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Study of the Substantial Factors while Conceptualizing Implant Failure in the Field of Dentistry: An Overview

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Abstract: Implantology is constantly shifting and upgrading. Innovative redesign and developments in implant research and development aim to improve implant success rates. Advanced technology have transformed three-dimensional patient evaluation, foster doctors to assess, plan, and treat accurately as well. This multidisciplinary patient-centric paradigm allows for customized and successful therapy. Here, Polyetheretherketone (PEEK), a light-weight bioinert, robust thermoplastic, is being used in orthopaedics and constantly researched as an alternative dental biomaterial. As, PEEK has better chemical resistance and stress shielding than metallic materials, making it ideal for implanted applications. Although the for in vivo applications, PEEK needs surface changes to improve antimicrobial, biologically active, and Osseointegation features. Carbon fiber (CF), hydroxyapatite (HA), titanium dioxide (TiO2), multi-material PEEK composites, and their applications are highlighted. These issues can be addressed to generate synergetic, multifaceted PEEK biomaterials for long-term implantability. Keywords: Dental implants; Biomaterials; Stress-Shielding; Implant Design; PEEK

I. INTRODUCTION

Loss of natural teeth can effect daily living by limiting mastication, neuromuscular coordination, communication, and esthetics [1]. Complete edentulism treatment is one alternative denture care [2]. The residual ridge degradation is a natural aspect of the treatment, resulting in denture loosening due to poor fit [3]. The inverted edge of mandibular restorations and the tongue stimulate the mandibular region, resulting in prosthesis displacement during mastication and phonation. Research demonstrates how people with full removable dentures experience diminished masticatory efficacy, leading to aversion of solid food and negatively affecting their nutritional intake [4]. Some studies suggest that a single implant-retained overdenture can produce satisfactory retention and success. When two implants are used to retain an overdenture, the surrounding tissues experience less stress than when only one implant is used, independent of implant type. Recent studies clarify no variation in success between one- and two-implant overdentures [5][6].

Fundamental and auxiliary stability determines dental implant proficiency. Elementary stability is the contact that occurs between an implant in your mouth and its neighboring bone following location [7]–[9] . Auxiliary stability refers to the boost in stability that is the result of biological processes, such as ossification or osteogenesis, and bone metabolism or bone turnover at the implant-bone interface [10]. Initially, the dental implants with recorded achievements are initially fabricated from the conventionally used metals or basic metal alloys and had either fundamental or pin designs trying to replicate the actual teeth, which are subsequently linked to a trans-mucosal prosthesis [11], [12]. However, failure injuries were shown in many cases owing to inadequate biomechanics, primarily unsustainable stabilization as they also had specific constraints [13], [14].Though, successful outcomes were there but biological and mechanical malfunctions, which eventually stimulated the dentists to construct and examine the designs more meticulously as they former ones, lacked resemblance to the dental morphology [15]–[18]. Bio-cooperative materials are progressively used for maintaining dental restorations, which would eventually facilitate osseous regeneration, and provide provisional support throughout the healing process, so obviating the need for surgical removal [19]–[21].

For effective Osseointegation [22], [23] bio-materials [24] must possess enough strength and low weight and exhibiting minimal degradation rates. In an ideal situation, these implants will decompose and progressively passing the strain to the mending tissue. From a biomechanical perspective, stresses [13] triggered by effective or parafunctional occlusal contact [16], [25]–[28]. Since implants are attached to bone, supporting tissues may respond physiologically [29]. However, if stress surpasses the host's adaptive capabilities, supporting tissues and prosthetic components may fail.



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Amplitude and duration of load applied to implant-restoration systems affect biomechanical stress dissipation inside the implantprosthesis system and neighboring tissues [30]. Implant location, angulation, implant-abutment relationship, and occlusal load amplitude and direction affect bone stress/strain distribution around implants. In biomechanics, stress shielding is crucial with readily available standardized implants [31]–[33]. This phenomenon occurs when the implant absorbs high stress, diminishing bone mechanical stimulation. This is frequent with biocompatible titanium alloy implants like Ti–6Al–4V [34]–[38]. The substantial disparity in the modulus of elasticity between bone like we have spongy bone: (precisely 1.4 GPa) cortical bone: (precisely 13.7 GPa;) and titanium alloy (approx.110-115 GPa) [32], [39]–[43] results in phenomenon popularly referred to as stress shielding, which ultimately causes loss of bone density and resorption. Dental implant durability and success depend on correcting this mechanical discrepancy.

To reduce stress shielding and increase implant function, many techniques have been implemented. Successful strategies use materials with elastic moduli close to bone. Therefore optimizing the mechanical characteristics of the implant to osseointegrate with the adjacent bone, stress distribution is enhanced, therefore decreasing the occurrence of stress shielding. The conventionally used titanium alloys and zirconia as ceramics continue to be favored for their excellent biocompatibility [44]; nevertheless, research indicates that advancements in material science are expanding the possibilities in study and looking for a better implant material. Plaque reduction is another implant design goal [30], [45].

This method uses a homogeneous implant body with smooth crestal surfaces [46]–[52]. Implant crest modules with flat surfaces are easier to clean and acquire less plaque. Therefore, if bone resorption occurs in the marginal areas of implants. The polished implant interface will accumulate less plaque and make it easier and hence, simple maintenance [53]. The smoother crown component positioned beneath the bone crest assists a small reduction in bone owing to the elongation of biological width. During implant uncover and shear forces during occlusal loading [54].

This design innovation deepens the space surrounding the dental implant. The majority issues pertain marginal bone loss before to loading but subsequent to implant exposure and to early implant failure post-loading, and marginal bone loss after the loading of the implant-bone interface. Primitive loading failures occur in weaker bone types (that are linked to osteoporosis or osteopenia) or shorter dental implants' lengths [55], [56]. Thus, implant body designs should focus on reducing the major sources of difficulties, namely the factor that affects implant loading after operation. The surgical trauma, bacterial contagion, and bone-implant stress can cause bone resorption [57]. Functional forces can cause peri-implant bone overloading due to load transfer system deficiencies caused by implant development at that region, poor occlusion, prosthesis and surgical allocation. Thus, the bone-implant contact may experience higher stress concentration [58], and associated strain in bone tissue may cause bone degeneration, reducing overall implant efficacy. Design elements, such as bone stress and strain distribution, affect load transfer and implant form. These include implant diameter, bone-implant interface length, thread pitch, shape, and depth for threaded implants [59]-[68]. To increase osseous integration surface area, threaded implants are favored over cylindrical layout. Bone effectiveness, surface enhancements, and thread configuration can profoundly influence implant stability and post-healing biomechanical properties [69]–[72]. Cylindrically smooth implants are easier to implant, but bone-implant contact has higher shear forces. The cylindrically tapered with certain degree of flute cut such implant transfers compressive load to bone-implant contact [63]. Compressive force to the contact increases with a bigger taper. An enhanced taper of a smooth-sided implant generally reduces its surface contact under stress and initial stability during extraction and insertion. Threaded implant do convert occlusal loads into the then generated compressive loads at the bone interface, hence thread configuration tends to play critical role for long-term load transmission. Buttresses or square-shaped threads on dental implants transfer compressive forces to bone under axial tension.

