



INTERNATIONAL JOURNAL FOR RESEARCH

IN APPLIED SCIENCE & ENGINEERING TECHNOLOGY

Volume: 12 Issue: VI Month of publication: June 2024

DOI: https://doi.org/10.22214/ijraset.2024.63259

www.ijraset.com

Call: © 08813907089 E-mail ID: ijraset@gmail.com



ISSN: 2321-9653; IC Value: 45.98; SJ Impact Factor: 7.538

Volume 12 Issue VI June 2024- Available at www.ijraset.com

Strength Improvement of Black Cotton Soil by using Different Materials

Mr. Alpesh K Sankhat¹, Shivani Joshi², Vijay Baraiya³

¹Professor, Department of Civil Engineering, GMB Polytechnic-Rajula (GTU), India

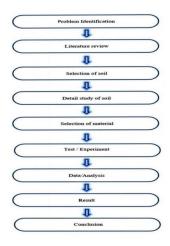
^{2, 3}Department of Civil Engineering, Gujarat Technological University

Abstract: This study examines the effect of geotextiles, plastic rings, plastic shavings and fibres on soil California bearing capacity (CBR). The experiment evaluates the effectiveness of these additions to improve the bearing capacity and reduce the sedimentation of the soil samples. Geotextiles are introduced to improve soil compaction and reduce lateral movement. Plastic rings and chips are added to create voids and improve drainage, which can reduce water content and improve strength. Polypropylene Fibres were added to study their effect on soil reinforcement and stress distribution improvement. CBR tests are performed on soil samples with hand without these additives to quantify the improvement in strength and deformation properties. The results of this study should provide valuable information on the potential benefits of using geotextiles, plastic rings, plastic chips and polypropylene fibres in pavement construction to improve soil CBR of soils in pavement applications Keywords: CBR Test, Geotextiles, plastic chips, plastic rings, polypropylene fibres,

I. INTRODUCTION

- 1) Black Cotton Soil: Black cotton soil, also known as regur soil, is a type of soil found in the Deccan Plateau region of India. It is characterized by its brown-black color, high clay content, and high shrink-swell properties.
- 2) CBR Test: CBR (California Bearing Ratio) testing is performed primarily to provide information for pavement design. It was first developed by the California State Highway Department. It is a penetration or subsidence test under load, mainly used to evaluate the base strength of roads, pavements and foundations..
- 3) Geotextiles: Geotextiles are essentially strong fabrics used in construction projects. They are the most Versatile type of geosynthetic material, with a wide range of applications. Due to the variety of Geotextiles available, choosing the right one for a specific project is crucial.
- 4) Polypropylene Fibres: Experiments were conducted using different Percentages of polypropylene fibres mixed with compacted soil samples. The tests measured the Soil's strength, bearing capacity, and swelling behaviour. While the detailed results aren't provided. This research suggests that fibre reinforcement has promise for improving problematic soils.
- 5) Plastic bottle: The project involves mixing the soil with various percentages of these plastic strips. Tests like Compaction and California Bearing Ratio (CBR) will then be conducted to analyse the impact on Soil properties

II. METHODOLOGY





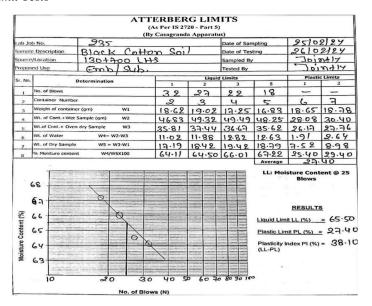
III. TESTS AND RESULTS

To determine the properties of soil tests we conducted on soil are:

1) Free Swell Index

			SWELL IN			* *	
Lab Jot	No.:	235	Date of Sampling:		25/02/24		
Sample	Sample Description: Black Co Hom		Soil	Date of Testing:	261	102124	
Source/Location:		130+700 LHS	Sampled By:	Jointy			
Proposo	od Use:	Embon kment	Subarca	Tested By:		かもっと	
Sr. No		Determination	, ,	Test-1	Test-2	Average	
1	Volume of Specimen in Graduated Cylinder Containing Distilled Water after 24 hrs = (ml)		Vd	20	21	/	
2		imen in Graduated Cylinder osene after 24 hrs = (ml)	Vk	13	13		
3	Difference of Vo	olume in Water & Kerosene (ml)	Vd-Vk	7	.8	/	
4	Free Swelling In		[(Vd-Vk)/Vk] x 100	53.85	61.54	57.70	

2) Liquid Limit And Plastic Limit Tests



3) Grain Size Analysis

10		GRAIN SIZE			
Lab Job No.	235	[AS per 13 27.	Date of Sampling	25/02/2	У
Sample Description	Black Ce	Hon Soil	Date of Testing	26/02/2	4
Source/Location	130+700		Sampled By	Toindly	
Proposed Use	Embl Sut		Tested By	Jointly	
Wt. of Sample (gm)		2000			
IS Sieve Size (mm)	Weight Retained (gm)	Cumulative Weight Retained (gm)	Cumulative Perentage Retained (%)	Cumulative Percentage Passing (%)	Remarks
100					
75					
. 19	0	0	0	100	
4.75	16	16	1.6	98.4	
2.0	9	25	2.50	97.5	
0.425	47	72	7.2	92.8	1
0.075	53	125	12.5	87.5	
Pan					
DESCRIPTION C	F PARTICLE	SIEVE SIZE (mm)		PERCENT	TAGE
	Coarse .	75 - 19		-	
Gravel -	Fine	19 - 4.75		1.60	1.60
	Coarse	4.75 - 2.00		0.90	
Sand	Medium	2.00 - 0.425		4.7	10.9
	Fine	0.425 - 0.075	the state of the s	5.3	
Silt & Clay		Passing through 0.07	5		89.5



