iJRASET
International Journal For Research in Applied Science and Engineering Technology



INTERNATIONAL JOURNAL FOR RESEARCH

IN APPLIED SCIENCE & ENGINEERING TECHNOLOGY

Volume: 5 **Issue:** XI **Month of publication:** November 2017

DOI: http://doi.org/10.22214/ijraset.2017.11104

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International Journal for Research in Applied Science & Engineering Technology (IJRASET)
ISSN: 2321-9653; IC Value: 45.98; SJ Impact Factor:6.887
Volume 5 Issue X1, November 2017- Available at www.ijraset.com

"Nonlinear Flexural behavior of Post Tensioned Beam"

Ajinkya S. Dixit[1], V.G. Khurd2
[1]*Student of P.G., M.E. Civil,-Structure Sanjay Ghodawat Institutions, Atigre,Shivaji University, Kolhapur, India*
[2]*Assistant Professor, Civil Engg. Department, Sanjay Ghodawat Institutions, Atigre, Shivaji University, Kolhapur, India*

Abstract: Analysis of a post tensioned concrete beam or determination of physical properties such as deflection, stress distribution under a two-point loading. For analysis purpose ANSYS V15.0 package program is used as a Finite Element Analysis tool. The main objective of this study was to develop three dimensional finite element modeling (3D-FEM) of Post Tensioned Concrete Beam that can be used to investigate the nonlinear response. The accuracy of the results obtained from nonlinear static analysis using ANSYS is validated by comparing it with previous literature study.
Keywords: 3D-FE, static analysis,

I. INTRODUCTION

Concrete structural components exist in buildings and bridges in different forms. Understanding the response of these components during loading is crucial to the development of an overall efficient and safe structure. In Prestressed concrete members, stresses are induced during the construction in such a way that they can resist stresses caused by externally applied loads. Prestressed concrete is most suitable for long span structural elements like beams and girders, where larger bending moment results in greater depth of beam or girder. (Chouragade, M., 2013)

Experimental based testing has been widely used as a means to analyze individual elements and the effects of concrete strength under loading. While this is a method that produces real life response, it is extremely time consuming, and the use of materials can be quite costly. **(**Kasat, A.S., and Varghese, V., 2012). There are a number of approaches for the study of the behaviour of concrete structures, viz., experimental, numerical, theoretical, etc. Finite Element Analysis (FEA) is a numerical one which provides a tool that can accurately simulate the behaviour of concrete structures. (Joshuva, N. R.,et al., 2014)

The use of computer software to model structural elements is much faster, and extremely cost-effective. To fully understand the capabilities of finite element computer software, one must look back to experimental data and simple analysis

II. DETAILING OF POST TENSIONED CONCRETE BEAMS

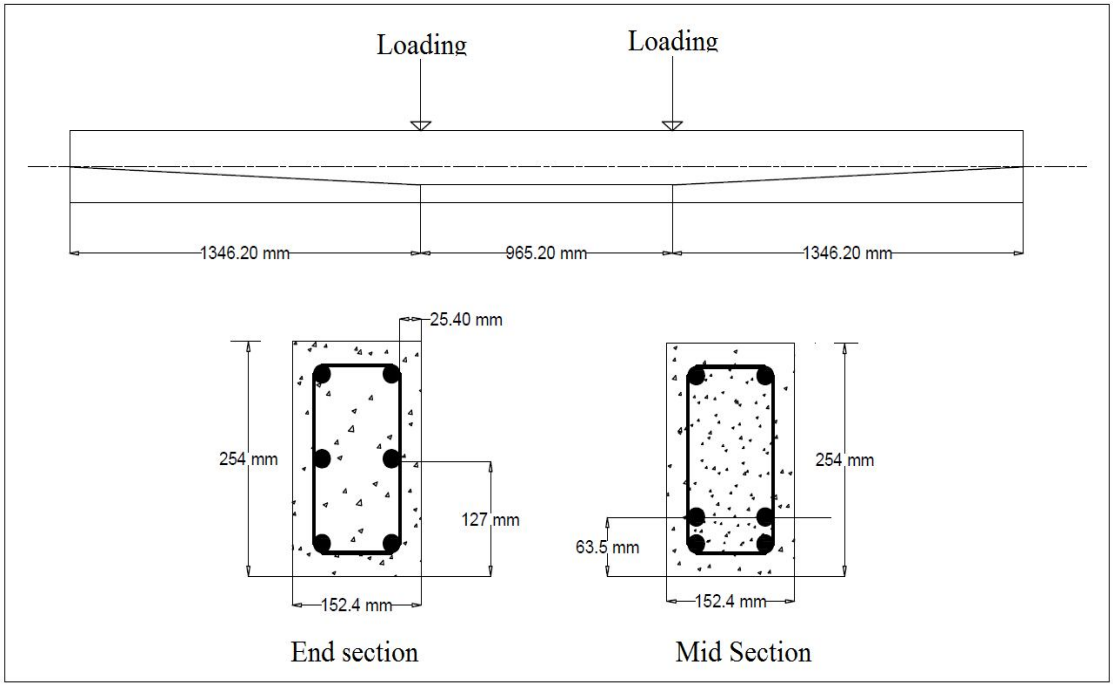


Figure 1.typical detail for post-tensioned concrete beams (Kim, U., et al. 2010,)

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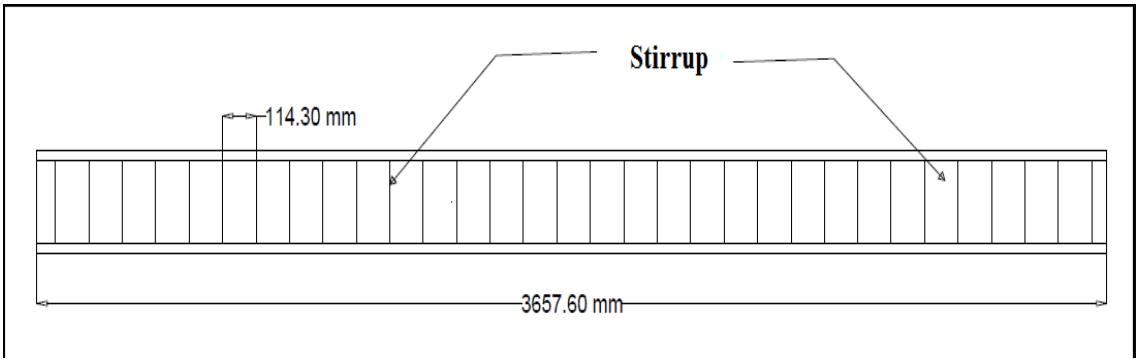


Figure 2. Stirrup detail for post-tensioned concrete beams (Kim, U., et al. 2010,)