II. FACTORS TO EVALUATE WHILE SELECTING AN IMPLANT SYSTEM

A. Impact of Thread Configuration/Geometry

Tapered or paralleled inserts are prevalent. Tapered configurations are more primary stable than parallel designs. Threads basically strengthen the initial contact thus leads to interfacial stress absorption. Threaded implants improve mechanical Osseointegation and load stress distribution. 9 Huang et al. said "interconnected implants could lessen both pressure on the bone and the implanted-bone sliding distance, thereby possibly improving initial reliability and prolonged durability." Chun et al. found that a square pitched thread with a narrower radius disseminates stress better. Geometric parameters which incorporates thread depth, thickness, thread pitch, face angle, and helix angle lay out the functional thread area and affect implant biomechanical load distribution [63], [73].



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B. Thread Pitch

Thread pitch is the parallel gap between implantation thread form parts. Number of threads per unit length = implant body threaded section height / pitch. A finer pitch increases implant body threads, assuming all other parameters remain unchanged. Of all design factors, pitch changes threaded implant surface area the most. Thread pitch [74] may reduce inferior grade bone stress. The poorest bone type (having their T- score less than 2.5) is 58% weaker than the ideal bone quality, therefore adding implant at this location can increase surface area and reduce stress on the poorer bone trabeculae. Thus, if consequential force, implant length, or bone density change, the thread pitch can be modified to increase thread count and accessible surface area. Different thread configurations are: square, V-shaped, buttress, reverse buttress whichever suits our prerequisite. Thread face angle may change prosthesis load direction to a new bone force vector. A V-like thread profile[59] resembles a buttress thread under axial strains if the face inclination is around 30°. A square thread design reduces shear strain by channeling the prosthesis's axial load and penetrates it on the implant to clench bone. The thread configuration is generally employed for loading design, but it may also affect direct bone contact healing. The face angle may redirect occlusal force at the bone contact. Axial occlusal stresses is actually the compressive forces at the bone interface with square-shaped threads, but V-shaped threads may increase shear forces. V-threads and reverse buttress threads have 10 times the shear force of square threads [75][47]. Low shear stress at the thread-bone interface improves compressive load transfer, which is crucial in circumstances of low bone density, short implant lengths, or high force magnitudes [55]. Many thread geometries with identical pitch reveal that implants with varied entire contact points at the implant-bone interface[71] alter fundamental stability. Stress loading on threaded implants is highest at the implant's initial pitch and cortical bone, according to previous studies. Thickness of cortical bone ranges from 0.80 to 2.00 mm, with thicker bone holding more load. Kong et al. recommended screwed implants with thread pitches of 0.75 mm for biomechanical reasons. Square threads with 0.60 mm pitches offer adequate stress, according to Lee et al.20 findings. Chung et al. founded in his research that 0.6-mm implants lost more crestal bone than 0.5-mm implants. Lan et al. found that loading variation is the main factor affecting stress distribution and that fastened implants using thread pitches bigger than 0.80 mm are biomechanically better. All thread shapes have optimum thread pitches basically to alleviate the bone stress.

C. Thread Depth

Thread depth is the gap between the significant and auxiliary diameters. Traditional implants have uniform thread depth across the whole implant. Parallel-walled implants have a uniform cross-sectional area because they possess a consistent minor diameter. A tapered insertion has the same internal diameter but a smaller outer diameter, diminishing thread depth toward the apex[73], [76], [77]. This implant design reduces surface area, which is important for shorter implants. Thus, the implant body taper may increase stress, especially with shorter implants. A broader thread maximizes implant surface area if all other factors remain unchanged. The implant increases its contact area by about 15–25% for every 1 mm diameter coverage. The thread depth can expand with an implant's diameter without affecting the wall width between its interior and the screw that supports the gap. Thread depth can be changed to match implant diameter, increasing overall surface area by 150% per 1-mm increment[46], [75].

D. Considerations for Crest Module

An implant body's transosteal area, or crest module, often includes the abutment implant connection's autorotation components. The implant's crest module affects surgery, biological width, loading profile (a mechanically strained part), and prosthetics. Thus, the implant body's design depends on this area [75]. A greater crest module increases surface area, therefore minimizes crestal stress[46]. Because the pressures are highest here, the larger surface area reduces bone stress and strengthens the implant body. Increasing the crest module diameter improves the abutment connection platform[62], reducing lateral loading stress on the screw. The platform dimension is more important than the height (or depth) of the abutment screw's antirotational hex in reducing stress to implant bodily link. Most implant occlusal stresses occur near the crest [70].

E. Designing the Apex

Circular root shape implants are the ones, when abutment links are torqued or when single-tooth implants are detached, circular cross-sections fail to resist torsional and shear loads. Thus, the implant body has an antirotational characteristic, usually apical. Hole or vent designs are most popular. Bone can develop through the coronal hole and sustain implant torsional forces [78]. The apical orifice may augment the surface area for the transmission of compressive stress in bone. The apical hole is detrimental when the implant penetrates the sinus floor or cortical plate [10]. Mucus tissue may fill the apical opening, causing retrograde contamination. Due to its smaller surface area, pointed shape increases bone stress. If moved, a V-shaped pinnacle, might irritate delicate tissues.



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F. Impact of implant shape, diameter, and length

Growing bone prefers to concentrate on protruding implant surface elements like crests, ridges, teeth, or the thread edge, that function as stress concentrators during load transfer [39]. Implant form determines stress transfer surface area and early stability. Threads on implant surfaces convert shear pressures into more resistive forces at the bone contact.

G. Implants' Length

From platform to apex, implant length is measured[79]. The average length is 8–13 mm, which is similar to normal root length. The crestal bone interface is not important for implant length or Osseointegation, but initial stability and bone–implant interface are. The longer length helps resist torque and shear pressures when screwing abutments in. However, the additional length does not reduce transosteal stress surrounding the implant at the ridge crest or affect Osseointegation [25].

H. Implants' Diameter

It measures from the widest thread peak to the same point on the other side. For bone load distribution, it is more significant than implant length. Most implants are around 4 mm in diameter to be precise for the strength but, at least 3.25 mm is definitely needed for strength. Wider implants engage more bone and distribute stress better in the surrounding bone, biomechanically. As proven, higher bone contact surface area may increase preliminary stability and stress resistance. The implant's surface area increases with diameter, enhancing bone contact. Previous research showed that expanding the diameter to 3 mm implant by 1 mm increases its surface area by approximately 35% for the same.

I. Implant Shape

The configuration of dental implants is a highly contested design aspect within endosseous systems and may influence biomechanics. The majority of implant devices consist of solid or hollow screws or cylinders. The crestal and apical regions of screw-type implants have been altered to facilitate self-tapping and minimize heat production. Alternative designs employ a stepped cylindrical configuration to replicate root morphology at both the cervical and apical terminals. The cylindrical implants offer superior stress dissipation compared to cylindrical or tapered implants, as well as enhanced crestal bone loading and alveolar aid in bone growth due to their root analog configuration.

