 2.5 mmpenetratioloa50.25 corrected Load at 5.0 mm
- Penetration Mould 34: 43.55 corrected load at 2.5 mm penetration, 60.30 corrected Load at 5.0 mm
- Penetration The CBR values are all relatively low, which indicates that the soils are weak and

May not be suitable for use in pavements without additional treatment. The report does not

Specify what the soils will be used for, but the CBR values are typically used to design the

Thickness of Pavement layers

CBR VALUE IS: - 3.05%



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G. CBR Test Result Analysis Black Soil + Fiber

The report shows the results of the CBR test for three soil samples (moulds, 33, 31, and 35). The CBR values for the three samples are:

- Penetration Mould 33: 16.75 corrected load at 2.5 mm penetration, 26.80 corrected load at 5.0 mm
- Penetration Mould 31: 20.10 corrected load at 2.5 mm penetration, 33.50 corrected load at 5.0 mm
- Penetration Mould 35: 33.50 corrected load at 2.5 mm penetration, 50.25 corrected load at 5.0 mm
- Penetration The CBR values are all relatively low, which indicates that the soils are weak and may not be suitable for use in pavements without additional treatment. The report does not specify what the soils will be used for, but the CBR values are typically used to design the thickness of Pavement layers
- CBR VALUE IS: 2.40%

H. CBR Test Result Analysis Black Soil + Plastic Chips

The report shows the results of the CBR test for three soil samples (moulds, 20, 21, and 25). The CBR values for the three samples are:

- Penetration Mould 20: 43.55 corrected load at 2.5 mm penetration, 60.30 corrected load at 5.0 mm
- Penetration Mould 21: 46.90 corrected load at 2.5 mm penetration, 67.00 corrected load at 5.0 mm
- Penetration Mould 25: 56.95 corrected load at 2.5 mm penetration, 73.70 corrected load at 5.0 mm
- Penetration The CBR values are all relatively low, which indicates that the soils are weak and may not be suitable for use in pavements without additional treatment. The report does not specify what the soils will be used for, but the CBR values are typically used to design the thickness of Pavement layers
- CBR VALUE IS: 4.00 %

CBR Test Result Analysis Black Soil + Plastic Rings

The report shows the results of the CBR test for three soil samples (moulds, 30, 34, and 31). The CBR values for the three samples are:

- Penetration Mould 25: 23.45 corrected load at 2.5 mm penetration, 33.50 corrected load at 5.0 mm
- Penetration Mould 26: 36.85 corrected load at 2.5 mm penetration, 60.30 corrected load at 5.0 min
- Penetration Mould 34: 46.90 corrected load at 2.5 mm penetration, 63.65 corrected load at 5.0 mm
- Penetration The CBR values are all relatively low, which indicates that the soils are weak and May not be suitable for use in pavements without additional treatment. The report does not Specify what the soils will be used for, but the CBR values are typically used to design the Thickness of Pavement layers
- **CBR VALUE IS :- 3.35 %**

V. **CONCLUSION**

Black cotton soil, despite its weakness, can be boosted for embankments using plastic waste. Crushed plastic or strips mixed in the soil improve its strength and reduce swelling. This creates a Stronger, more stable material for building embankments. However, this method doesn't address the core issue for subgrades – shrinkage and swelling with Moisture changes. Embankments sit above ground with less water exposure, but subgrades are Directly impacted by seasonal variations. The treated soil might still experience these drastic volume Changes, causing cracks and compromising the structural integrity of the road or building above.

In short, plastic waste strengthens black cotton soil for embankments, but it doesn't address the Moisture sensitivity that plagues subgrades.

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