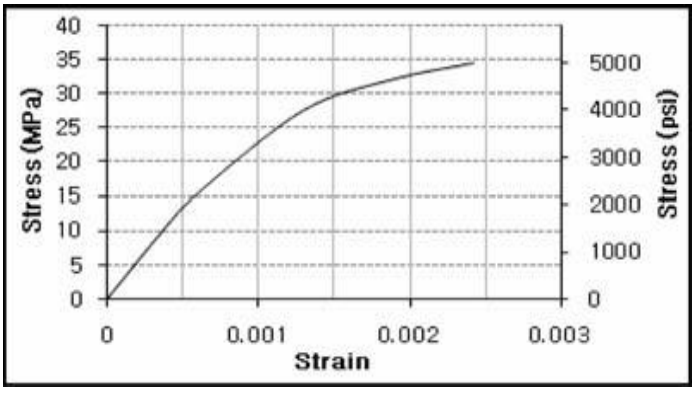
The Post tensioned concrete beams were modeled in ANSYS workbench. The size and loading case is same as mentioned in paper "Nonlinear Finite Element Analysis of Unbonded Post Tensioned Concrete Beam"by Kim, U., Chakrabarti, P. R., & Choi, J. H.,

III. MATERIAL PROPERTIES

The engineering data of new materials for the project can be input or edited in this. M35 grade of concrete and Fe 415 grade of steel is chosen for the beam specimens. ANSYS automatically defines the material properties as per the selected grade of concrete steel, and high tension wire.In the longitudinal direction, 2 numbers of 9.53mm diameter rods were used in the tension side and 2 numbers of 9.53mm diameter rods were used in the compression side. 5.43mm stirrups at 140mm c/c were used in the transverse direction. The steel for the finite element models has been assumed to be an elastic-perfectly plastic material and identical in tension and compression.

Table1. Properties of strands, stirrups and concrete

Properties of strands, stirrups and concrete.	
Area of Strands	23.2 mm^2
Ultimate Strength of Prestressing Strand	1862(MPa)
Area of Stirrups	71mm^2
Yield Strength of Stirrup, fy, (MPa) Compressive Strength of Concrete, f 'c,	414(MPa) 32.4(MPa)

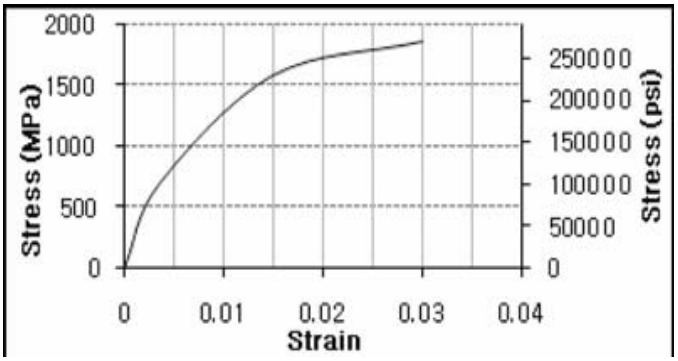


Graph 1.Compressive Uniaxial Stress-Strain Relationship for Concrete

This section explains the material properties of the post-tensioned concrete beams. The complete stress-strain history for concrete subjected to uniaxial compression provides data for use in characterizing the response of concrete to general loading Graph 1 shows the stress-strain curve of the concrete. The value used for the uniaxial tensile cracking stress of concrete was 3.6 MPa (520 psi). During the analysis, if the tensile stress was over 3.6 MPa, cracking would begin to appear. The ANSYS model of the beam specimens with reinforcement is shown in Figure 1 and 2

Material properties of the strands were input as multi-linear isotropic material properties. Graph 2 illustrates the stress-strain curve of the strands.

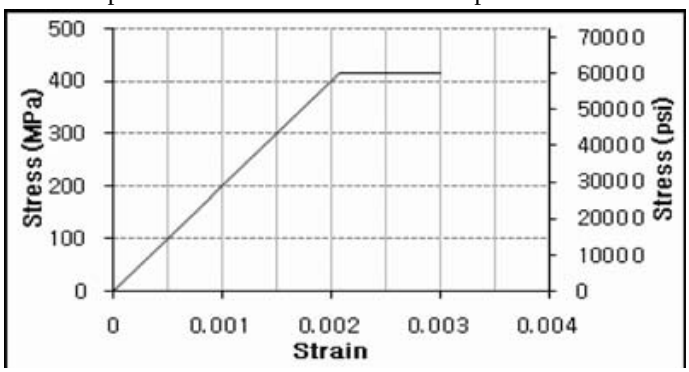
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Graph 2. Stress strain curve for high tensioned wire

For prestressed concrete member's high strength steel generally of wires, bars or strands. The wires which are individually or in wire cables are generally from 3 to 8mm in diameter. The strands which are used in nominal diameter from 10 to 44 mm

Graph 3.Stress-Strain Curve for Stirrup and Rebar



Graph 3.Stress strain curve forstirrups and rebar's

Graph 3 shows the stress-strain curve of the stirrups and rebar's as bilinear isotropic material properties. The stress-strain behavior for concrete steel bar and high tensioned wire was given as per paper. Normalized stress-strain values were calculated by dividing each stress value by the peak stress and dividing each strain value by strain at peak stress. From the normalized stress-strain values of mixes, the average normalized stress-strain curves obtained. The software allows us to define stress-strain diagrams, to control the linear or non-linear behavior of the material and to select the activation time of the material.

IV. MODELLING OF THE STRUCTURE

For the analysis, the post tensioned beam is being modelled as shown in figure. The beam is simply supported at the ends. Before modeling the structure, it is important to define the unit's system that is going to be used. The unit system used will be the following:

a) Length: meter (m) b) Force: Kilo-Newton (KN)

The beam is located in the X-Z plane. And longitudinal length is along the Y direction. The gravity loads act along the Z direction. Hence deflection and bending moments are along Z direction respectively. As shown in figure 3