J. Bio-Compatible Implant Material

Recent advancements in the creation of new alloys, particularly Molybdenum-based materials, which have exceptional mechanical capabilities that have not been previously investigated in relation to biodegradable implants[80]. We also examine improved surface alteration and manufacturing options that improve biodegradable metallic implant performance. [81]. These materials' corrosion mechanism is extensively researched to highlight their dynamic deterioration. They elucidate the intricate interplay of implant materials, adjacent tissues, and the body's acidic milieu. This article offers a comprehensive overview of biodegradable metallic implants and establishes a foundation for future research and the development of implants with enhanced mechanical qualities and controlled degradation rates.

K. Magnesium alloys/composite

Magnesium-based alloys may be orthopedic biomaterials[21]. Young's modulus and cortical bone anisotropy are correlated with Mg. After degradation in physiological environments, Mg is osteopromotive and biocompatible. Due to its increased availability, magnesium is widely used in medicine. Edward C.H. initially employed magnesium wires as blood vessel ligatures in 1878. Next, magnesium plates, tubes and screws for arthroplasty and connections for nerves were examined. These trials showed lower biocompatibility and deterioration than expected. Subcutaneously gas cavities and deteriorated structure post-operation were also identified in subsequent decades. Though, Magnesium and Cadmium alloy screws and plates have successfully treated fractures[36]. Mg–Cd implants improved fracture healing resilience. Some failures were caused by gas cysts or infections. The individuals had neither acute inflammatory responses nor abnormal blood magnesium alloys are more biocompatible. Bio-ceramics like PLLA, POLYETHERETHERKETONE[82], and polyglycolic acid, magnesium alloys are more biocompatible. Bio-ceramics like tricalcium phosphate (TCP)[83] and hydroxyapatite (Hap)[73], which often lack mechanical strength for bone implantation are surpassed by these bio polymer. Surface quality, stiffness, and malleability make magnesium alloys sterilizable. The byproducts of magnesium alloys and implants, especially magnesium ions, are non-toxic and safe.



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Their osteopromotive properties are unique. Osterix levels rise and bone healing is accelerated by degraded Mg ions and transporter proteins. Due to its rapid mechanical degradation before surrounding tissues recover, this substance has limited biological usefulness.

L. Polymeric Biomaterials

The primary benefits of polymeric biomaterials[84] over metal materials are simplicity of fabrication into many forms, straightforward secondary processing, cost-effectiveness, and accessibility with requisite mechanical and physical qualities. The essential characteristics of polymeric biomaterials[85] align with those of other biomaterials, including biocompatibility, sterilizability, sufficient mechanical and physical qualities, and manufacturability. Despite the ease of synthesizing hundreds of polymers suitable for biomaterials, only 10 to 20 polymers are mostly used in the manufacture of medical devices, ranging from disposable items to long-term implants. Polyetheretherketone (PEEK)[86] is aesthetically tooth-colored polymer, the use of this biomaterial in orthopedics is already been done. It is produced by step-growth dialkylation of bis-phenolates. A common PEEK synthesis includes reacting 4,4'-difluorobenzophenone with the metallic salt of hydroquinone at 305-310°C in a polar solvent such diphenyl sulphone. Semicrystalline, its melting point is around 335 °C[87]. Pre-polymerization with functionalized monomers or post-polymerization with sulphonation, amination, and nitration can modify PEEK. Most beneficial for orthopedic implant applications is its lower Young's (elastic) modulus is around (3-4.5 GPa), which roughly matches human bones' elastic modulus. Adding different components can easily modify polyetheretherketone. Carbon fiber reinforcement can increase the pure PEEK elastic modulus to somewhat 18 GPa[57]. Titanium and its alloys have a higher elastic modulus than required for a bone to endure, causing stress shielding and failure. Carbon-reinforced Polyetheretherketone has the same modulus as cortical bone and dentin, suggesting it may have less stress shielding than titanium, an implant material. In mechanical terms, Polyetheretherketone is an appropriate materials for rehabilitation whilst its tensile properties are similar to bone, enamel, and dentin[36]. A stepwise progression dialkylation process of bis-phenolates transforms ether ketone monomer units to yield polyetheretherketone, a thermoplastic polymer with semicrystalline structure having the chemical formula (-C6H4-CO-C6H4-O-C6H4-O-)n. Physiochemically, polyetheretherketone has a high melting point of 334°C, ensuring structural integrity above 300°C. It withstands organic solvents, acids, and bases. It is also strong, fatigue- and abrasion-resistant, and compatible with various reinforcing agents. Polyetheretherketone lacks osteoconductive properties like titanium[88]. Therefore, substantial study has been done to improve Polyetheretherketone implant bioactivity. Polyetheretherketone can exhibit its biological properties through the application of synthetic osteoconductive hydroxyapatite coatings, enhancement of surface roughness, implementation of chemical changes, or incorporation of bioactive particles[9]. The white hue and robust mechanical characteristics render polyetheretherketone an excellent option for both permanent and detachable dental prostheses. Polyetheretherketone surface modification has been tested for adhesion with luting agents and removed teeth. Polyetheretherketone can also be an attractive orthodontic wire. Polyetheretherketone orthodontic wires can provide superior orthodontic forces compared to polyether sulfone (PES) and polyvinylidene difluoride (PVDF), while preserving a cross-section comparable to metallic wires[89] such as cobalt-chromium (Co-Cr), titanium-molybdenum (Ti-Mo), and nickel-titanium. Polyetheretherketone is suitable for dental applications due to its distinctive physical and mechanical qualities.

M. PEEK implant material

Tension remodels bone, as per the Wolff's Law[40]. Stress shielding diminishes bone density surrounding an implant by alleviating the mechanical stresses and concentrating all the stresses on itself rather than dividing to the whole bone surrounding it. Finite element analysis of CFR-Polyetheretherketone implants revealed they may give less stress shielding than titanium. Since Polyetheretherketone dental implants are not commonly used in clinical practice, it is uncertain if they differ from titanium implants in bone resorption in humans[79], [90], [91]. A recent analysis by Sarot et al. finds that no stress distribution difference between polyetheretherketone and titanium dental implants. Further clinical trials are needed to determine if polyetheretherketone implants reduce stress shielding compared to titanium implants. Unmodified Polyetheretherketone is biocompatible and hydrophobic with an 80–85.8-degree water contact angle. Unrevised Polyetheretherketone does not affect cell proliferation in vitro, according to research. In contrast, conventional and CFR-polyetheretherketone materials have been shown to increase protein turnover in cells. Animal studies show that polyetheretherketone can last three years with only localized irritation. Numerous studies show that polyetheretherketone inhibits miRNA processing, which may limit surface cellular growth and cause long-term damage. The similar proteomic studies showed no bio inertness difference between polyetheretherketone, zirconia, and titanium.

