iJRASET
International Journal For Research in Applied Science and Engineering Technology



INTERNATIONAL JOURNAL FOR RESEARCH

IN APPLIED SCIENCE & ENGINEERING TECHNOLOGY

Volume: 6 **Issue:** I **Month of publication:** January 2018

DOI: http://doi.org/10.22214/ijraset.2018.1126

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International Journal for Research in Applied Science & Engineering Technology (IJRASET)
ISSN: 2321-9653; IC Value: 45.98; SJ Impact Factor :6.887
Volume 6 Issue I, January 2018- Available at www.ijraset.com

Two Wheeled Self Balancing Vehicle

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Abstract: The main concept and the challenge of two wheeled self balancing vehicle is to bring out the stability of the vehicle. In this paper, the stability is analysed by comparing three types of controller in order to identify the desired stable output. A non-model controller of fuzzy mandian and modelled linear controller of PID and Linear quadratic regulator (LQR) is implemented. A common transfer function is derived from a state space equation of the system model. The same values are implemented in all the controllers to determine the better stability output.
Keywords: Stability, Fuzzy, PID, LQR, state space equation.

I. INTRODUCTION

Two wheel transporter moves from one place to another with simple operation. It is like a scooter but the wheels are parallel to each other. It was first invented by Dean kamen in 2007. It is widely used for its advantages over energy saving, simple structure, safety, consumer acceptance, parking impact and land use. It is a mode of transportation where it can be used by golfers, individual sightseeing, for a short distance travelling which reduces the human walk. The main key factor for this vehicle is stability. As the vehicle is running only in two wheels the stability of the wheel with the cart and the pendulum is must for the movement. For a slight movement of vehicle, it starts to fall down until we control the angle of the cart and the pendulum. It is similar to the operation of inverted Pendulum. In inverted pendulum, it is kept in opposite direction which is of pi angle. And that pendulum should be controlled from falling. The same concept is applied in the two wheeled inverted pendulum. In vehicle it consists of cart and the pendulum. Depending on the movement of the cart the pendulum should be balanced. If a person is travelling in a vehicle he should move front or back in order to balance the vehicle. When a person moves forward the vehicle moves forward, and to run the vehicle backwards the person should lean back words. To move the vehicle left or right the movable steering is connected to the cart. The angle between the pi angle and the deviation of the pendulum is known as pitch angle. And that pitch angle is sensed by the accelerometer and gyroscope. Depending on the capacity of the battery the vehicle distance is determined. These all functions are based on the controller.

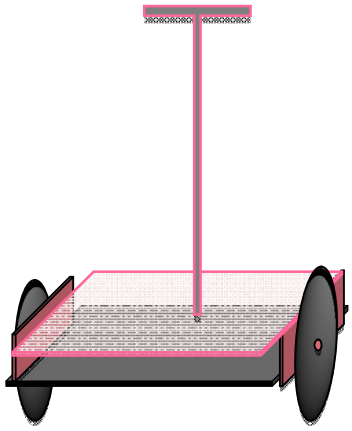
In order to control the vehicle, we use fuzzy, PID and LQR controllers. Even though these controllers are changed period vice, the LQR controller shows the better stability than fuzzy and PID for this system. The system is a non-linear model, it is converted into a linear model using state space equation. By comparing the rise time and settling time of three controller's better stability is determined. The main concept is to reduce the complexity of the mathematical model and to bring out the good stability of the system. They replace the heavy vehicle used for personal short-range transportation. They are eco-friendly and reduces the gasoline consumption, reduces air pollution and consumption of fossil fuels. They are used in both indoor and outdoor environment. This system is carried out in MATLAB/SIMULINK.

II. SYSTEM MODEL

The model has the cart and the pendulum
For simplification, let us assume it is of inverted pendulum attached to a cart.
g = Gravity constant
Ψ = Angle deviation
L = Length of the pendulum
m = Mass of the cart
M = Mass of the pendulum
x = Movement of direction
f = Friction
F_x = Force between cart and pendulum in x direction
F_y= Force between cart and pendulum in y direction

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A. Vehicle Model



Equation of the cart

$F_{input} = m\ddot{x} + f\dot{x} + fx$ ..... (1)

Equation of the pendulum

$F_x = m\ddot{x} + ml\ddot{\Theta}\cos\Theta - Ml\dot{\Theta}^2\sin\Theta$…. (2)

when the force is perpendicular to the pendulum.