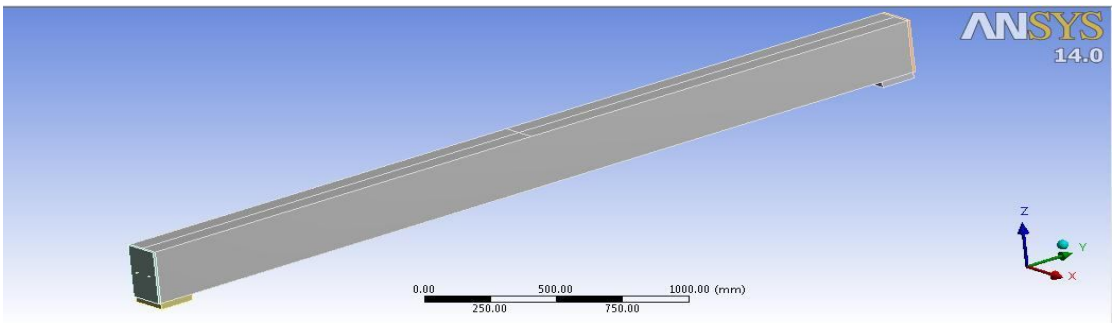


Figure 3. Post tensioned concrete beam model

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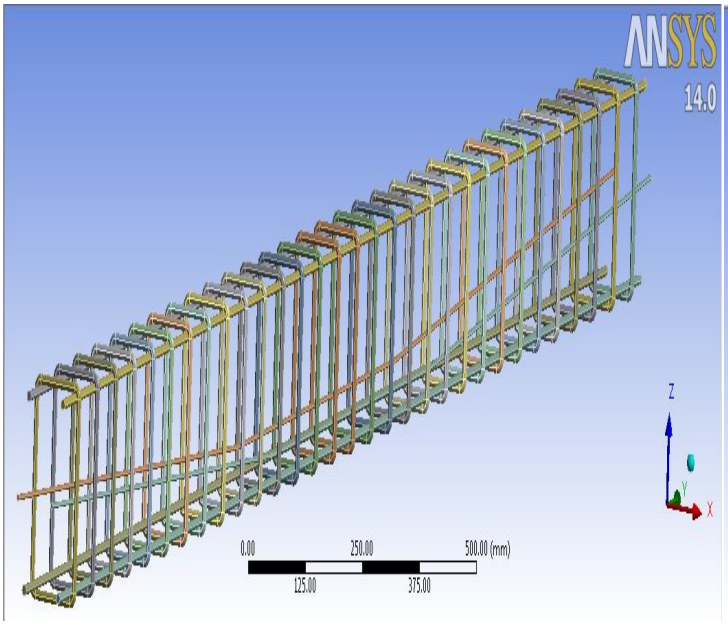


Figure 4. Stirrups, Bars and Wire connection

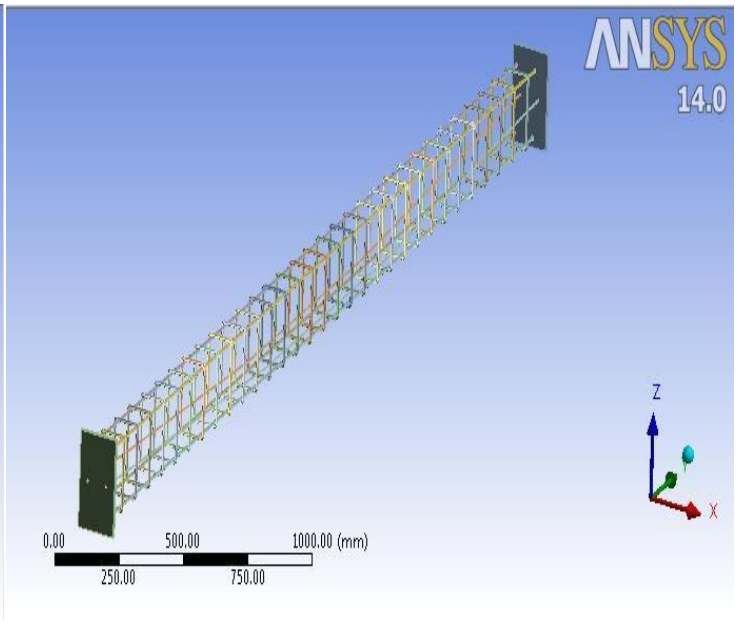
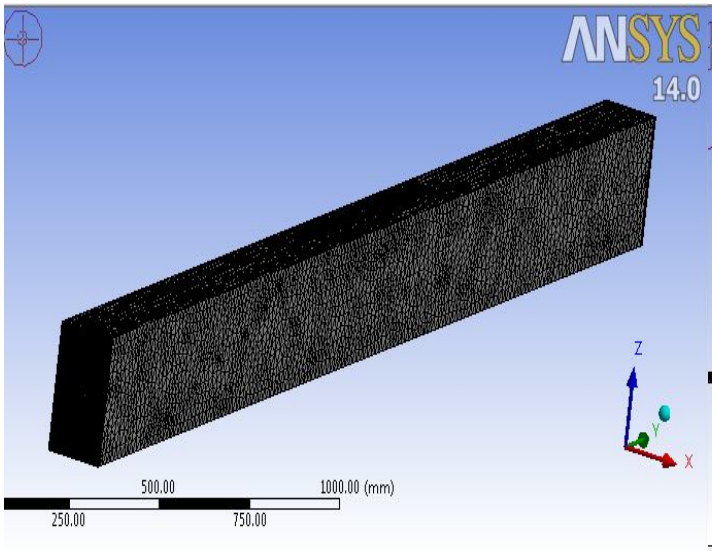


Figure 5. Placement of Stirrups, Bars and Wire connection

A. Finite Element Discretization



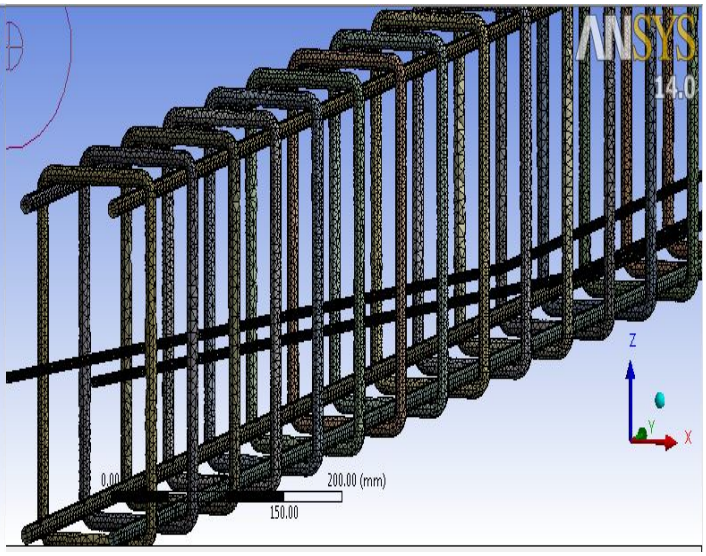


Figure6. Meshing with 4 noded tetrahedral elementFigure 7. Meshing of bar stirrup and wire

A finite element analysis requires meshing of the model. An important step in finite element modelling is the selection of the mesh density. A convergence of results is obtained when an adequate number of elements are used in a model. This is practically achieved when an increase in the mesh density has a negligible effect on the results. This properly sets the width and length of elements in the plates to be consistent with the elements and nodes in the concrete portions of the model.

The numbering control command is used to merge all the items to make it as a single entity. Very fine size was chosen to get more accurate results. The meshed model of the beam specimen is shown in Figure 6 and 7

A 1.0 mesh size was used for this model. Therefore, the concrete beam was meshed with cubes that have the dimensions of 25.4 mm (1.0 in) × 25.4 mm × 25.4 mm. If a mesh size less than 1.0 was used, the convergence would have a high tendency to fail in the analysis. Concrete beam is modelled as 4 noded solid tetrahedron element having 25.4mm element size. The Bars and stirrups are also modelled as 4 noded solid element as shown in figure 4. The wire and concrete connections may be the region of high stress intensity when the prestress load applied, so it requires a precise mesh refinement. Hence a refined mesh is developed at curvature of wire and steel bars. such a representation permits the studying of behavior of post tensioned beam under incremental loading

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V. BOUNDARY CONDITIONS

Boundary conditions are required to get a proper solution for the model. Displacement boundary conditions were assigned similar to the experimental set up so as to constrain the model to get a unique solution. One end of the beam had hinged support and the other end had a roller support as shown in figure 8 below