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Unaltered polyetheretherketone is a biointert material, although its osteoconductive capabilities are unknown in vivo or in vitro. Therefore, the long-term survival rate of undamaged polyetheretherketone implants is unknown. Polyetheretherketone materials have undergone several changes to improve mechanical and biological properties. However, polyetheretherketone dental implants have not been widely used in clinical settings, and there is little long-term data on their efficacy.

Polyetheretherketone has been nano-modified to improve bioactivity and osseoconductive characteristics. Plasma spraying has coated polyetheretherketone with bioactive compounds like osseoconductive calcium hydroxyapatite (hap) or titanium. Plasma torch deposits particles on implants. Plasma liquefies particles and deposits them on the implant, creating a texture. For larger dental implants, a bioactive layer may work, but not for smaller ones. Delamination of the thick apatite layer (Ra \approx 7-8 mm) might cause implant failures. Plasma-spray coating polyetheretherketone with hap at high temperatures is another drawback[92]. Due to its low melting point (340-343°C), polyetheretherketone may degrade at higher temperatures. High temperatures during plasma-sprayed hap coatings on CFR-polyetheretherketone may evaporate carbon fibers from the implant's surface, reducing bond strength (2.9 MPa).

Bioactive polyetheretherketone nanocomposites and nanoscale coatings containing bioactive apatite have received significant attention. Osteogenic implant coatings change dental implant surfaces[93]. Bioactive surface coatings improve implant Osseointegation by interacting with bone tissues. Spin-coating deposits nanoscale calcium hydroxyapatite on polyetheretheretherethere surfaces[94]. Apatite suspended in solvents made from organic matter is applied to an adjusting implant. Thermal processing forms implants strengthen bone-implant contact (BIC). Removal torque did not change significantly. Plasma-gas etching can modify polyetheretherketone nanoscale surfaces. Low-pressure gases provide nano-scale surface roughness and functional groups on polyetheretherketone implants, increasing hydrophilicity for material-tissue interaction. Gas-plasma modified polyetheretherketone implants increased human mesenchymal cell proliferation and differentiation in vitro. Many have recently studied CFRpolyetheretherketone hip stems in ovine subjects, but Polyetheretherketone altered by low-pressure conditions prevail oxygen plasma placed in rabbit bones is still lacking a significant enhancement in bone-implant contact (BIC). CFR-polyetherethereketone hip stems were plasma-sprayed with a 17-18 nm-thick TiO₂ and hydroxyapatite layer, then immersed in Alpha-tricalcium phosphate. They possess remarkable biocompatibility and mechanical properties for hip implants devoid of metallic ions. Ha-coated CFR/polyetheretherketone grafts provide cement-free retention for carrying load applications. These studies show that coated polyetheretherketone polymers have great dental implant potential.

There have been no human clinical trials with coated polyetheretherketone dental implants, which are needed to determine biocompatibility before use.

Electron-beam (e-beam) deposition utilizes an electron beam in order to breakdown and deposit an incredibly thin nano-rough film of matter onto a substrate[95]. Many nano-modifications have improved Polyetheretherketone's biological and physical qualities. Titanium covering polyetheretherketone with this approach increases hydrophilicity and cell proliferation. Anodized nanoporous titanium electron beam-coated may help immobilize bone morphogenic protein-2. Titanium/bmp-2-coated polyetheretherketone implants have great potential for oral Implantology. E-beam-coated prostheses remain untested in vivo, rendering their clinical potential uncertain. A high-voltage particle plasma may form a thin coating of particles on a substrate. This is plasma immersion ion implantation [96].

III. CONCLUSION

The loading type, material characteristics of the insertion and artificial tooth, implant geometry, surface topology, and the caliber and measure of the surrounding bone, along with the bone–implant interface, influence the stress and strain distributions around osseointegrate dental implants. Many implant concepts and sizes, forms, materials, and surfaces are commercially accessible. Stress study of mechanical interactions between bone and implant and implant failure risk assessment are crucial to endosseous implant effectiveness and dependability. Closed-form stress evaluation is impossible for the coupled bone–implant biomechanical system due to its complicated shape. Thus, numerical methods like finite element analysis can forecast stress and strain distributions in peri-implant regions, examine implant and prosthesis designs, load magnitude and orientation, and bone mechanical properties, and simulate various clinical situations to analyze endosteal dental implants.

Swift progress in biodegradable implants and gadgets has shown novel therapeutic pathways for fostering favorable biological reactions. Temperature, pH, and biological cues can induce these biomaterials to dynamically change their characteristics or functions.



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Synthetic implants called biomaterials can temporarily replace and improve biological tissues. Medical biomaterials are chosen based on their mechanical characteristics, biocompatibility, and weight by mass, biodegradability and physicochemical attributes. Titanium are the predominant materials utilized in orthopedic implants. They exhibit effective healing owing to their robustness and resistance to corrosion. Nonetheless, these materials are non-biodegradable, necessitating further procedures for implant extraction, which restricts growth, temperature sensitivity, and cross-contamination. Bone replacement, dental surgery, and bone stabilization require implants, which may have side effects. Synthetic biodegradable polymer implants reduce procedures and speed healing thanks to medical research.

New biomaterials are preferred to improve medicines and life have advanced significantly in the recent decade. Recent advances in specialized drug delivery, regenerative therapies, and tissue engineering have boosted the utilization of biodegradable substances for sophisticated clinical applications. Polydioxanone and poly (L-lactic acid) are utilized in bile duct stents. Biliary stents are made from biodegradable polymers with different biodegradation rates. The selection of biodegradable polymers is contingent upon mechanical integrity, elevated tensile strength, non-toxicity, and a controlled degradation rate.

Additionally, chemical properties greatly affect biocompatibility. For sustained physiological immersion, bio implants should be biocompatible with the body. Magnesium, and Zinc are the main bio-absorbable metals. After performing medicinal functions like tissue regeneration, disease detection, and support, these biomaterials corrode and degrade in vivo without harming the host. Biodegradable metals outperform polymeric bone implants and cardiovascular stents in strength and performance.

Absorbable implant materials offer large market prospects due to their medicinal benefits. The synthetic biodegradable polyesters are much in studies.

These needs complicate biomaterial production. Primary concern is corrosion degradation products released into the environment. These items may injure the body further. For biosafety, deteriorated commodities must be improved. Biocompatible material degradation should match healing kinetics. In cardiovascular applications, healing involves inflammation, granulation, and remodeling. Broken bones recover through inflammation, repair, and remodeling.

This paper critically evaluates and discusses biodegradable and bio-absorbable materials for medical applications, their future usage and prospects.