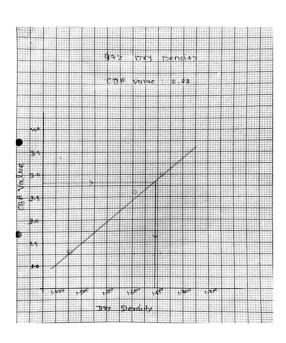


4) Modified Proctor Test

	N	IODIFIE		TOR COL	MPACTIO	ON TEST		
Lab Job No.	23	_	Asic		Date of Sample	ing	25/02	124
Sample Description	Black	Conth	on So	;)	Date of Testing		26/02	
Source/Location	100 +2	100 L	18	, ,	Sampled By			2417
Proposed Use	Empl		12		Tested By			ハナリケ
	0010	_				h		
Mould No % of Water		Wt. of N	Mould, W ₁ (gm)	399	227.	Volume of mou	26%	T
		()	18%	20%		247		
Wt. of Wet Sample +		(gm)	2486	5979	6058	5956	5831	
Wt. of Wet Sample, V		(gm)	1996	1989	2068	1966	1881	
Wet density, Y _p = W ₃	N	(gm/cc)	1.796	1.989	2.068	1.966	1.881	
Container No.			56	57	58	59	60	
Wt. of container,Ws		(gm)	40.30	46.4	43.57	48.25	48.15	
Wt. of wet soil + cont	. We	(gm)	146.99	161.89	166.61	170.47	171.92	
Wt. of dry soil + cont.	.w,	(gm)	130.60	142.80	145.14	146.5	146.3	
Wt. of water, W _s =(W _s	-W ₇)	(gm)	16.39	19.09	21.47	23.97	25.62	
Wt. of dry soil, W _e =(V	V-W,	(gm)	90.30	96.40	99.57	98.25	98.15	
Moisture content w =\	W ₈ /W ₉ x 100	(%)	18.15	19.80	22.00	24.40	26.10	
Dry density Y = Yb'(1+ w/100)	(gm/cc)	1.520	1.660	1.695	1.580	1.492	
or Dy Dessity (grifce)		<u> </u>	ζ)		D		Test Results MDD (gm/cc) = OMC (%) =	1.69 <i>5</i> 9 22.00
1-400	(0	Co Mois	22 ture Conten	24		2 C	*	

- 5) California Bearing Ratio Test
- a) CBR Test With Noramal Black Soil

Laboratory Job	b No.	235		Date of 1	Sampling :	25/021	24
Location/Soun	ce	130+ 10		Sampled		Teintly	
Type of Mater	ial :		Black	nil Tested b	y:	Jointly	
Proposed use:		- House			Casting:	281021'24	
Period of Soal		06.11		Date of T		3/03/2	
	ung: ONTENT AND UNIT W	96 Hou	us	loate or 1		310312	
HOISTURE CO	DATENT AND UNIT W		d No. a)4	Mos	id No. of 5	Mo	uld No. 46
No. of layers		5	0 NO. 074	-	-	5	5_
No. of blows per	layer	10	10	30	30	65	65
CONDITION OF		Before soaking	After soaking	Before soaking	After soaking	Before soaking	After soaking
Wt. of Mould, W		6995	6995	7960	7960	6885	6885
Wt. of Wet Same	ple + Mould, W ₂ (gm)		11122	123.90	12424	11441	11493
	ple, W ₃ =(W ₂ -W ₁) (gm)	11072 1170U	LID	4430	4464	4556	4608
Volume of mouk		2250	2350	350	4700	07.50	J250
	= W _x /V (gm/cc)	1.812	1.834	1.969	1.964	2,025	2.048
MOISTURE DET		Before soaking	After soaking	Before soaking	After soaking	Before soaking	After soaking
Container No.	DOMESTICAL STREET	better stearing	Arter soaking) L	4		6
Wt. of container	W.(om)	44.31	48, 90	48,71	46,31	U6.29	48.87
	ple +Cont., W ₄ (gm)	241.15	345.55	348 - 35	350.34	353.45	312.33
	ple + Cont., W ₄ (gm) ple + Cont., W ₇ (gm)	289,31	287.90	293,71	292,31	298.29	261.87
	pe + core, w ₇ (gm) (₄ =(W ₄ -W ₇) (gm)	201.84	57.65	54.64	68.03	55.16	10.46
	ple, W ₄ =(W ₇ -W ₃) (gm)		2 39 . 0	24.64	246.12	377.0	213.0
	pre, W ₁ =(W ₇ -W ₅) (gm)	21.42	2U.12	22.30	23.59	21,69	23.69
	x W = W _b /W ₅ (%) = Y _b /(1+ w/100) (gm/cc		1,418	1.610	1,605	1.661	1.15
Proving rin		Moul		Mou	ld No. 42 5		id No. 4/6
		Proving ring Reading		Proving ring Reading		Proving ring Reading	
1	0.5	1	3,35	3	10.0	3	10.01
2	1.0	2	6.70	- 5	16.75	6	20.10
3	2.0	3	13.40	8	23.05	8	33.50
5	2.5	2	13.40	10	33.50	12	40.20
6	3.0	6	20.10	11	36,85	13	40.20
7	4.0	9	23.45	Iu	46.90	16	53.60
	5.0	8	26.80	16	53,60	18	60.40
8		10	33.50	19	63.65	21	70:35
9	7.5						43.40
	10.0	11	36.85	20	67.0		
9 10 11	10.0		36.85	20	73.7	23	77.05
9	10.0 12.5	11	36.85		73,7	23	77.05
9 10 11	10.0 12.5 ILATION Corrected Unit Load in kgf(from graph) 2.5 mm 5.0 mm	CBR% 2.5 mm 5.0 mm	36.85	Note: 1) Graph for k	d vs penetration	attached	77.05
9 10 11 CBR CALCU	10.0 12.5 LATION Corrected Unit Load in lightnon graph 2.5 mm 5.0 mm	CBR% 2.5 mm 5.0 mm	36 · 85 36 · 85	Note: 1) Graph for k	73, 7 ad vs penetration ected load/standa	attached	
9 10 11 CBR CALCU	10.0 12.5 LATION Corrected Unit Load in lightnon graph 2.5 mm 5.0 mm	CBR% 2.5 mm 5.0 mm	36 · 85 36 · 85	Note: 1) Graph for lo 2) CBR = (con	73, T ad vs penetration ected load/standa it load :	attached rd load) x 100	tion = 1370 Kg
9 10 11 CBR CALCU Mould No.	10.0 12.5 ILATION Corrected Unit Load in kgf(from graph) 2.5 mm 5.0 mm	CBR% 2.5 mm 5.0 mm	36.85	Note: 1) Graph for lo 2) CBR = (con 3) Standard ur	73,7 ad vs penetration ected load/standa it load :	attached rd load) x 100 @ 2.5mm Penetra	tion = 1370 Kg