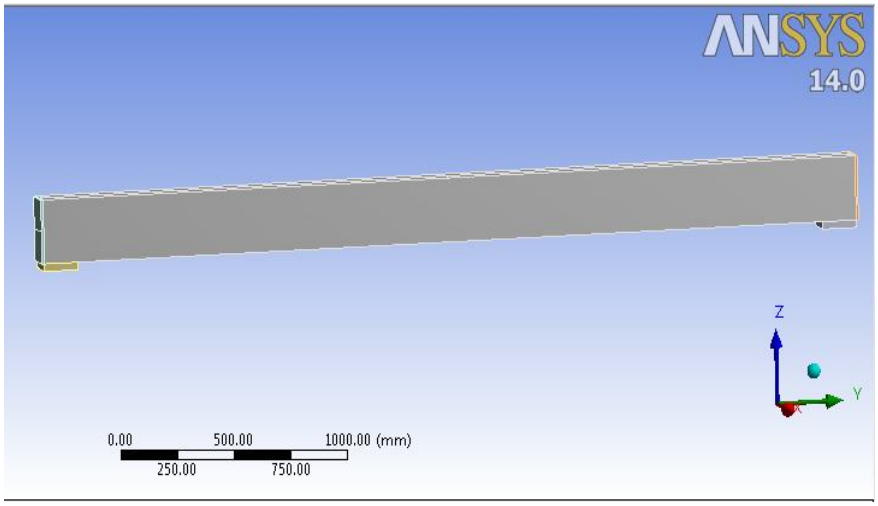


Figure8. Boundary condition

The finite element model of the beam with loads is shown in Figure 6 and 8 The analysis type chosen was static. The beam specimens were analyzed at various load increments until failure load

In order for the nonlinear analysis to be done accurately, the loads are required to have a gradual application, and the nonlinear analysis also requires handling of solution controls. Two point loadings were applied in small incremental loads on beam using the load step and sub step

A. Load steps, Sub steps and Time

For a nonlinear analysis, the total load is subdivided into a series of load increments and applied. A typical load history has been described in terms of loadsteps, substeps and time. At the completion of each solution for the given incremental load, the stiffness matrix of the model is adjusted to reflect the nonlinear (incrementally linear) changes in structural stiffness before proceeding to the next load increment. gradual application, and the nonlinear analysis also requires handling of solution controls. Two point loadings were applied in small incremental loads on beam using the load step and sub step The automatic time stepping facility available in the ANSYS software package is utilized to predict and control the loadstep sizes. Table 2 and Table 3 shows the Solution control for obtaining nonlinear response of beam.

Table2. Basic Solution Control

Analysis options	Small displacement
Calculate prestress effects	Off
Automatic time stepping On	On
Time at end of loadstep	0
Number of substeps	50
Max no. of substeps	100
Min no. of substeps	10
Write items to results file	All solution items
Frequency	Write every Substeps

The applied loads are automatically determined in response to the current state of the analysis under consideration gaining a better balance between accuracy and economy. The maximum and minimum loadstep sizes are required for the automatic timestepping. In this study, the maximum and minimum loadstep sizes are determined depending upon the behavior of reinforced concrete beam under loading. Just before cracking of concrete, the load step sizes need not be small. As Cracking of concrete starts, the solution

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becomes difficult to converge. So The loads are applied gradually with small load increments. The Automatic time stepping will bisect the load until it is equal to the minimum load step size

In order for the nonlinear analysis to be done accurately, the loads are required to have a gradual application, and the nonlinear analysis also requires handling of solution controls

Table3. Nonlinear convergence for solution control.

DOF solution predictor	Program chosen
Maximum number of iteration	20
Equiv. plastic strain	0.15
Explicit creep ration	0.1
Implicit creep ration	0
Incremental displacement 1	10,000,000
Set convergence criteria	Force convergence
Reference Value	1.6
Tolerance	0.05
Min. Ref	−1

Two point loadings were applied in small incremental loads on beam using the loadstep and sub step as shown in figure 9 and 10

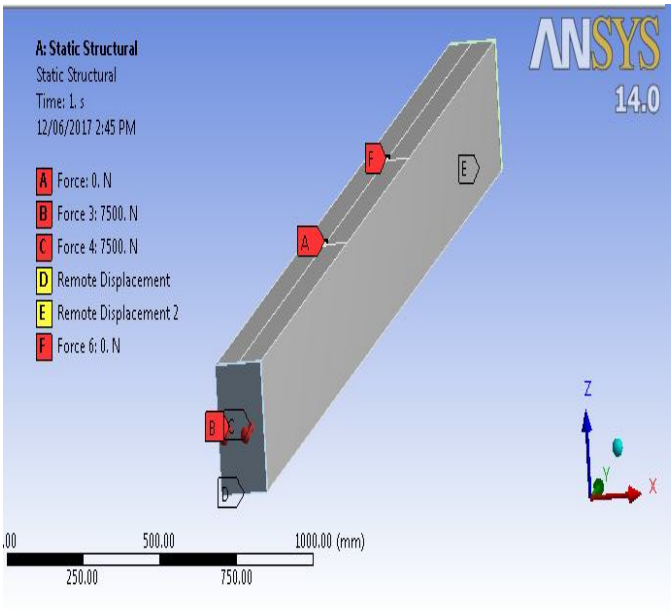


Figure 9. Loading applied on beam in case I

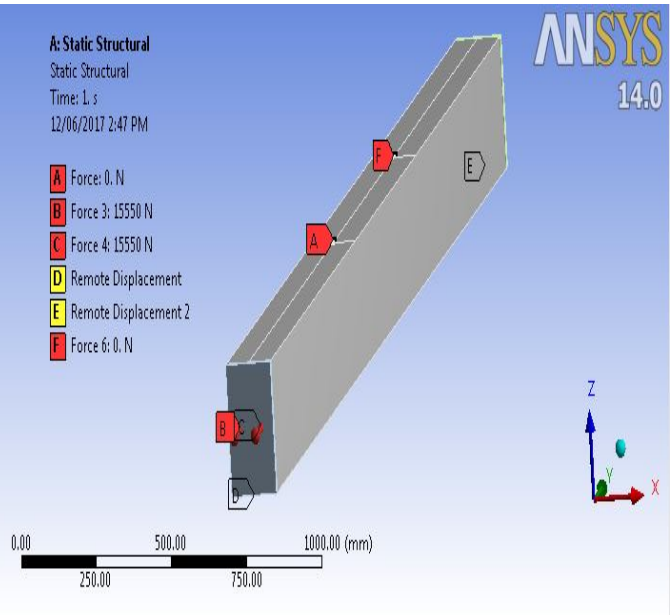


Figure 10. Loading applied on beam in case II

For obtaining the nonlinear solution for given loading in analysis setting result is setfor large deflection on and solution is run for nonlinear solution control.