REFERENCES

- Q. Nafeesa and I. Zahid, "Principles and concepts of occlusion in restorative dentistry," Int. J. Oral Craniofacial Sci., vol. 9, no. 1, pp. 001–007, 2023, doi: 10.17352/2455-4634.000059.
- [2] "Dziedzic, A., & Puryer, J. S. (2019). Complete Dentures Assessment of the Loose Denture. Dental Update, 46 (8), 760-767., vol. 46, pp. 760–767, 2019.
- [3] I. Alfahdawi, "New direct resilient relining material of denture base," Int. Med. J., vol. 25, no. 2, pp. 125–127, 2018.
- [4] I. Tsolianos, A.-B. Haidich, D. G. Goulis, and E. Kotsiomiti, "The effect of mandibular implant overdentures on masticatory performance: A systematic review and meta-analysis," Dent. Rev., vol. 3, no. 4, p. 100072, 2023, doi: 10.1016/j.dentre.2023.100072.
- [5] R. Srivastava, R. Bansal, P. K. Dubey, and D. Singh, "A comparative evaluation of masticatory load distribution in different types of prosthesis with varying number of implants: A FEM analysis," J. Oral Biol. Craniofacial Res., vol. 14, no. 3, pp. 284–289, 2024, doi: 10.1016/j.jobcr.2024.03.010.
- [6] A. J. Sharma, R. Nagrath, and M. Lahori, "A comparative evaluation of chewing efficiency, masticatory bite force, and patient satisfaction between conventional denture and implant-supported mandibular overdenture: An in vivo study," J. Indian Prosthodont. Soc., vol. 17, no. 4, pp. 361–372, 2017, doi: 10.4103/jips_jips_76_17.
- [7] F. Javed, H. Ahmed, R. Crespi, and G. Romanos, "Role of primary stability for successful osseointegration of dental implants: Factors of influence and evaluation," Interv. Med. Appl. Sci., vol. 5, no. 4, pp. 162–167, 2013, doi: 10.1556/IMAS.5.2013.4.3.
- [8] R. S. Liddell, E. Ajami, Y. Li, E. Bajenova, Y. Yang, and J. E. Davies, "The influence of implant design on the kinetics of osseointegration and bone anchorage homeostasis," Acta Biomater., vol. 121, pp. 514–526, 2021, doi: 10.1016/j.actbio.2020.11.043.
- [9] S. Yadav, A. Nath, R. Suresh, A. Kurumathur Vasudevan, B. Balakrishnan, and M. Rajan Peter, "Advances in Implant Surface Technology: A Biological Perspective," Cureus, vol. 17, no. 1, pp. 1–11, 2025, doi: 10.7759/cureus.78264.
- [10] V. Swami, V. Vijayaraghavan, and V. Swami, "Current trends to measure implant stability," J. Indian Prosthodont. Soc., vol. 16, no. 2, pp. 124–130, 2016, doi: 10.4103/0972-4052.176539.
- [11] A. Celeste M, "A Brief Historical Perspective on Dental Implants, Their Surface Coatingsand Treatments," Open Dent. J., vol. 8, pp. 50–55, 2014.
- [12] M. Saini, "Implant biomaterials: A comprehensive review," World J. Clin. Cases, vol. 3, no. 1, p. 52, 2015, doi: 10.12998/wjcc.v3.i1.52.
- [13] M. Gasik, F. Lambert, and M. Bacevic, "Biomechanical properties of bone and mucosa for design and application of dental implants," Materials (Basel)., vol. 14, no. 11, 2021, doi: 10.3390/ma14112845.
- [14] A. Manea et al., "Principles of biomechanics in oral implantology," Med. Pharm. Reports, vol. 92, no. 3, pp. 14–19, 2019, doi: 10.15386/MPR-1512.
- [15] H. C. Campista, J. D. M. de Matos, D. A. Queiroz, L. C. Maciel, P. Marcelo Massaroni, and P. Daiane Cristina, Dental anatomy and morphology, no. March. 2023. doi: 10.22533/at.ed.298230903.
- [16] R. Ćelić, H. Pezo, S. Senzel, and G. Ćelić, "The Relationship between Dental Occlusion and 'Prosthetic Occlusion' of Prosthetic Restorations Supported by Natural Teeth and Osseointegrated Dental Implants," 2023, doi: 10.5772/intechopen.109941.
- [17] E. Lidia Crăciunescu et al., "Dental Anatomy and Morphology of Permanent Teeth," 2023, doi: 10.5772/intechopen.110223.