$F_y\sin\Theta + F_x\cos\Theta - Mg\sin\Theta = Ml\ddot{\Theta} + M\ddot{x}\cos\ddot{\Theta}$ ……. (3)

Torque acting on the centre of the pendulum is given as

$-F_y l\sin\Theta - F_x l\cos\Theta = I\ddot{\Theta}$ ……. (4)

On combining cart and pendulum equation:

From equations (1) and (2)

$F_{input} = (m+M)\ddot{x} + f\dot{x} + Ml\ddot{\Theta}\cos\Theta - Ml\dot{\Theta}^2\sin\Theta$ ……. (5)

Combining (2) and (3)

$(I + Ml^2)\ddot{\Theta} + Mgl\sin\Theta = -Ml\ddot{x}\cos\Theta$ ……. (6)

B. Linearizing the equations

To determine the transfer function from the equations (5) and (6) for the position x and angle deviation Ψ

$\cos\Theta = \cos(\Pi+\Psi) \approx -1$ ……. (7)

$\sin\Theta = \sin(\Pi+\Psi) \approx -\Psi$ ……. (8)

$\Theta^2 = \Psi^2 \approx 0$ ……... (9)

The linearized equation is from (5), (6), (7), (8), (9)

$(I + Ml^2)\ddot{\Psi} - Mgl\Psi = Ml\ddot{x}$…… (10)

$U = (m + M)\ddot{x} + f\dot{x} - Ml\ddot{\Psi}$…… (11)

Taking Laplace transform for (10) and (11), we get

$(I + Ml^2)\Psi(s)s^2 - Mgl\Psi(s) = MlX(s)s^2$ …… (12)

$u(s) = (m + M)\,X(s)s^2 + f\,X(s)s - Ml\Psi(s)s^2$ …… (13)

From (12)

$X(s) = \left[\frac{I+Ml}{Ml} - \frac{g}{s}\right]\Psi(s)$ ……... (14)

Substitute (14) in (13)

$u(s) = (m + M)\left[\frac{I+Ml}{Ml} - \frac{g}{s}\right]\Psi(s)s^2 + \left[\frac{I+Ml}{Ml} - \right]\Psi(s)s - Ml\Psi(s)s^2$ …… (15)

On rearranging equation (15)

$$\Psi(s) = \frac{\frac{M}{q}s}{s + \frac{f(I+Ml)}{q}s - \frac{(m+M)Mgl}{q}s - \frac{fMgl}{q}}\,u(s)$$

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where,

$q = [(m + M) (I + Ml^2) – (Ml)^2]$

Transfer function for cart position X (s) is

$$X(s) = \frac{(I+Ml)s-gMl}{s + f\left(\frac{I+Ml}{q}\right)s-\frac{(m+M)Mgl}{q}s-\frac{fmpgl}{q}s}\ u(s)$$

In state space method,

$x = A\ x + B\ u$

$y = C\ x + D\ u$

$$\begin{bmatrix} \dot{x} \\ \ddot{x} \\ \dot{\psi} \\ \ddot{\psi} \end{bmatrix} = A \begin{bmatrix} x \\ \dot{x} \\ \psi \\ \dot{\psi} \end{bmatrix}$$

$$A = \begin{matrix} 0 \\ 0 \\ 0 \\ 0 \end{matrix} \begin{bmatrix} 1 & 0 & 0 \\ A22 & A23 & 0 \\ 0 & 0 & 1 \\ A42 & A43 & 0 \end{bmatrix}$$