VI. DETERMINATION OF NONLINEAR FLEXURAL RESPONSES OF BEAM

In nonlinear analysis, the total load applied to a finite element model is divided into a series of load increments called load steps. At the completion of each incremental solution, the stiffness matrix of the model is adjusted to reflect nonlinear changes in structural stiffness before proceeding to the next load increment. The ANSYS program uses Newton Raphson equilibrium iterations for updating the model stiffness. Newton-Raphson equilibrium iterations provide convergence at the end of each load increment within tolerance limits. Prior to each solution, the Newton-Raphson approach assesses the out-of-balance load vector, which is the difference between the restoring forces (the loads corresponding to the element stresses) and the applied loads. Subsequently, the program carries out a linear solution, using the out-of-balance loads, and checks for convergence. If convergence criteria are not satisfied, the out-of-balance load vector is re-evaluated, the stiffness matrix is updated, and a new solution is attained. This iterative procedure continues until the problem converges

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A. By Using Software

The beam is pinned at one end and roller support. Since all material properties, cross sectional properties, loads and boundary conditions have been defined, the beam can now be analyzed. The software ANSYS gave the following results.

Loading –load increment is as below prestressing force -31.1KNprestressing force -15.1KN

Table 4. load increment I

S.r No	Incremental load	Prestressing force(KN)
1	18,014N	31.1KN
2	26,243N	31.1KN
3	34,250N	31.1KN

Loadingcase1-For1st model

Table 5. load increment II

S.r No	Incremental load	Prestressing force(KN)
1	15,568N	15.1KN
2	23,130N	15.1KN
3	28956N	15.1KN

Loading case 2 -For 2nd model

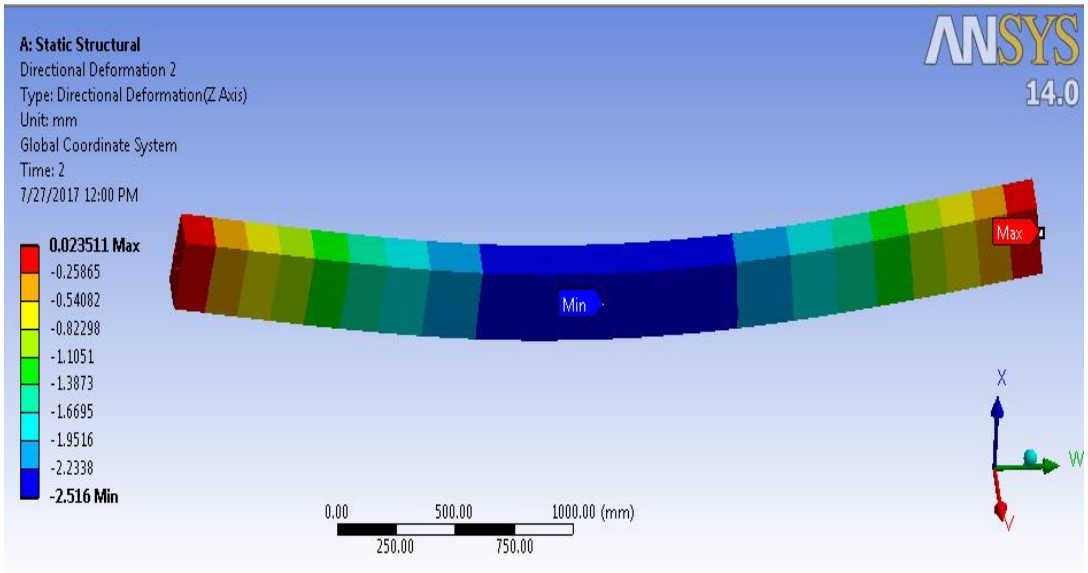


Figure 11. Deflection of beam for loading 18,014N and prestressing force 31.1KN

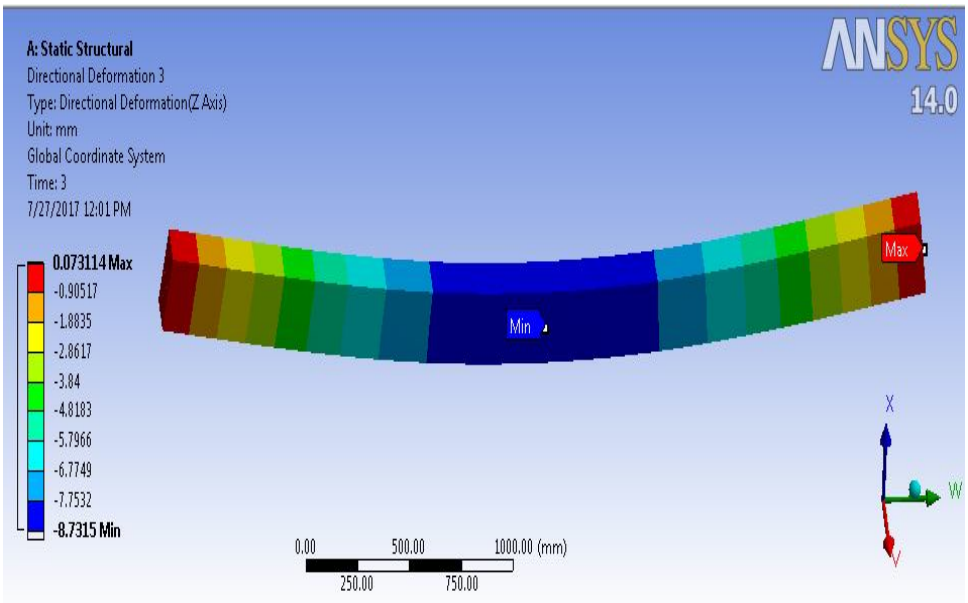


Figure 12. Deflection of beam for loading 26, 243N and prestressing force 31.1KN

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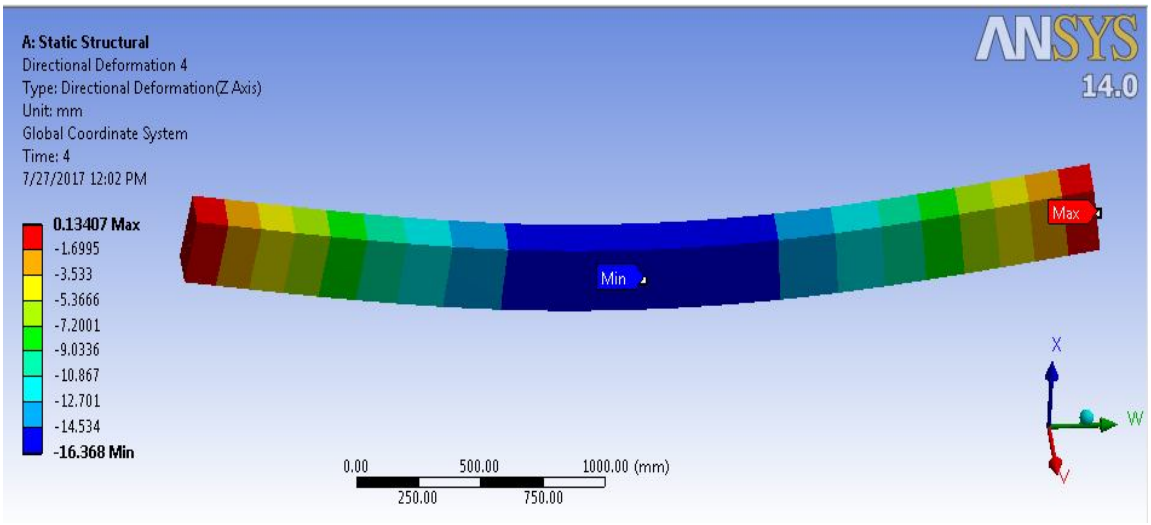