ISSN: 2321-9653; IC Value: 45.98; SJ Impact Factor: 7.538

Volume 13 Issue VII July 2025- Available at www.ijraset.com

- [18] G. Oxilia, M. Tomasella, and A. Cecere, "Dental Morphology in Restorative Dentistry: A Pilot Study on Morphological Consistency and Variability in Human Upper First Molars," Dent. J., vol. 13, no. 3, pp. 1–12, 2025, doi: 10.3390/dj13030122.
- [19] A. Szwed-Georgiou et al., "Bioactive Materials for Bone Regeneration: Biomolecules and Delivery Systems," ACS Biomaterials Science and Engineering, vol. 9, no. 9. American Chemical Society, pp. 5222–5254, Sep. 11, 2023. doi: 10.1021/acsbiomaterials.3c00609.
- [20] F. H. Alzahrani et al., "Letters in High Energy Physics Volume 2024 The Use of Biocompatible Materials in Restorative Dentistry," vol. 2024, pp. 1920–1933, 2024.
- [21] W. Wang and K. W. K. Yeung, "Bone grafts and biomaterials substitutes for bone defect repair: A review," Bioact. Mater., vol. 2, no. 4, pp. 224–247, 2017, doi: 10.1016/j.bioactmat.2017.05.007.
- [22] C. Pandey, D. Rokaya, and B. P. Bhattarai, "Contemporary Concepts in Osseointegration of Dental Implants: A Review," BioMed Research International, vol. 2022. Hindawi Limited, 2022. doi: 10.1155/2022/6170452.
- [23] N. Walter, T. Stich, D. Docheva, V. Alt, and M. Rupp, "Evolution of implants and advancements for osseointegration: A narrative review," Injury, vol. 53, pp. S69–S73, 2022, doi: 10.1016/j.injury.2022.05.057.
- [24] U. Oza, H. Parikh, S. Duseja, and C. Agrawal, "Dental Implant Biomaterials: A Comprehensive Review," Int. J. Dent. Res., vol. 5, no. 2, pp. 87–92, 2020, doi: 10.31254/dentistry.2020.5212.
- [25] D. Flanagan, "Bite force and dental implant treatment: A short review," Med. Devices Evid. Res., vol. 10, pp. 141–148, 2017, doi: 10.2147/MDER.S130314.
- [26] Y. Zhu, F. Zheng, Y. Gong, J. Zhu, D. Yin, and Y. Liu, "Effect of occlusal contact on TMJ loading during occlusion: An in silico study," Comput. Biol. Med., vol. 178, no. 174, p. 108725, 2024, doi: 10.1016/j.compbiomed.2024.108725.
- [27] M. Wang et al., "Impact of occlusal contact pattern on dental stability and oromandibular system after orthodontic tooth movement in rats," Sci. Rep., vol. 13, no. 1, pp. 1–13, 2023, doi: 10.1038/s41598-023-46668-x.
- [28] R. Chaithanya, S. Sajjan, and A. V. R. Raju, "A study of change in occlusal contacts and force dynamics after fixed prosthetic treatment and after equilibration-Using Tekscan III," J. Indian Prosthodont. Soc., vol. 19, no. 1, pp. 9–16, 2019, doi: 10.4103/jips.jips_238_18.
- [29] T. Albrektsson and C. Johansson, "Osteoinduction, osteoconduction and osseointegration," Eur. Spine J., vol. 10, pp. S96–S101, 2001, doi: 10.1007/s005860100282
- [30] V. John, D. Shin, A. Marlow, and Y. Hamada, "Peri-Implant Bone Loss and Peri-Implantitis: A Report of Three Cases and Review of the Literature," Case Rep. Dent., vol. 2016, 2016, doi: 10.1155/2016/2491714.
- [31] K.-Y. Liu, L.-X. Yin, X. Lin, and S.-X. Liang, "Development of Low Elastic Modulus Titanium Alloys as Implant Biomaterials," Recent Prog. Mater., vol. 4, no. 2, pp. 1–1, Mar. 2022, doi: 10.21926/rpm.2202008.
- [32] M. Niinomi and M. Nakai, "Titanium-based biomaterials for preventing stress shielding between implant devices and bone," Int. J. Biomater., vol. 2011, 2011, doi: 10.1155/2011/836587
- [33] S. Najeeb, M. S. Zafar, Z. Khurshid, and F. Siddiqui, "Applications of polyetheretherketone (PEEK) in oral implantology and prosthodontics," Journal of Prosthodontic Research, vol. 60, no. 1. Elsevier Ltd, pp. 12–19, Jan. 01, 2016. doi: 10.1016/j.jpor.2015.10.001.
- [34] J. Han, J. Zhao, and Z. Shen, "Zirconia ceramics in metal-free implant dentistry," Adv. Appl. Ceram., vol. 116, no. 3, pp. 138–150, 2017, doi: 10.1080/17436753.2016.1264537.
- [35] F. D. Al-Shalawi et al., "Biomaterials as Implants in the Orthopedic Field for Regenerative Medicine: Metal versus Synthetic Polymers," Polymers, vol. 15, no. 12. MDPI, Jun. 01, 2023. doi: 10.3390/polym15122601
- [36] K. Moghadasi et al., "A review on biomedical implant materials and the effect of friction stir based techniques on their mechanical and tribological properties," Journal of Materials Research and Technology, vol. 17. Elsevier Editora Ltda, pp. 1054–1121, Mar. 01, 2022. doi: 10.1016/j.jmrt.2022.01.050.
- [37] R. Comino-Garayoa, J. C. B. Brinkmann, J. Peláez, C. López-Suárez, J. M. Martínez-González, and M. J. Suárez, "Allergies to titanium dental implants: What do we really know about them? A scoping review," Biology, vol. 9, no. 11. MDPI AG, pp. 1–15, Nov. 01, 2020. doi: 10.3390/biology9110404.
- [38] K. Treutler and V. Wesling, "applied sciences The Current State of Research of Wire Arc Additive Manufacturing (WAAM): A Review," Appl. Sci., 2021.
- [39] L. Shi et al., "The Improved Biological Performance of a Novel Low Elastic Modulus Implant," PLoS One, vol. 8, no. 2, pp. 4–9, 2013, doi: 10.1371/journal.pone.0055015.
- [40] A. Schwitalla and W. D. Müller, "PEEK dental implants: A review of the literature," J. Oral Implantol., vol. 39, no. 6, pp. 743–749, 2013, doi: 10.1563/AAID-JOI-D-11-00002.
- [41] F. Ahmad, S. Nimonkar, V. Belkhode, and P. Nimonkar, "Role of Polyetheretherketone in Prosthodontics: A Literature Review," Cureus, May 2024, doi: 10.7759/cureus.60552.
- [42] W. Al-Zyoud, D. Haddadin, S. A. Hasan, H. Jaradat, and O. Kanoun, "Biocompatibility Testing for Implants: A Novel Tool for Selection and Characterization," Materials (Basel)., vol. 16, no. 21, 2023, doi: 10.3390/ma16216881.
- [43] K. J. Chun, H. H. Choi, and J. Y. Lee, "Comparison of mechanical property and role between enamel and dentin in the human teeth," J. Dent. Biomech., vol. 5, no. 1, pp. 1–7, 2014, doi: 10.1177/1758736014520809.
- [44] P. V Singh, A. Reche, P. Paul, and S. Agarwal, "Zirconia Facts and Perspectives for Biomaterials in Dental Implantology," Cureus, Oct. 2023, doi: 10.7759/cureus.46828.
- [45] J. Prathapachandran and N. Suresh, "Management of peri-implantitis," vol. 9, no. 5, 2012.
- [46] P. Shetty, P. Yadav, M. Tahir, and V. Saini, "Implant Design and Stress Distribution," Int. J. Oral Implantol. Clin. Res., vol. 7, no. 2, pp. 34–39, 2016, doi: 10.5005/jp-journals-10012-1151.
- [47] M. Rismanchian, R. Birang, M. Shahmoradi, H. Talebi, and R. J. Zare, "Developing a new dental implant design and comparing its biomechanical features with designs.," (Isfahan)., 2010. four Dent. Res. J. vol. 7. no. 2, pp. 70-5.[Online]. Available: http://www.ncbi.nlm.nih.gov/pubmed/22013460%0Ahttp://www.pubmedcentral.nih.gov/articlerender.fcgi?artid=PMC3177371
- [48] T. Tushar, S. Garg, A. Chaudhary, and A. Aggarwal, "Scientific Rationale of Implant Design: A Review Article," Saudi J. Oral Dent. Res., vol. 7, no. 4, pp. 101–106, 2022, doi: 10.36348/sjodr.2022.v07i04.001.
- [49] A. Mishra, M. Khatri, M. Bansal, Mohd. Rehhan, S. Gaind, and S. Khan, "Changing trends in implant designs: A review," IP Int. J. Periodontol. Implantol., vol. 8, no. 3, pp. 117–123, 2023, doi: 10.18231/j.ijpi.2023.024