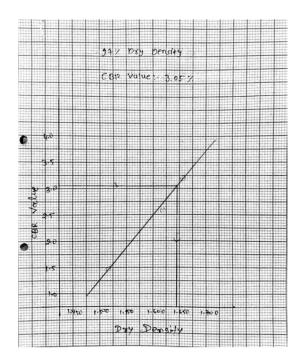






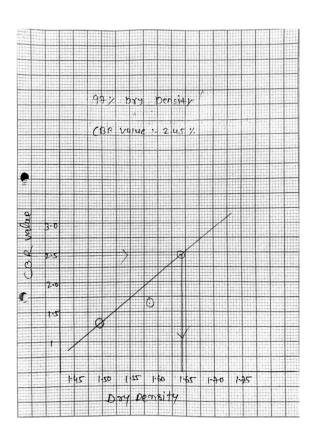
b) CBR Test with Geotextile

	Job No.	1 00	[IS 2720 (PA	A BEARING F	931		1
Location/S		235			Sampling :	25/02	124
		130 +	30 + 100 LHS		by:	Jointly	
Type of Ma		huth	textile	Tested b		Tointly	
Proposed u	ise:	1	- ALA ULL	Date of 6	e of Casting: UIO31'24		
Period of S	icaking:	96 H		Date of 1		1031,50	
MOISTURE	CONTENT AND UNIT	WEIGHT OF TEST	lowes	Date or	esting:	1031 20	
			uld No. 25	Mov	ld No. 26	Mou	M No. 34
No. of layers		5	5	5	5	7	-
No. of blows		10	10	3.0	30	65	65
CONDITION		Before soaking	After soaking	Before soaking	After soaking	Before soaking	After soaking
Wt. of Mould,		6741	6741	6880	6880	7070	1070
	ample + Mould, W ₂ (gm)	10913	11016	11246	11403	11613	11620
	ample, W ₃ =(W ₂ -W ₁) (gm)	4172	4275	4466	4523	4543	4550
Volume of mo		2250	2250	2250	2250	2250	2250
	$Y_b = W_y/V (gm/cc)$	1.854	1,900	1.985	2.010	2.109	2.022
MOISTURE D	ETERMINATION	Before soaking	After soaking	Before soaking	After soaking	Before soaking	After soaking
Container No.		5	6	22	26	25	22
Wt. of contain	ner, W ₃ (gm)	45.30	46.80	43.61	48.70	48.71	46.23
Wt. of Wet Sa	ample +Cont., W ₄ (gm)	292.56	292.06	310.58	353.95	307.01	303.10
Wt. of Dry Sa	mple + Cont., W, (gm)	248.86	242.65	262.81	294.55	261.25	257.12
Wt. of water,	W _s =(W _s -W _s) (gm)	42.70	49.41	41.71	59.40	45.76	46.67
Wt. of Dry Sar	mple, W _s =(W ₇ -W ₅) (gm)	20356	195.85	216.56	245.85	212,54	210.89
	ent W = W ₈ /W ₄ (%)	21.47	25.23	22.03	24.16	21,53	22.13
Dry Density Y,	= Y _b /(1+ w/100) (gm/cc	1.536	1.517	1.627	1.619	1.661	1.656
	TRATION TEST DATA :	1.326	1.011	11.021			1.0.0
LOAD- PENE							
Proving ri			ng Ring Calibrat	ion Factor :			
Proving ri	ng No.:	Provi	ld No. 25	ion Factor : Moul	1 No. 26	Moul	d No. 34
LOAD- PENE	ng No.:	Provi	ld No. 25			Moul Proving ring Reading	
Proving ri Sr.No.	ng No.:	Provi	ld No. 25 Corrected load (Kg)	Moul	Corrected load (Kg)		Corrected load (Kg)
Proving ri Sr.No.	Penetration (mm) 0.5 1.0	Proving ring Reading	Id No. 25 Corrected load (Kg) 3.35	Moul	Corrected load (Kg)	Proving ring Reading	Corrected load (Kg)
Proving ri Sr.No.	Penetration (mm) 0.5 1.0 1.5	Proving ring Reading	Id No. 25 Corrected load (Kg) 3 - 35	Moul Proving ring Reading	[D.05]	Proving ring Reading	Corrected load (Kg)
Proving ri Sr.No.	Penetration (mm) 0.5 1.0 1.5 2.0	Proving ring Reading 1 3	Id No. 25 Corrected load (Kg) 3.35	Proving ring Reading	Corrected load (Kg)	Proving ring Reading	10.05 20.10
Proving ri Sr.No.	Penetration (mm) 0.5 1.0 1.5 2.0 2.5	Proving Fround Reading 1 3 4	1d No. 25 Corrected load (Kg) 3.35 10.05 13.40	Proving ring Reading	10.05 13.40 16.75 23.45	Proving ring Reading 3 6 9	10.05 20.10 30.15 36.65
Proving ri Sr.No.	Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0	Proving ring Reading 1 3 4 6	10.05 13.40 16.75	Proving ring Reading	10.05 13.45 16.75	Proving ring Reading 3 6 9	10.05 20.10 30.15
Proving ri Sr.No. 1 2 3 4 5 6	Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0	Proving ring Reading 1 3 41 5 6	dd No. 25 Corrected load (Kg) 3.35 10.05 13.40 16.75 20.1	Moul Proving ring Reading	10.05 13.40 16.75 23.45 30.15	Proving ring Reading 3 6 9 11 1.3	10.05 20.10 30.15 36.85 43.55
Proving ri Sr.No.	Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0	Proving ring Reading 1 3 41 5 6 7	10.05 10.05 13.40 16.75 20.1 23.45 26.8	Mould Proving ring Reading	Corrected load (Kg) 1D.05 13.40 16.75 23.45 30.15 36.85 40.2	Proving ring Reading 3 6 9 11 13 14 16	10.0 C 20.1 D 30.1 C 36.6 S 43.5 46.90
Proving ri Sr.No.	Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 7.5	Proving ring Reading 1 3 4 5 6 7 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1	Ad No. 25 Corrected lead (Kg) 3.35 10.05 13.40 16.75 20.1 23.45 26.8	Mount Proving ring Reading	Corrected laud (Kg) 10.05 13.40 16.75 23.45 30.15 36.85 40.2 60.25	Proving ring Reading 3 6 9 11 13 ! Li	20-10 20-10 30-15 36-85 43-5 46-90 3-60-30