Figure 13. Deflection of beam for loading 34,250N and prestressing force 31.1KN

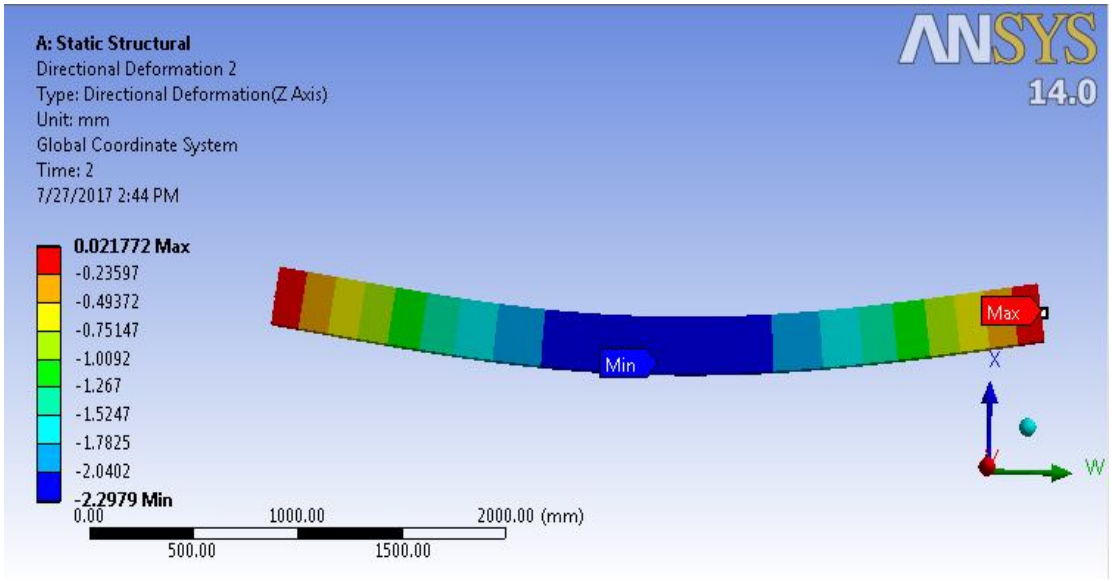


Figure 14. Deflection of beam for loading 15,568N and prestressing force 15.1KN

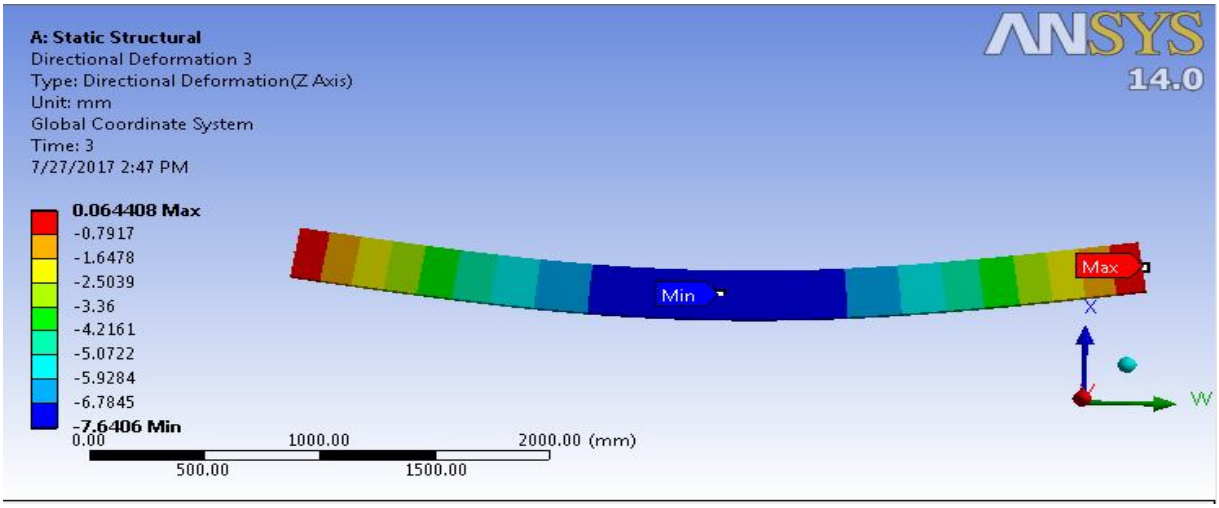


Figure 15. Deflection of beam for loading 23,130N and prestressing force 15.1KN

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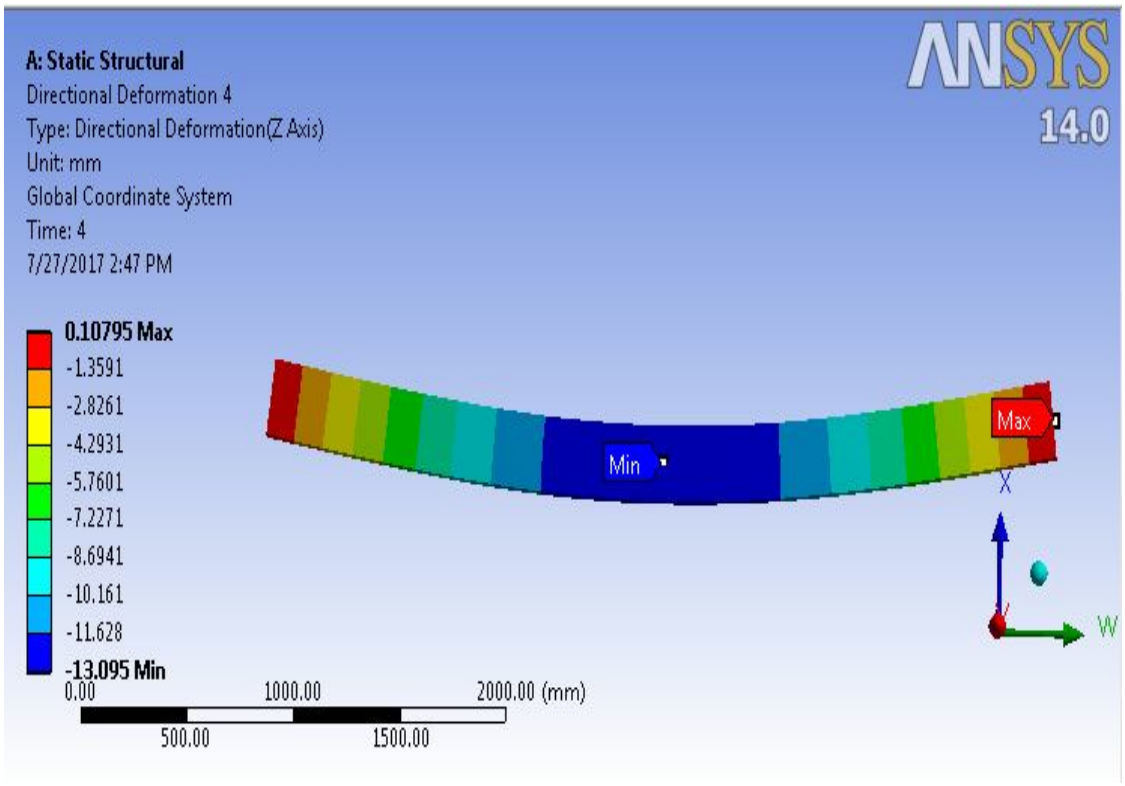