ISSN: 2321-9653; IC Value: 45.98; SJ Impact Factor: 7.538

Volume 13 Issue VII July 2025- Available at www.ijraset.com

- [50] A. Jenner, G. P. Sabatini, S. Abou-Ayash, E. Couso-Queiruga, V. Chappuis, and C. Raabe, "Primary implant stability of two implant macro-designs in different alveolar ridge morphologies: an in vitro study," Int. J. Implant Dent., vol. 11, no. 1, 2025, doi: 10.1186/s40729-025-00605-x.
- [51] D. Sciences and K. Layout, "ORIGINAL RESEARCH PAPER IMPLANT DESIGN CONSIDERATIONS A REVIEW," no. 6, 2020.
- [52] J. Z. C. Chang et al., "Optimizing dental implant design: Structure, strength, and bone ingrowth," J. Dent. Sci., vol. 20, no. 2, pp. 1016–1026, 2025, doi: 10.1016/j.jds.2024.11.024.
- [53] L. Preiss et al., "Bone mechanical behavior around dental implants: Densification and deformation follow-up by in-situ computed tomography," J. Mech. Behav. Biomed. Mater., vol. 167, no. March, 2025, doi: 10.1016/j.jmbbm.2025.106966.
- [54] J. Z. C. Chang et al., "Optimizing dental implant design: Structure, strength, and bone ingrowth," J. Dent. Sci., vol. 20, no. 2, pp. 1016–1026, 2025, doi: 10.1016/j.jds.2024.11.024.
- [55] H. C. Wu, H. L. Huang, L. J. Fuh, M. T. Tsai, and J. T. Hsu, "Influence of implant length and insertion depth on primary stability of short dental implants: An in vitro study of a novel mandibular artificial bone model," J. Dent. Sci., vol. 19, no. 1, pp. 139–147, 2024, doi: 10.1016/j.jds.2023.05.019.
- [56] M. Xing et al., "All-in-one design of titanium-based dental implant systems for enhanced soft and hard tissue integration," Biomaterials, vol. 320, no. March, 2025, doi: 10.1016/j.biomaterials.2025.123251.
- [57] W. T. Lee, J. Y. Koak, Y. J. Lim, S. K. Kim, H. B. Kwon, and M. J. Kim, "Stress shielding and fatigue limits of poly-ether-ether-ketone dental implants," J. Biomed. Mater. Res. Part B Appl. Biomater., vol. 100 B, no. 4, pp. 1044–1052, May 2012, doi: 10.1002/jbm.b.32669.
- [58] T. Stich, F. Alagboso, T. Křenek, T. Kovářík, V. Alt, and D. Docheva, "Implant-bone-interface: Reviewing the impact of titanium surface modifications on osteogenic processes in vitro and in vivo," Bioeng. Transl. Med., vol. 7, no. 1, pp. 1–20, 2022, doi: 10.1002/btm2.10239.
- [59] K. Singh, R. Upadhyaya, M. Rayes, S. Bind, A. Poundarik, and A. Tiwari, "A comparative analysis of insertion of dental implants of V, square and trapezoidal screw designs," Next Res., vol. 2, no. 3, p. 100462, 2025, doi: 10.1016/j.nexres.2025.100462.
- [60] L. P. Raut and R. V Taiwade, "Wire Arc Additive Manufacturing: A Comprehensive Review and Research Directions," J. Mater. Eng. Perform., vol. 30, no. 7, pp. 4768–4791, 2021, doi: 10.1007/s11665-021-05871-5.
- [61] C. L. Chang, J. J. Chen, and C. S. Chen, "Using optimization approach to design dental implant in three types of bone quality A finite element analysis," J. Dent. Sci., vol. 20, no. 1, pp. 126–136, 2025, doi: 10.1016/j.jds.2024.09.017.
- [62] F. Sun, L. B. Xu, S. X. Lai, H. Xu, X. C. Li, and Z. Lin, "Effect of platform design of dental implant abutment on loosening and fatigue performance," Eng. Fail. Anal., vol. 168, no. November 2024, 2025, doi: 10.1016/j.engfailanal.2024.109134.
- [63] H. S. Ryu, C. Namgung, J. H. Lee, and Y. J. Lim, "The influence of thread geometry on implant osseointegration under immediate loading: A literature review," J. Adv. Prosthodont., vol. 6, no. 6, pp. 547–554, 2014, doi: 10.4047/jap.2014.6.6.547.
- [64] C. Cucinelli, M. S. Pereira, T. Borges, R. Figueiredo, and B. Leitão-Almeida, "The Effect of Increasing Thread Depth on the Initial Stability of Dental Implants: An In Vitro Study," Surgeries (Switzerland), vol. 5, no. 3, pp. 817–825, 2024, doi: 10.3390/surgeries5030065.
- [65] P. A. da Costa Ward, F. Ward, M. F. R. P. Alves, C. R. Moreira da Silva, L. P. Moreira, and C. dos Santos, "Numerical analysis of the mechanical behavior of ceramic dental implants based on Ce-TZP/Al2O3 composite," J. Mech. Behav. Biomed. Mater., vol. 150, no. June 2023, 2024, doi: 10.1016/j.jmbbm.2023.106335.
- [66] G. A. F. Silva, F. Faot, A. P. da R. Possebon, W. J. da Silva, and A. A. Del Bel Cury, "Effect of macrogeometry and bone type on insertion torque, primary stability, surface topography damage and titanium release of dental implants during surgical insertion into artificial bone," J. Mech. Behav. Biomed. Mater., vol. 119, no. March, 2021, doi: 10.1016/j.jmbbm.2021.104515.
- [67] L. S. Colepícolo et al., "Comparative analysis of a conventional cantilever abutment and innovative double abutment in dental implant prosthesis: A finite element analysis study," Biomed. Eng. Adv., vol. 9, no. December 2024, p. 100151, 2025, doi: 10.1016/j.bea.2025.100151.
- [68] N. G. A. Willemen et al., "From oral formulations to drug-eluting implants: using 3D and 4D printing to develop drug delivery systems and personalized medicine," Bio-Design and Manufacturing, vol. 5, no. 1. pp. 85–106, 2022. doi: 10.1007/s42242-021-00157-0
- [69] K. Yokoyama, T. Ichikawa, H. Murakami, Y. Miyamoto, and K. Asaoka, "Fracture mechanisms of retrieved titanium screw thread in dental implant," Biomaterials, vol. 23, no. 12, pp. 2459–2465, 2002, doi: 10.1016/S0142-9612(01)00380-5.
- [70] A. Sahi and S. Gali, "Effect of implant systems in differing bone densities on peri-implant bone stress: A 3 dimensional finite element analysis," Mater. Today Proc., vol. 50, pp. 1300–1307, 2021, doi: 10.1016/j.matpr.2021.08.231.
- [71] M. R. Niroomand, M. Arabbeiki, and G. Rouhi, "Optimization of thread configuration in dental implants through regulating the mechanical stimuli in neighboring bone," Comput. Methods Programs Biomed., vol. 231, 2023, doi: 10.1016/j.cmpb.2023.107376.
- [72] Q. Zhong, Z. Zhai, Z. Wu, Y. Shen, and F. Qu, "Thread design optimization of a dental implant using explicit dynamics finite element analysis," pp. 1–19, 2025.
- [73] C. Erbel, M. W. Laschke, T. Grobecker-Karl, and M. Karl, "Preclinical Performance of a Novel Dental Implant Design Reducing Mechanical Stress in Cortical Bone," J. Funct. Biomater., vol. 16, no. 3, pp. 1–10, 2025, doi: 10.3390/jfb16030102.
- [74] C. L. Chang, J. J. Chen, and C. S. Chen, "Using optimization approach to design dental implant in three types of bone quality A finite element analysis," J. Dent. Sci., vol. 20, no. 1, pp. 126–136, 2025, doi: 10.1016/j.jds.2024.09.017.
- [75] A. Abdulrahman, I. Mutlu, Y. Kisioglu, and E. Mohamed, "The Effect of V-Thread and Square Thread Dental Implants on Bone Stresses," J. Biomimetics, Biomater. Biomed. Eng., vol. 60, no. June, pp. 83–96, 2023, doi: 10.4028/p-3qasy2.
- [76] S. El Refaiy Fouda, H. Hamed, H. Fattouh, and M. Atef, "Evaluation of Insertion Torque and Initial Stability of Tapered Threaded Implant Depending on Apical Portion Design Solid Implant Versus Core-Vent Versus Double Grooves Design an in Vitro Study," Egypt. Dent. J., vol. 68, no. 1, pp. 145–157, 2022, doi: 10.21608/edj.2021.95307.1787.
- [77] J. Duyck, H. J. Rønold, H. Van Oosterwyck, I. Naert, J. Vander Sloten, and J. E. Ellingsen, "The influence of static and dynamic loading on marginal bone reactions around osseointegrated implants: An animal experimental study," Clin. Oral Implants Res., vol. 12, no. 3, pp. 207–218, 2001, doi: 10.1034/j.1600-0501.2001.012003207.x.
- [78] M. Satpathy et al., "Screening dental implant design parameters for effect on the fatigue limit of reduced-diameter implants," Dent. Mater., vol. 41, no. 4, pp. 444–450, 2025, doi: 10.1016/j.dental.2025.02.001.
- [79] A. D. Schwitalla, M. Abou-Emara, T. Spintig, J. Lackmann, and W. D. Müller, "Finite element analysis of the biomechanical effects of PEEK dental implants