LOAD-PENE Proving ri Sr.No. 1 2 3 4 5 6 7 8 9	Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 7.5 10.0	Proving ring Reading 1 3 4 5 6 7 8 9 10 11	16 No. 25 Corrected lead (1/g) 3 · 35 10 · 05 13 · 40 16 · 75 20 · 1 23 · 45 26 · 8 30 · 15 34 · 5 36 · 8	Moul Proving ring Reading	Corrected laad (Kg) 10.05 13.40 16.75 23.45 30.15 36.85 40.2 50.25 63.66	7 3 6 9 11 13 14 16 18 18 18 18 18 18 18 18 18 18 18 18 18	10:05 20:10 30:15 36:85 43.5 46:90 53:60 60:30
DAD- PENE Proving ri Sr.No. 1 2 3 4 5 6 7 8 9 10 11	Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 7.5 10.0 12.5	Proving ring Reading 1 3 4 5 6 7 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1	dd No. 25 (corrected lead (Vig) 3.35 10.05 13.40 16.75 20.1 23.45 26.8 30.15	Moule Proving ring Reading	Corrected laud (Kg) 10.05 13.40 16.75 23.45 30.15 36.85 40.2 60.25	Proving ring Reading 3 6 9 11 13 14 16 18 21	10.05 20.10 30.15 36.85 43.5 46.90 53.60 60.30
LOAD- PENE Proving ri Sr.No. 1 2 3 4 5 6 7 8 9 10	Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 1.7.5 1.0 1.2 2.5 1.0 1.0 1.2 2.5 1.0 1.0 1.2 2.5 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	Proving ring Reading 1 3 4 5 6 7 1 8 9 10 11	16 No. 25 Corrected lead (1/g) 3 · 35 10 · 05 13 · 40 16 · 75 20 · 1 23 · 45 26 · 8 30 · 15 34 · 5 36 · 8	Moul Proving ring Reading T	Corrected bad (Kg) 1D . 0.5 13 . 4.10 16 . 15 23 . 4.5 36 . 8.5 40 . 2.5 63 . 65 67 . 0	Proving ring Reading 3 6 9 11 13 14 16 18 21 23	10:05 20:10 30:15 36:85 43.5 46:90 53:60 60:30
DAD- PENE Proving ri Sr.No. 1 2 3 4 5 6 7 8 9 10 11	Penetration (mm) 0.5 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 7.5 10.0 11.5 Corrected Unit Load in Selffen regen)	Proving ring Reading 1 3 4 5 6 7 8 9 10 11	da No. 25 Corrected load (1/4) 3.35 10.05 13.40 16.75 20.1 23.45 26.8 30.15 34.85 36.85	Moule Proving ring Reading	Corrected bad (Kg) 1D . 0 S 13 . 4 D 16 . 15 23 . 4 S 36 . 8 S 40 . 2 50 . 2 S 63 . 6 S 67 . 0 d vs penetration at	Proving ring Reading 3 6 9 11 13 14 16 18 21 23 24 tached	Corrected load (Kg 10.05 20.10 30.15 36.85 43.5 46.90 53.60 60.30
DAD- PENE Proving ri Sr.No. 1 2 3 4 5 6 7 8 9 10 11 CBR CALCU	Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 1.0 1.5 5.0 1.0 1.5 5.0 1.5 5.0 1.5 5.0 1.5 5.0 1.5 5.0 1.5 5.0 1.5 5.0 1.5 5.0 1.5 5.0 1.5 5.0 5.0	Proving ring Reading 1 3 4 5 5 6 6 7 1 1 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	16 No. 25 Corrected lead (1/g) 3 · 35 10 · 05 13 · 40 16 · 75 20 · 1 23 · 45 26 · 8 30 · 15 34 · 5 36 · 8	Moult Proving ring Reading	Corrected load (Kg) 10.05 13.40 16.75 23.45 30.45 36.65 40.2 50.25 60.3 64.0 divs penetration at ted load/standard	7 Proving ring Reading 3	Do 0 Corrected load (% Do 0 Correct
LOAD-PENE Proving ri Sr.No. 1 2 3 4 5 6 6 7 7 8 9 10 11 11 CBR CALCUI	Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 7.5 10.0 12.5 MATION Convected Unit Load in 15((mm sign)) 2.5 mm	Proving ring Reading 1	48 No. 25 (corrected load (%) 3, 35 (10, 05 13, 440 16, 15 20, 1 23, 445 26, 8 30, 15 36, 85	Moule Proving ring Reading	Corrected load (Kg) 10.05 13.40 16.75 23.45 30.45 36.65 40.2 50.25 60.3 64.0 divs penetration at ted load/standard	Proving ring Reading 3 6 9 11 13 14 16 18 21 23 24 tached	Do 0 Corrected load (% Do 0 Correct
LOAD-PENE Proving ri	Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 1.2.5 1.0 1.2.5 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	Proving ring Reading 1	da No. 25 Corrected load (1/4) 3.35 10.05 13.40 16.75 20.1 23.45 26.8 30.15 34.85 36.85	Moult Proving ring Reading	Corrected lad (Kg) 1D . 05 13 . 4D 16 . T5 23 . 45 36 . 85 40 . 2 50 . 25 67 . 0 d vs penetration at teted load/standard load: 10 . 05	Proving ring Reading 3 6 q 11 1.3 1.4 1.6 1.8 2.1 2.3 2.4 tached load) x 100 9 2.5mm Penetratis 5.0 mm Penetratis	Corrected load (Kg D
LOAD-PENE Proving ris Sr.No. 1 2 3 4 5 6 7 8 9 10 11 CER CALCU	Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 1.2.5 1.0 1.2.5 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	Proving ring Reading 1	48 No. 25 (corrected load (%) 3, 35 (10, 05 13, 440 16, 15 20, 1 23, 445 26, 8 30, 15 36, 85	Moult Proving ring Reading	Corrected lad (Kg) 1D . 05 13 . 4D 16 . T5 23 . 45 36 . 85 40 . 2 50 . 25 67 . 0 d vs penetration at teted load/standard load: 10 . 05	7 Proving ring Reading 3 6 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Corrected load (Kg D