Figure 16. Deflection of beam for loading 28956N and prestressing force 15.1KN

VII. COMPARISON OF DEFLECTION OF BEAM WITH PREVIOUS STUDY

In previous literature paper "Nonlinear Finite Element Analysis of Unbonded Post Tensioned Concrete Beam "by Kim, U., et al.2010, has developed a sophisticated 3-D finite element model for simulating the nonlinear flexural behavior of unbounded post-tensioned beams, and compared analysis results with experimental results to verify the accuracy of the developed 3-D finite element model, and investigated the effects of various prestressing forces on the flexural behavior of post-tensioned beams. Four post-tensioned beams were tested at the structures laboratory of California State University, Fullerton and the test results were compared with the analysis results obtained using Ansys.

Table 6. Literature result for beam I

Percent difference of load-displacement between actual test and ANSYS for beam I			
Displacement	2.5mm	12.7mm	22.9mm
Load (ANSYS)	18,014	26,243	34250
Load (TEST)	13,122	26,688	33,805
Difference	27.16%	1.67%	1.3%

Beam model I-Prestressing Force -31.1KN

Table 7. Literature result for beam II

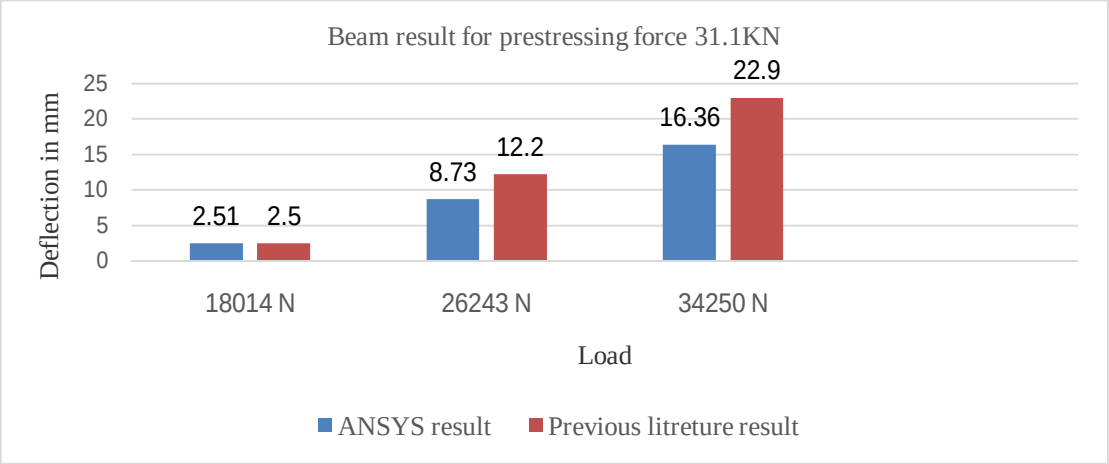
Percent difference of load-displacement between actual test and ANSYS for beam 2			
Displacement	2.5mm	12.7mm	17.9mm
Load (ANSYS)	15,568	23,130	28,956
Load (TEST)	10.008	22,018	27,527
Difference	35.71%	4.81%	4.94%

Beam model II-Prestressing Force -15.1KN

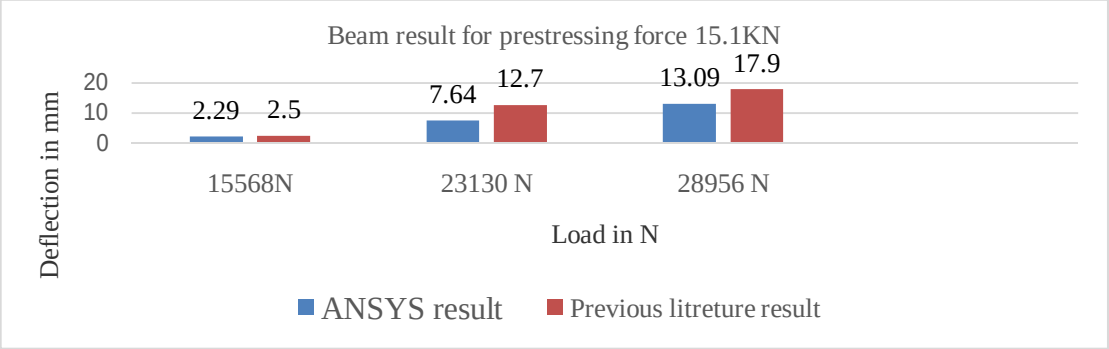
The observation of ANSYS result and previous literature result study is as below

The deflection developed in the post tensioned beam under loading condition are observed for Nonlinear analysis for incremental loading condition to get actual nonlinear response of beam ANSYS solution the obtained result for fully prestressing condition (prestressing force 31.1KN) and partial prestressing condition (prestressing force 15.1KN) are compared and plotted as below

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Graph 4.Comparison of deflection in post tensioned beam between ANSYS and Previous literature result



Graph 5.Comparison of deflection in post tensioned beam between ANSYS and Previous literature result

VIII. CONCLUSION

In the present work, three dimensional finite element analysis of post-tensioned concrete beam using commercial software ANSYS is presented. From study following conclusion can be drawn

The results of the fully prestressing case (31.1 KN) and the partial prestressing force (15.1KN) for post-tensioned concrete beams.

A. Results obtained for nonlinear analysis of post tensioned beam is validated by comparing it with previous literature study. The result reveals the response obtained by Ansys for nonlinear analysis are close to literature study for given loading condition and deflection.