$$B = \begin{bmatrix} 0 \\ B12 \\ 0 \\ B14 \end{bmatrix}$$

Where,

$$A_{22} = \frac{-(I+Ml2)f}{I\ (m+M)+mMl2}$$

$$A_{23} = \frac{M2gl2}{I(m+M)+mMl2}$$

$$A_{42} = \frac{-Mfl}{I(m+M)+mMl2}$$

$$A_{43} = \frac{Mgl\ (m+m)}{I(m+M)+mMl2}$$

$$B_{12} = \frac{I+Ml2}{I(m+M)+ mMl2}$$

$$B_{14} = \frac{Ml}{I\ (m+M)+mMl2}$$

$$C = \begin{matrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{matrix}$$

$$D = \begin{matrix} 0 \\ 0 \end{matrix}$$

The values for the parameters are given

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Table 1

M(Kg)	M(Kg)	I(Kgm^2)	L(m)	g(m/sec^2)
1.5	0.2	0.055	0.05	9.8

The state space equation of the system is

$$\begin{pmatrix} \dot{x} \\ \ddot{x} \\ \dot{\Psi} \\ \ddot{\Psi} \end{pmatrix} = \begin{pmatrix} 0 & 1 & 0 & 0 \\ 0 & -0.0134 & 95.156 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 1.425 & 180.79 & 0 \end{pmatrix} \begin{pmatrix} x \\ \dot{x} \\ \Psi \\ \dot{\Psi} \end{pmatrix} + \begin{pmatrix} 0 \\ 0.9092 \\ 0 \\ 9.699 \end{pmatrix} u$$

$$Y = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{pmatrix} \begin{pmatrix} x \\ \dot{x} \\ \Psi \\ \dot{\Psi} \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \end{pmatrix} u$$

The transfer function of the system is

$$G(s) = \frac{102s+173.5}{s3+2.64s2-83.60s-307.2}$$

III. DESIGNOFFUZZYCONTROLLER

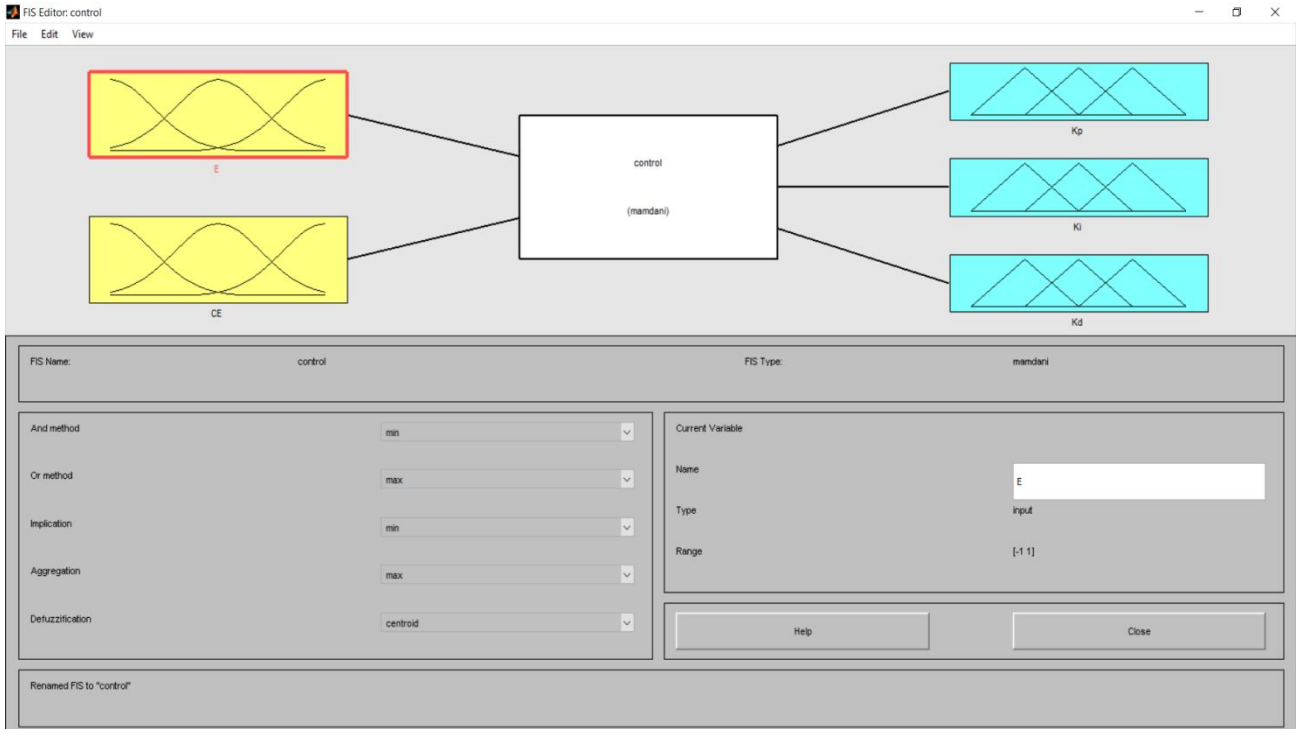
Fuzzy controller is of if, then rules. Values which are implemented are based on assumptions. There are two inputs for fuzzy as error and change in error. Those values are assigned with 7 inputs. The output obtained will be of three outputs, which denotes K_p , K_i, K_d values.