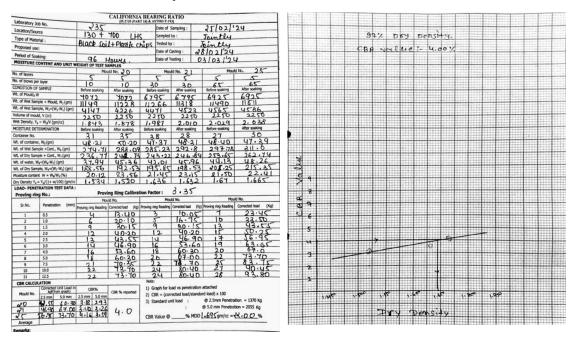


c) CBR Test with Fibre

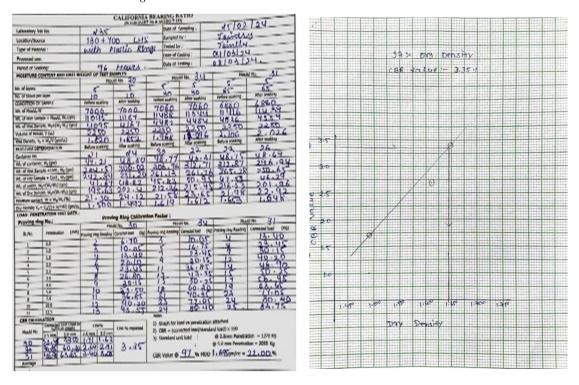
			CALIFORNIA	BEARING RA				
Laboratory	Job No.	235	[IX 1720 (FAR)	Date of S	ampling: 0	5 1021	124	
Location/S	ource	130+700 LH		IC Sampled h			Jointly	
Type of M	***			Tested by	-	Jointl	· ·	
		with	there	SAME OF BRIDE S	Date of Cesting :		1/24	
Proposed i				CONTRACTOR DE CONTRACTOR DE C	N. P. OF SHARPS AND REAL PROPERTY.	08/03 1/24 12 03 1/24		
Period of S			lows	Date of Te	esting:	12 1 031	14	
MOISTURE	CONTENT AND UNIT V		MPLES	Moul	1 6 .on	Mouk	1 No. 35	
No. of layers		-	Id No. 32	5	1	-	-	
No. of blows	per layer	10	10	30	30	65	65	
CONDITION		Before scaking	After sooking	Before soaking	After soaking	Before soaking	After soaking	
Wt. of Mould	W	6959	6959	1910	7910	7005	100F	
Wt. of Wet S	ample + Mould, W ₂ (gm)	11097	11164	12211	1233 4	11521	115 13	
	ample, W ₃ =(W ₂ -W ₃) (gm)	4138	4205	4367	4424	4516	4568	
Volume of mo		2250	2250	2250	2250	2250	2250	
	Y _b = W _b V (qm/cc)	1.839	1,869	1.941	1.966	2.004	2.030	
	ETERMINATION	Before soaking	After soaking	Before soaking	After soaking	Before soaking	After soaking	
Container No.		28	44	26	33	39	38	
Wt. of contain	ner, W. (om)	49.8D	48.15	U8.87	48.69	47.37	47.37	
	ample +Cont., W ₄ (gm)	330.34	316.85	334.15	317.36	968.67	352,28	
	mple + Cont., W _r (gm)	279.94	263.2	282.99	265. 27	310.62	293.88	
	W _g =(W _s -W _r) (gm)	50.40	53.65	51.16	52,09	58.05	58.40	
		230.14	215.05	234.12	216.58	263.25	246.5	
Wt. of Dry Sample, W ₅ =(W ₇ -W ₅) (gm)								
Moisture corb	ont W = W./W. (%)	21.90	201.95	28.10	04.05	22.05	23.69	
Dry Density Y	tent $W = W_0/W_0(%)$ $V_d = Y_0/(1 + w/100) (gm/cc)$		1,496	21.85	1.586	1.644	1.64	
Dry Density Y LOAD- PEN Proving ri	e = Y _b /(1+ w/100) (gm/cc ETRATION TEST DATA : ing No.:	Provi	1. 496 ng Ring Calibrat Id No. 22	ion Factor :	1.586 Al No. 31	1.644 Ma	1.64 MHO. 35	
Dry Density Y. LOAD- PENI Proving ri Sr.No.	e = Y _s /(1+ w/100) (gm/cc ETRATION TEST DATA : ing No.: Penetration (mm)	Provi	ng Ring Calibrat Id No. 32 Corrected load (Kg)	ion Factor :	Ad No. 3.1 Corrected load (Kg)	1,644	ald No. 3.5 Corrected load (Kg)	
Dry Densty Y. LOAD- PENI Proving ri St.No.	e = Y _n /(1+ w/100) (gm/cc ETRATION TEST DATA : ing No.: Penetration (mm)	Proving ring Reading	ng Ring Calibrat Id No. 32 Corrected bad (Kg)	ion Factor :	1.586 Ad No. 3.1 Corrected load (Kg) 3.35	Mox Proving ring Reading	Ad No. 3.5 Corrected load (Kg)	
Dry Density Y. LOAD- PENI Proving ri Sr.No. 1 2	_c = Y _s /(1+ w/100) (gm/cc ETRATION TEST DATA : ing No.: Penetration (mm) 0.5 1.0	Proving ring Reading	ng Ring Calibrat Id No. 32 Corrected bad (Kg) 3.35 6.40	don Factor : Mox Proving ring Reading	1.585 Ad No. 3.1 Corrected bad (Kg) 3.35 10.05	1.644 Ma	10. 05 16. 15	
Dry Densby Y. LOAD- PENI Proving ri Sr.No. 1 2 3	e Y ₀ /(1+ w/100) (gm/cc ETRATION TEST DATA : ing No.: Penetration (mm) 0.5 1.0	Proving ring Reading	1. 49 G ng Ring Calibrat 1d No. 32 Corrected bad (Kg) 3.35 A. 40 10.05	don Factor : Hos Proving ring Reading	1.5% ad No. 3.1 Corrected load (Ng) 3.35 10.05 13,40	Mox Proving ring Reading	dd No. 3.5 Corrected load (Kg)	
Dry Densby Y. LOAD- PENI Proving ri Sr.No. 1 2 3 4	e = Y ₀ /(1+ w/100) (gm/cc ETRATION TEST DATA : ing No.: Penetration (mm) 0.5 1.0 1.5 2.0	Proving ring Reading 1 2 3 4	1, 49 6 Ing Ring Calibrat Id No. 32 Corrected bad (Kg) 3, 35 A, 40 10, 05 13, 40	ion Factor : Mox Proving ring Reading	d No. 3 Corrected load (Vg) 3.35 10.05 13,40 16.75	Mox Proving ring Reading	ad No. 3.5 Corrected load (%) 10. 05 16. 15 23. 45	
Dry Density Y. LOAD- PENI Proving ri Sr.No. 1 2 3 4 5	t = Y ₀ /(1+ w/100) (gm/ct ETRATION TEST DATA : ing No.: Penetration (mm) 0.5 1.0 1.5 2.0 2.5	Proving ring Reading	1, 49 6 ng Ring Calibrat ld No. 32 Corrected bad (6g) 3, 35 A 7 0 10, 05 13, 40	Jon Factor : Mox Proving ring Reading U G	1.5% ad No. 3.1 Corrected load (%) 10.05 13.40 16.75 20.10	Moving ring Reading 3	J • 6 4 J • 6 4 Corrected load (Kg) 10 • 05 16 • 15 23 • 4 5 26 • 80 33 • 50	
Dry Density Y. LOAD- PENI Proving ri \$r.No. 1 2 3 4 5 6	, = Y ₃ /(1+ w/100) (gm/cc ETRATION TEST DATA : ing No.: Penetration (mm) 0.5 1.0 1.5 2.5 3.0	Provide the Provid	1, 49 6 ng Ring Calibrat Id No. 32 Corrected bad (6g) 3, 35 A. 10 10, 05 13, 40 16, 75 20, 10	don Factor : Mou Proving ring Reading U G G G G T	1.5% ad No. 3.1 Corrected load (Vg) 10.05 13,40 16.75 20.10 23.45	Proving ring Reading	1.64 at No. 35 corrected load (Vg 10.05 16.15 26.80 33.55 36.85	
Dry Density Y. LOAD- PENI Proving ri Sr.No. 1 2 3 4 5 6 7	e * Y_f/(1+ w/100) (gm/cc ETRATION TEST DATA : ing No.: Penebation (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0	Provide the Provid	1, 496 Ing Ring Calibrat Id No. 32 Corrected load (I/g) 3, 35 A. 10 10, 05 13, 40 16, 15 20,10 23, 45	ion Factor : Mox. Proving ring Reading 1 3 4 6 7	1.586 id No. 3.1 Corrected load (Ng) 3.35 10.05 13,40 16.75 20.10 23.45 30.15	Moving ring Reading 3	10.05 10.05 16.15 23.45 26.80 33.65 46.90	