B. The initial behaviour for first loading shows close agreement in deflection than the remaining load cases it was due to difference in convergence criteria for nonlinear analysis and due to mesh density

REFERENCES

[1] Barbosa, A.F., Ribeiro, G.O., “Analysis of reinforced concrete structures using ANSYS nonlinear concrete model” In: Idelsohn, S., Onate, E., and Dvorkin, E. (Eds.), Computational Mechanics: New trends andapplications, pp. 1-7, 1998

[2] Dawari, V. B.,and Vesmawala, G. R., “Application Of Nonlinear Concrete Model For Finite Element Analysis Of Reinforced Concrete Beam” International Journal of Scientific & Engineering Research, Volume 5, Issue 9, September-(2014)

[3] ISSN 2229-5518 Fanning, P., “Nonlinear Models of Reinforced and Post-tensioned Concrete Beams”, Electronic Journal of Structural Engineering,vol 2 (2001), pages (111-119)

[4] Gupta, P. K.,and Khapre, R. N.,“A Study On Development Of Stresses In Anchorage Zone Using Parallel Processing” Asian Journal Of Civil Engineering (Building And Housing) Vol. 9, No. 1 (2008) Pages 47-59

[5] Joshuva, N. R., Saibabu, S., Sakaria, E. P., Lakshmikandhan, K. N., Sivakumar, P., “Finite Element Analysis of Reinforced and Pre-Tensioned Concrete Beams” International Journal of Emerging Technology and Advanced Engineering ,ISSN 2250-2459, Volume 4, Issue 10, (October 2014)

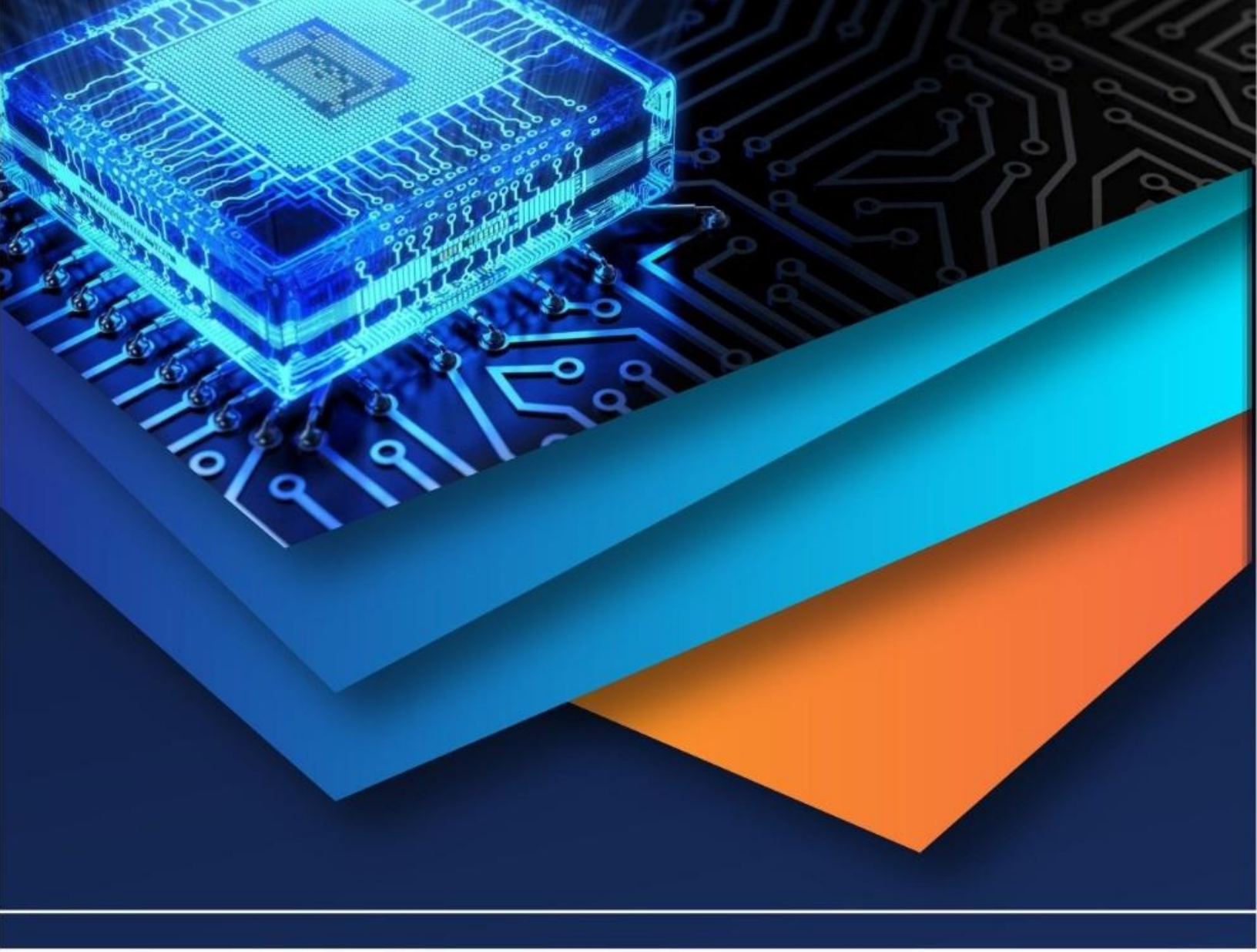
[6] Kaewunruen. S., Remennikov. A., “Nonlinear finite element modelling of railway prestressed concrete sleeper” Faculty of Engineering and information Science 2006

©IJRASET (UGC Approved Journal): All Rights are Reserved

[7] Kang,T., Huang,Y.,"Computer Modeling of Post-Tensioned Structures" International Conference on Computer Modeling and Simulation IPCSIT vol.22 (2012) Singapore
[8] Kasat, A.S., varghese, V., "finite element analysis of prestressed concrete beams" International journal of advanced technology in civil engineering,issn: 2231 –5721, volume-1, issue-3, 2012
[9] Kim, U., Chakrabarti, P. R., & Choi, J. H., "Nonlinear finite element analysis of unbonded post-tensioned concrete beams" Challenges, Opportunities and Solutions in Structural Engineering and Construction – Ghafoori (ed.) 2010 Taylor & Francis Group, London, ISBN 978-0-415-56809-8
[10] Kote, P. B., Patil, S. P., Sangle, K. K.,"Finite Element analysis of Prestressed Beam", International Journal of Advance Foundation and Research in Science & Engineering ,Volume 1, Issue 3, August 2014.
[11] Lou,T., Xiang, Y., "Finite element modeling of concrete beams prestressed with external tendons" Engineering Structures 28 (2006)
[12] Maroliya, M. K., "Comparative Study Of Flexural Behaviour Of Reinforced Concrete Beam And Prestressed Concrete Beam" International Journal of Engineering Research and Applications (IJERA) ISSN: 2248-9622 Vol. 2, Issue 6, November- December 2012,
[13] Markovic, M., Krauberger, N., Saje, M., Planinc ,I., Bratina, S., "Non-linear analysis of pre-tensioned concrete planar beams" Engineering Structures 46 (2013) 279–293
[14] Naghipour, M., Nemati, M., Doostdar,H. M., "Experimental study and modeling of reinforced concrete beams strengthened by post-tensioned external reinforcing bars" International Journal of Engineering Transactions A: Basics Vol. 23, No. 2, April 2010 – 127
[15] Yapar, O., Basu ,p. k., Nordendale N., "Accurate finite element modeling of pretensioned prestressed concrete beams" Engineering Structures 101 (2015) 163–178

A. Standard Codes
1) IS1343, "Code of practice for prestress concrete", Second Revision.
2) IS 456-2000. "Indian Standard Plain and Reinforced Concrete – Code of Practice", Fourth Revision.
B. Books
1) N Krishna Raju "Prestressed Concrete" Fourth Edition Tata McGraw-Hill, New Delhi, 2011
2) S. Ramamrutham "Prestressed Concrete" Fifth Revised and Enlarged Edition

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