The values assigned for the input and output are

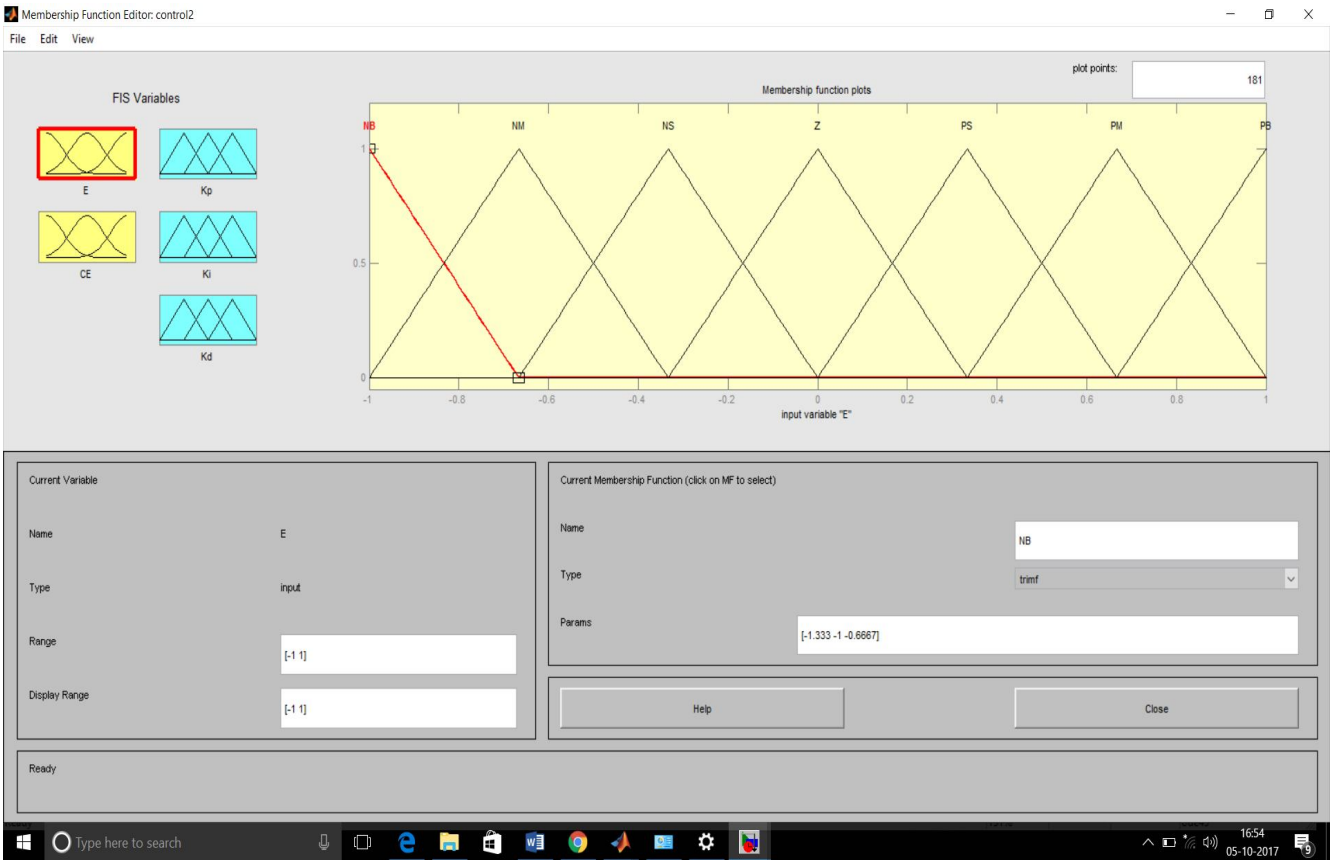
NB - Negative Big
NM - Negative Medium
NS - Negative small
ZO - Zero
PS - Positive Small
PM - Positive Medium
PB – Positive Big