Dry Density Y. LOAD- PENI Proving ri Sr.No. 1 2 3 4 5 6 7 8	e * Y ₂ /(1+ w/100) (gm/cc ETRATION TEST DATA : ing No.: Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0	Provide Mou. Proving ring Reading 1 2 3 4 5 6 7 8	1, 49 6 Ing Ring Calibrat Id No. 32 Corrected load (Kg) 3, 35 A-70 10, 05 13, 40 16, 75 20,10 23, 45 26,80	ion Factor : Mox. Proving ring Reading 1 3 4 6 7	1.586 Id No. 3.1 Corrected toal (fg) 3.3.5 10.05 13,40 16.75 20.10 23.45 30.15 33.50	Proving ring Reading An I I	10.05 10.05 10.05 10.15 26.80 33.05 36.85 46.85	
Dry Densty Y. LOAD- PENII Proving ri Sr.No. 1 2 3 4 5 6 7 8 9	e " Y ₂ /(1+ w/100) (gm/cc ETRATION TEST DATA : ing No.: Penebation (mm) 0.5 1.0 2.0 2.5 3.0 4.0 7.5	Proving ing Reading J S G G G G G G G G G G G G	1, 496 Ing Ring Calibrat Idd No. 32. Corrected bad (6g) 3, 35 4, 40 10, 05 13, 40 16, 45 20, 10 23, 45 20, 10 23, 45 20, 10 23, 45 20, 10 23, 45	Jon Factor: Mou. Proving ring Reading J G G T G G J G G G G G G G G G G G G G	1.586 ad No. 3.1 Corrected load (Vg) 3.3.5 10.05 13,40 16.75 20.10 23.45 33.50 43.75	Proving ring Reading And Proving ring Reading To The Proving ring Reading To The Proving ring Reading	10.05 10.05 10.05 16.15 23.45 36.85 46.90 50.90 60.30	
Dry Densty Y. LOAD- PENIT Proving ri Sr.No. 1 2 3 4 5 6 7 8 9 10	e * Y ₂ /(1+ w/100) (gm/cc ETRATION TEST DATA : Ing No.: Penebation (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 7.5 10.0	Provide the provided of the pr	1, 496 ng Ring Calibrat Mo 3, 32 Corrected load (6) 3, 35 4, 40 10, 05 13, 40 16, 15 20,10 23, 45 26,80 90,15 33,50	don Factor: Mox. Proving ring Reading 1 3 4 5 6 7 9 10	1.586 Ad No. 3.1 Corrected tool (No) 3.25 10.05 13,40 16.15 20.10 23.45 30.15 34.50 44.50	Moo Proving ring Reading 10 11 11 11 11 11 11 11 11 11 11 11 11	1.6 4 10.05 16.75 23.45 26.80 33.65 36.85 46.90 50.30 60.30	
Dry Densty Y. LOAD- PENIT Proving ri Sr.No. 1 2 3 4 5 6 7 8 9 10 11	e * Y,/(1 * w/100) (gmicc ETRATION TEST DATA : ing No.: Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 7.5 1.00 12.5	Proving ing Reading J S G G G G G G G G G G G G	1, 496 Ing Ring Calibrat Idd No. 32. Corrected bad (6g) 3, 35 4, 40 10, 05 13, 40 16, 45 20, 10 23, 45 20, 10 23, 45 20, 10 23, 45 20, 10 23, 45	Jon Factor: Mou. Proving ring Reading J G G T G G J G G G G G G G G G G G G G	1.586 ad No. 3.1 Corrected load (Vg) 3.3.5 10.05 13,40 16.75 20.10 23.45 33.50 43.75	Moo Proving ring Reading 10 11 11 11 11 11 11 11 11 11 11 11 11	10.05 10.05 10.05 16.15 23.45 36.85 46.90 50.90 60.30	
Dry Densty Y. LOAD- PENIT Proving ri Sr.No. 1 2 3 4 5 6 7 8 9 10	, * Y ₂ /(1 * W/100) (gmicc ETRATION TEST DATA : Ing No.: Penebation (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 7.5 100 125 100 11	Provide Provid	1, 496 ng Ring Calibrat Mo 3, 32 Corrected load (6) 3, 35 4, 40 10, 05 13, 40 16, 15 20,10 23, 45 26,80 90,15 33,50	Jon Factor: Mox. Proving ring Reading J G G J J J J J J J J J J	1.5% ad No. 3.1 Consider load (%) 3.3.5 10.05 13.400 16.15 20.10 23.41 30.15 44.50 43.53 46.90 46.90	Proving ring Reading A I O II I I G I G I G I G I G I	1.6 4 10.05 16.75 23.45 26.80 33.65 36.85 46.90 50.30 60.30	
Dry Densty Y. LOAD- PENIT Proving ri Sr.No. 1 2 3 4 5 6 7 8 9 10 11	a * Y_/(1* w/100) (gm/cc: ETRATION TEST DATA : NO :: Penetration (mm) 0.5 1.0 1.5 2.0 2.5 3.0 4.0 5.0 7.5 10.0 12.5 LAULTION Corrected Unit Load in Application graph :	Provide Provid	1, 496 ng Ring Calibrat Mo 3, 32 Corrected load (6) 3, 35 4, 40 10, 05 13, 40 16, 15 20,10 23, 45 26,80 90,15 33,50	ion Factor: Mox. Proving ring Reading Q C G G I I I I I I I I I I I	1.5% At No. 3.1 Corrected tod (kg) 3. 2.5 10.05 13.440 16.15 20.10 23.415 34.50 46.90 46.90 46.90	Proving ring Reading 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.6 4 10.05 16.75 23.45 26.80 33.65 36.85 46.90 50.30 60.30	
Dry Densty Y. LOAD- PENI Proving ri Sr.No. 1 2 3 4 5 6 7 8 9 10 11 CBR CALCU	_ v_J(I + w)100) (gm/cc ETRATION TEST DATA :	Proving Proving (Reading 1)	7, 496 ng Ring Calibration 32 Comment last (6) 3,355 A-40 10,05 13,45 10,05 20,10 23,45 26,80 30,15 33,50	ion Factor: How Proving ring Reading Q Q Q Q Q Q Q Q Q Q Q Q Q	1.5% At No. 3.1 Corrected load (%) 3.3.5 10.05 13.40 16.15 20.10 23.3.50 43.50 43.50 43.50 43.50 43.50 43.50 43.50 43.50 43.50 43.50 43.50	How h	10.05 10.05 10.05 10.05 22.45 26.80 33.75 36.85 46.90 33.65 67.00	
Dry Densty Y. LOAD- PENI Proving ri Sr.No. 1 2 3 4 5 6 7 8 9 10 11 CBR CALCU	- *L/(I+ w/130) (series to Ali A: (in page 4) (in page	Provided Pro	7, 496 ng Ring Calibrate da No. 32 Comment last (fg) 3, 43 10, 05 13, 49 16, 75 20, 10 23, 47 26, 80 9,0, 15 33, 50 CBR % reported	ion Factor: Mox. Proving ring Reading Q C G G I I I I I I I I I I I	1.5% At No. 3.1 Corrected load (%) 3.3.5 10.05 13.40 16.15 20.10 23.3.50 43.50 43.50 43.50 43.50 43.50 43.50 43.50 43.50 43.50 43.50 43.50	How	10. 05 16. 15 10. 05 16. 15 23. 17 26. 80 33. 75 36. 85 46. 90 50. 27 60. 30 63.67 67. 00	
Dry Densty Y. LOAD- PENI Proving ri Sr.No. 1 2 3 4 5 6 7 8 9 10 11 CBR CALCU	_ v_J(I + w)100) (gm/cc ETRATION TEST DATA :	Proving my Reading How Proving my Reading 1 2 3 4 7 6 9 10 10 10 10 11 10 11 11 11	1, 496 Ing Ring Calibration (Ing) Ing Ring Calibration (I S 9 2 don Factor : Hou Proving ring Reading C G G G G G G G G G G G G G G G G G G	1.5% at to. 3.1 Corrected at (vg) 10.05 13.49 16.15 20.10 23.45 30.15 43.50 43.75 46.90	How h	16 10 10 10 10 10 10 10	