ISSN: 2321-9653; IC Value: 45.98; SJ Impact Factor: 7.538

Volume 13 Issue VII July 2025- Available at www.ijraset.com

on the peri-implant bone," J. Biomech., vol. 48, no. 1, pp. 1-7, Jan. 2015, doi: 10.1016/j.jbiomech.2014.11.017.

- [80] A. R. Khan, N. S. Grewal, C. Zhou, K. Yuan, H. J. Zhang, and Z. Jun, "Recent advances in biodegradable metals for implant applications: Exploring in vivo and in vitro responses," Results Eng., vol. 20, no. October, p. 101526, 2023, doi: 10.1016/j.rineng.2023.101526.
- [81] M. H. Mobarak et al., "Recent advances of additive manufacturing in implant fabrication A review," Appl. Surf. Sci. Adv., vol. 18, no. September, p. 100462, 2023, doi: 10.1016/j.apsadv.2023.100462.
- [82] D. Shukla, Y. S. Negi, J. Sen Uppadhyaya, and V. Kumar, "Synthesis and modification of poly(ether ether ketone) and their properties: A review," Polym. Rev., vol. 52, no. 2, pp. 189–228, 2012, doi: 10.1080/15583724.2012.668151.
- [83] I. I. Preobrazhenskii and V. I. Putlyaev, "3D Printing of Hydrogel-Based Biocompatible Materials," Russ. J. Appl. Chem., vol. 95, no. 6, pp. 775–788, 2022, doi: 10.1134/S1070427222060027.
- [84] M. Hussain, S. M. Khan, M. Shafiq, and N. Abbas, "A review on PLA-based biodegradable materials for biomedical applications," Giant, vol. 18, 2024, doi: 10.1016/j.giant.2024.100261.
- [85] T. D. Ngo, A. Kashani, G. Imbalzano, K. T. Q. Nguyen, and D. Hui, "Additive manufacturing (3D printing): A review of materials, methods, applications and challenges," Compos. Part B Eng., vol. 143, no. February, pp. 172–196, 2018, doi: 10.1016/j.compositesb.2018.02.012
- [86] J. Knaus, D. Schaffarczyk, and H. Cölfen, "On the Future Design of Bio-Inspired Polyetheretherketone Dental Implants," Macromol. Biosci., vol. 20, no. 1, Jan. 2020, doi: 10.1002/mabi.201900239.
- [87] A. Schwitalla and W. D. Müller, "PEEK dental implants: A review of the literature," Journal of Oral Implantology, vol. 39, no. 6. pp. 743–749, Dec. 2013. doi: 10.1563/AAID-JOI-D-11-00002.
- [88] B. Łosiewicz, P. Osak, D. Nowińska, and J. Maszybrocka, "Developments in Dental Implant Surface Modification," Coatings, vol. 15, no. 1, 2025, doi: 10.3390/coatings15010109.
- [89] A. Samran, A. W. Hashem, S. Ali, M. Al-Akhali, S. Wille, and M. Kern, "Influence of post material and ferrule thickness on the fracture resistance of endodontically treated premolars: A laboratory study," J. Prosthet. Dent., vol. 133, no. 1, pp. 194–201, 2024, doi: 10.1016/j.prosdent.2024.01.022.
- [90] F. Suska et al., "Enhancement of CRF-PEEK osseointegration by plasma-sprayed hydroxyapatite: A rabbit model," J. Biomater. Appl., vol. 29, no. 2, pp. 234– 242, 2014, doi: 10.1177/0885328214521669.
- [91] A. Pandey and V. Pratap Singh, "Advancement in PEEK Properties for Dental Implant Applications: An Overview," Int. Res. J. Eng. Technol., 2021, [Online]. Available: www.irjet.net
- [92] G. A. El-Awadi, "Review of effective techniques for surface engineering material modification for a variety of applications," AIMS Mater. Sci., vol. 10, no. 4, pp. 652–692, 2023, doi: 10.3934/MATERSCI.2023037.
- [93] S. Najeeb, Z. Khurshid, S. Zohaib, and M. S. Zafar, "Bioactivity and osseointegration of PEEK are inferior to those of titanium: A systematic review," Journal of Oral Implantology, vol. 42, no. 6. Allen Press Inc., pp. 512–516, Dec. 01, 2016. doi: 10.1563/aaid-joi-D-16-00072.
- [94] S. Najeeb, Z. Khurshid, J. P. Matinlinna, F. Siddiqui, M. Z. Nassani, and K. Baroudi, "Nanomodified Peek Dental Implants: Bioactive Composites and Surface Modification - A Review," Int. J. Dent., vol. 2015, 2015, doi: 10.1155/2015/381759.
- [95] Y. H. Joung, "Development of implantable medical devices: From an engineering perspective," Int. Neurourol. J., vol. 17, no. 3, pp. 98–106, 2013, doi: 10.5213/inj.2013.17.3.98.
- [96] S. Najeeb, Z. Khurshid, J. P. Matinlinna, F. Siddiqui, M. Z. Nassani, and K. Baroudi, "Nanomodified Peek Dental Implants: Bioactive Composites and Surface Modification - A Review," International Journal of Dentistry, vol. 2015. Hindawi Publishing Corporation, 2015. doi: 10.1155/2015/381759.











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