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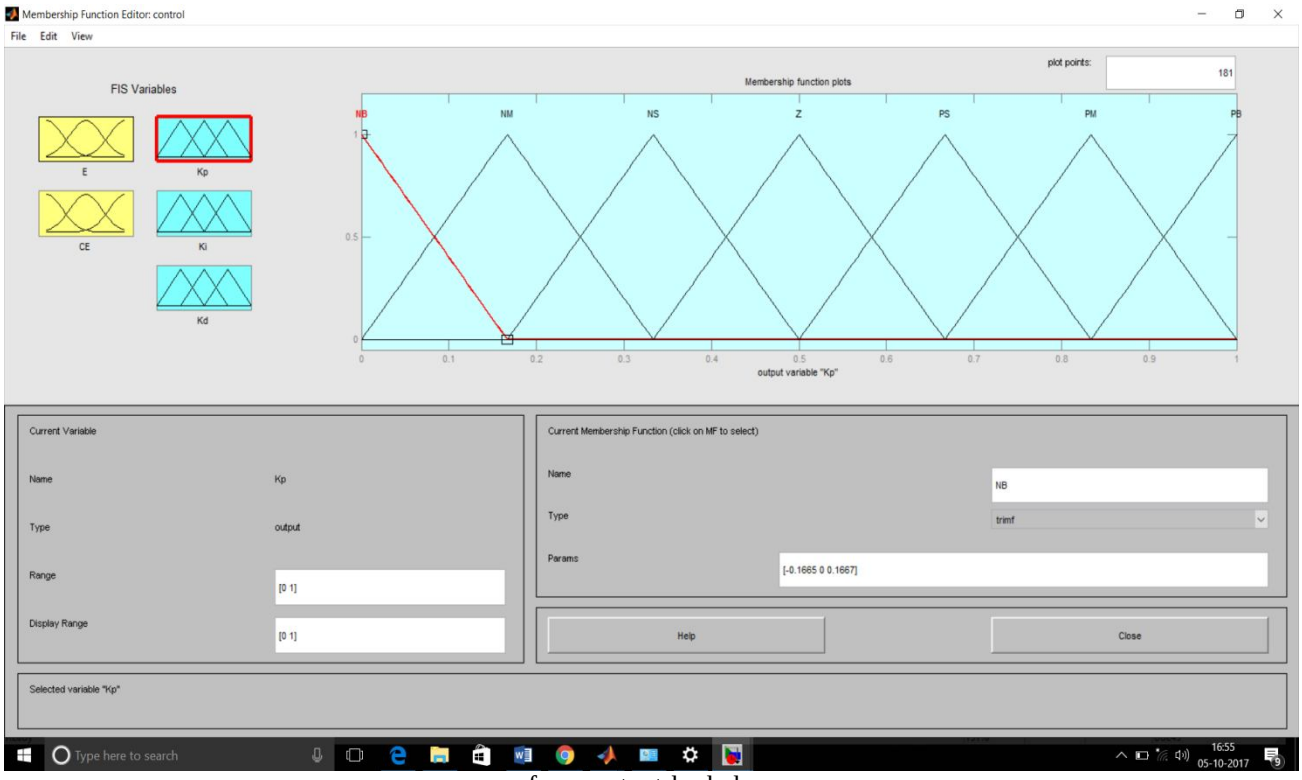