d) CBR Test Black with Plastic Bottle Chips



e) CBR test with Plastic Bottle Ring



IV. RESULT ANALYSIS

A. Free Swell Index Result Analysis

Here's an analysis of the Free Swell Index test results:

- Free Swell Index: The Free Swell Index of the soil sample is 57.70%. A free swell index greater than 30% indicates a high swelling potential
- Interpretation:

PADILIDA SELECTION ADDILIDA SELE

International Journal for Research in Applied Science & Engineering Technology (IJRASET)

ISSN: 2321-9653; IC Value: 45.98; SJ Impact Factor: 7.538

Volume 12 Issue VI June 2024- Available at www.ijraset.com

The high Free Swell Index suggests that the soil sample has a high potential to swell when saturated with water. This can cause problems with foundations and other structures built on this soil, as the swelling soil can cause cracking and movement.

B. Liquid Limit Result Analysis

Atterberg Limits

- Liquid Limit (LL): The Liquid Limit is 65.50%. This is the moisture content at which the soil changes from a liquid state to a plastic state
- Plastic Limit (PL): The Plastic Limit is 27.40%. This is the moisture content at which the Soil changes from a plastic state to a brittle state.
- Plasticity Index (PI): The Plasticity Index (PI) is calculated as the difference between the
- Liquid Limit (LL) and the Plastic Limit (PL). In this case, the PI is 65.50% 27.40% = 38.10%. A higher PI value indicates a more plastic soil.

C. Grain Size Analysis Result Analysis

Here's an analysis of the grain size distribution:

- Gravel(75-19 mm): 1.60% of the sample falls into the gravel size category.
- Sand (4.75-0.075 mm): 10.9% of the sample falls into the sand size category. This can be Further broken down into: Coarse sand (4.75-2.00 mm): 0.90%, Medium sand (2.00-0.425 mm): 4.7% &Fine sand (0.425-0.075 mm): 5.3%
- Silt and Clay (particles smaller than 0.075 mm): 87.5% of the sample falls into the silt And clay size category.

D. Modified Proctor Test Result Analysis

- Dry Density (g/cm³): The data sheet shows the Dry Density for five different moisture Content values. The Dry Density increases as the moisture content increases up to a certain Point, and then starts to decrease. The highest Dry Density is 1.695 g/cm³ at a moisture Content of 22.00%, which is considered the Maximum Dry Density (MDD).
- Optimum Moisture Content (OMC): The Optimum Moisture Content (OMC) is the Moisture content at which the Maximum Dry Density (MDD) is achieved. In this case, the OMC is 22.00%

E. Cbr Test Result Analysis Noramal Black Soil

The report shows the results of the CBR test for three soil samples (moulds 24, 25, and 26).

The CBR values for the three samples are:

- Mould 24: 16.75 corrected load at 2.5 mm penetration, 26.80 corrected load at 5.0 mm Penetration
- Mould 25: 33.50 corrected load at 2.5 mm penetration, 53.60 corrected load at 5.0mm penetration
- Mould 26: 40.20 corrected load at 2.5 mm penetration, 60.30 corrected load at 5.0 mm penetration
- The CBR values are all relatively low, which indicates that the soils are weak and may not be Suitable for use in pavements without additional treatment. The report does not specify what The soils will be used for, but the CBR values are typically used to design the thickness of Pavement layers.
- CBR VALUE IS :- 2.82%

F. CBR Test Result Analysis Black Soil + Geotextile

The report shows the results of the CBR test for three soil samples (moulds, 25, 26, and 34). The CBR values for the three samples are:

- Penetration Mould 25: 20.10corrected load at 2.5 mm penetration, 30.15 corrected Load at 5.0 mm
- Penetration Mould 26: 30.15 corrected load at 2.5 mmpenetratioloa50.25 corrected Load at 5.0 mm
- Penetration Mould 34: 43.55 corrected load at 2.5 mm penetration, 60.30 corrected Load at 5.0 mm
- Penetration The CBR values are all relatively low, which indicates that the soils are weak and

May not be suitable for use in pavements without additional treatment. The report does not

Specify what the soils will be used for, but the CBR values are typically used to design the

Thickness of Pavement layers

CBR VALUE IS: - 3.05%



International Journal for Research in Applied Science & Engineering Technology (IJRASET)

ISSN: 2321-9653; IC Value: 45.98; SJ Impact Factor: 7.538

Volume 12 Issue VI June 2024- Available at www.ijraset.com

G. CBR Test Result Analysis Black Soil + Fiber

The report shows the results of the CBR test for three soil samples (moulds, 33, 31, and 35). The CBR values for the three samples are:

- Penetration Mould 33: 16.75 corrected load at 2.5 mm penetration, 26.80 corrected load at 5.0 mm
- Penetration Mould 31: 20.10 corrected load at 2.5 mm penetration, 33.50 corrected load at 5.0 mm
- Penetration Mould 35: 33.50 corrected load at 2.5 mm penetration, 50.25 corrected load at 5.0 mm
- Penetration The CBR values are all relatively low, which indicates that the soils are weak and may not be suitable for use in pavements without additional treatment. The report does not specify what the soils will be used for, but the CBR values are typically used to design the thickness of Pavement layers
- CBR VALUE IS :- 2.40%

H. CBR Test Result Analysis Black Soil + Plastic Chips

The report shows the results of the CBR test for three soil samples (moulds, 20, 21, and 25). The CBR values for the three samples are:

- Penetration Mould 20: 43.55 corrected load at 2.5 mm penetration, 60.30 corrected load at 5.0 mm
- Penetration Mould 21: 46.90 corrected load at 2.5 mm penetration, 67.00 corrected load at 5.0 mm
- Penetration Mould 25: 56.95 corrected load at 2.5 mm penetration, 73.70 corrected load at 5.0 mm
- Penetration The CBR values are all relatively low, which indicates that the soils are weak and may not be suitable for use in pavements without additional treatment. The report does not specify what the soils will be used for, but the CBR values are typically used to design the thickness of Pavement layers
- CBR VALUE IS: 4.00 %

I. CBR Test Result Analysis Black Soil + Plastic Rings

The report shows the results of the CBR test for three soil samples (moulds, 30, 34, and 31). The CBR values for the three samples are:

- Penetration Mould 25: 23.45 corrected load at 2.5 mm penetration, 33.50 corrected load at 5.0 mm
- Penetration Mould 26: 36.85 corrected load at 2.5 mm penetration, 60.30 corrected load at 5.0 min
- Penetration Mould 34: 46.90 corrected load at 2.5 mm penetration, 63.65 corrected load at 5.0 mm
- Penetration The CBR values are all relatively low, which indicates that the soils are weak and May not be suitable for use in pavements without additional treatment. The report does not Specify what the soils will be used for, but the CBR values are typically used to design the Thickness of Pavement layers
- CBR VALUE IS :- 3.35 %

V. CONCLUSION

Black cotton soil, despite its weakness, can be boosted for embankments using plastic waste. Crushed plastic or strips mixed in the soil improve its strength and reduce swelling. This creates a Stronger, more stable material for building embankments. However, this method doesn't address the core issue for subgrades – shrinkage and swelling with Moisture changes. Embankments sit above ground with less water exposure, but subgrades are Directly impacted by seasonal variations. The treated soil might still experience these drastic volume Changes, causing cracks and compromising the structural integrity of the road or building above.

In short, plastic waste strengthens black cotton soil for embankments, but it doesn't address the Moisture sensitivity that plagues subgrades.

REFERENCES

- [1] Tingle, J. S. And Jersey, S. R. (2005). "Cyclic plate load testing of geosynthetic reinforced Unbounded aggregate roads." Transportation Research Record: Journal of the Transportation Research Board, No. 1936, Transportation Research Board of the National Academies, Washington, D.C., pp. 60-69
- [2] MILAD SAGHEBFAR (2014). "PERFORMANCE OF GEOTEXTILE-REINFORCED BASES FOR PAVED ROADS". Transportation Research Record: Journal of the Transportation Research Board. Upload by Milad saghebfar.
- [3] Bayomy, F. M., Al-Shaikh, A. M., and Abduljauwad, S. N. (1996). "Effect of geotextile on Permanent deformation in salt-encrusted subgrade soils." Transportation Research Record: Journal of The Transportation Research Board, No. 1534, Transportation Research Board, Washington, D.C., pp.40-49.
- [4] Bhutta, S. A. (1998). "Mechanistic-empirical pavement design procedure for geosynthetically Stabilized flexible pavements." Ph.D. dissertation, Virginia Tech., Blacksburg, VA



International Journal for Research in Applied Science & Engineering Technology (IJRASET)

ISSN: 2321-9653; IC Value: 45.98; SJ Impact Factor: 7.538 Volume 12 Issue VI June 2024- Available at www.ijraset.com

- [5] Brandon, T. L., Al-Qadi, L. L., Lacina, B. A., and Bhutta, S. A. (2005). "Construction and Instrumentation of geosynthetically stabilized secondary road test sections." Transportation Research Record: Journal of the Transportation Research Board, No. 1534, Transportation Research Board, Washington, D.C. pp. 50-57.
- [6] BHBouacha, N.; Bouguerra, A.; Bouafia, (2023) Improving the Resilience Of the Road Network in Algeria A Comparative Analysis of Flexible, Geosynthetically Reinforced, and Rigid 14426.https://doi.org/10.3390/Su151914426
- [7] Dr. Umesh Sharmaa, Abhishek Kanaoungob, And Ankita Khatric (2018). Application of Geotextiles In Pavement Drainage Systems" International Journal of Civil Engineering Research. ISSN 2278-3652 Volume 5, Number 4 (2014), pp. 385-390 Research India Publications https://www.ripublication.com/ijcer.html
- [8] Dr. P. Senthil Kumar, R. Rajkumar (2012). "Effect of Geotextile on CBR Strength of Unpaved Road with Soft Subgrade". Electronic Journal of Geotechnical Engineering, Volume 17. Uploaded by rajkumar Ramasamy.
- [9] R. M. Tailor, M.D. Desai and N. C. Shah, (20115-17 "Geotextile as reinforcement in flexible Pavement for swelling" Proceedings of Indian Geotechnical Conference December 15-17, 2011, Kochi(PaperNo.J-230.).
- [10] Nikhil Verma, Prateek Malik (2015). "Use of Geosynthetic Material To Improve the Properties of Subgrade Soil" ISSN: 2278-0181, Vol. 4
- [11] Debasree Paul, Tarikul Islam, Mir Muhammad Fahad and Engr. Md. Eanamul Haque Nizam (2017), "Geotextiles-A Potential Technical Textile Product". The Journal of Scientific and Engineering Research November 2017.uploaded by Tarikul Islam.
- [12] Ravindra Kumar, Utsav Singh, Priyanshu Saini, Varun Sharma and Matloob Ali (2020). A Study Review on Geosynthetics use on Flexible Pavement Design "Published by International Journal of Engineering Research & Technology (IJERT) ISSN: 2278-0181. Vol. 9 Issue 06, June-2020
- [13] Natika Farooq, Er. Manish Kaushal(2022). "Use of Geosynthetic to improve the property of flexible Pavements". International Journal of Engineering Research & Technology (JERT). Volume 10





10.22214/IJRASET



45.98



IMPACT FACTOR: 7.129



IMPACT FACTOR: 7.429



INTERNATIONAL JOURNAL FOR RESEARCH

IN APPLIED SCIENCE & ENGINEERING TECHNOLOGY

Call: 08813907089 🕓 (24*7 Support on Whatsapp)