Fuzzy Control Structur

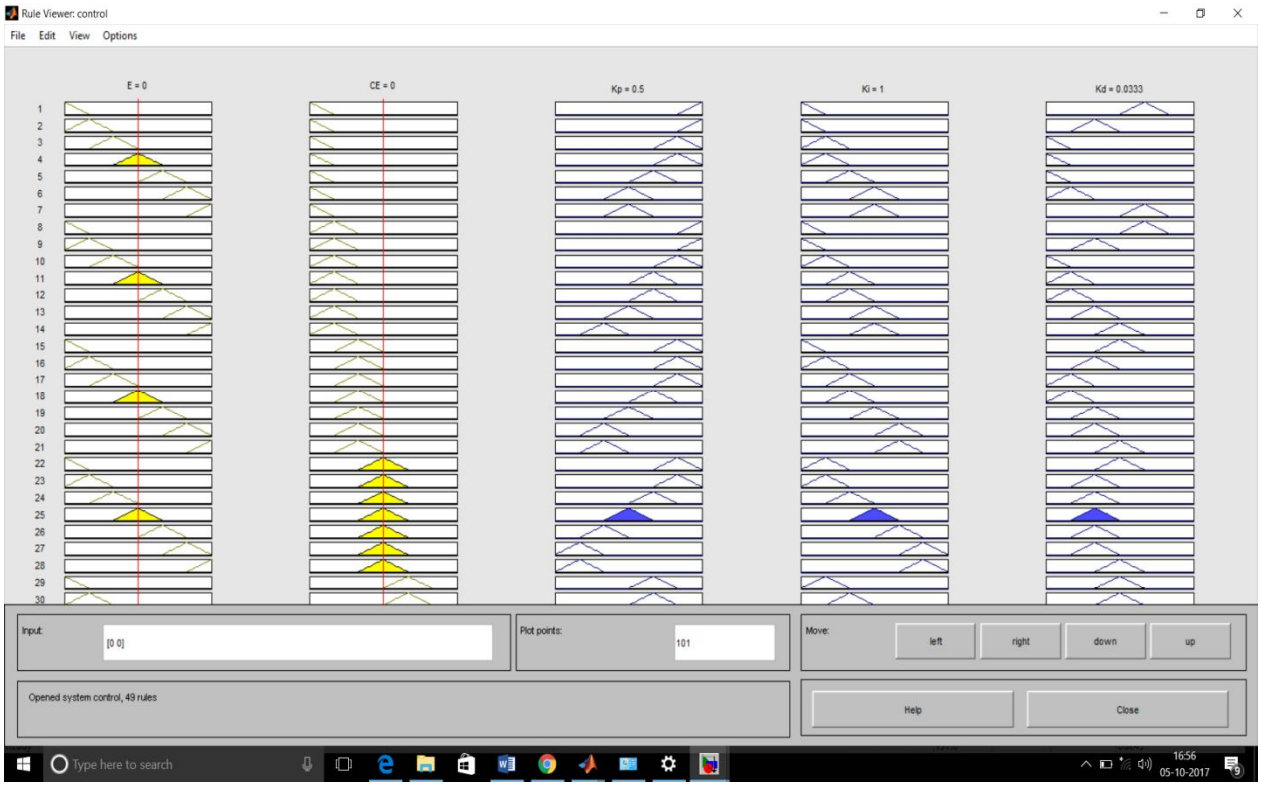


Fuzzy Input-Error And Change In Error

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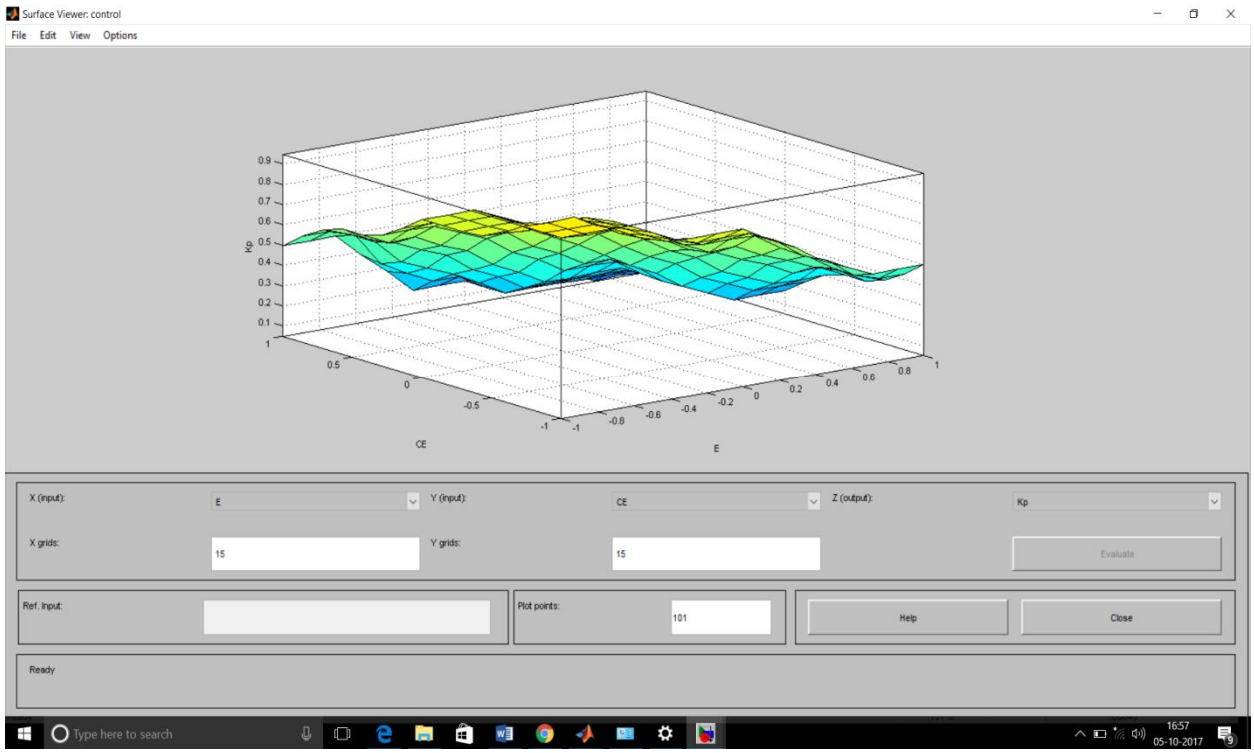
fuzzy output-k_p, k_i, k_d.



Fuzzy Rules

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Surface Output of the Fuzzy

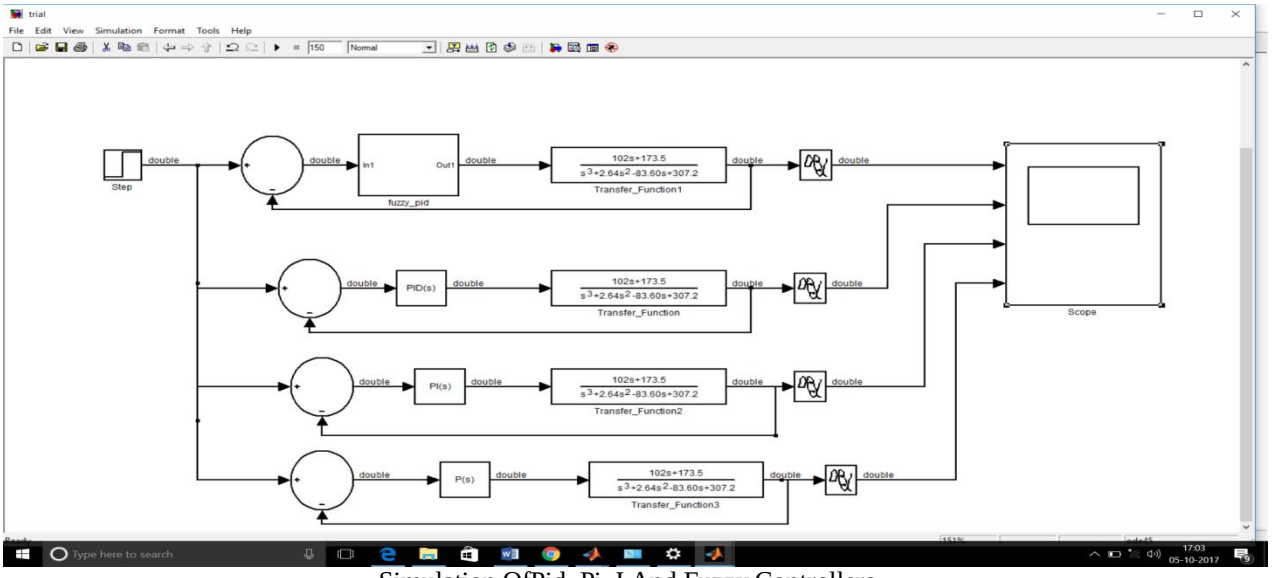
IV. DESIGN OF PID CONTROLLER

In PID controller the proportional, integral and derivative values are given, such that the cart should balance the pendulum. The control equation for PID controller is

$$u(t) = Kp\, e(t) + \frac{1}{Ti}\int e(t)dt + Td\frac{de(t)}{dt}$$

Here,

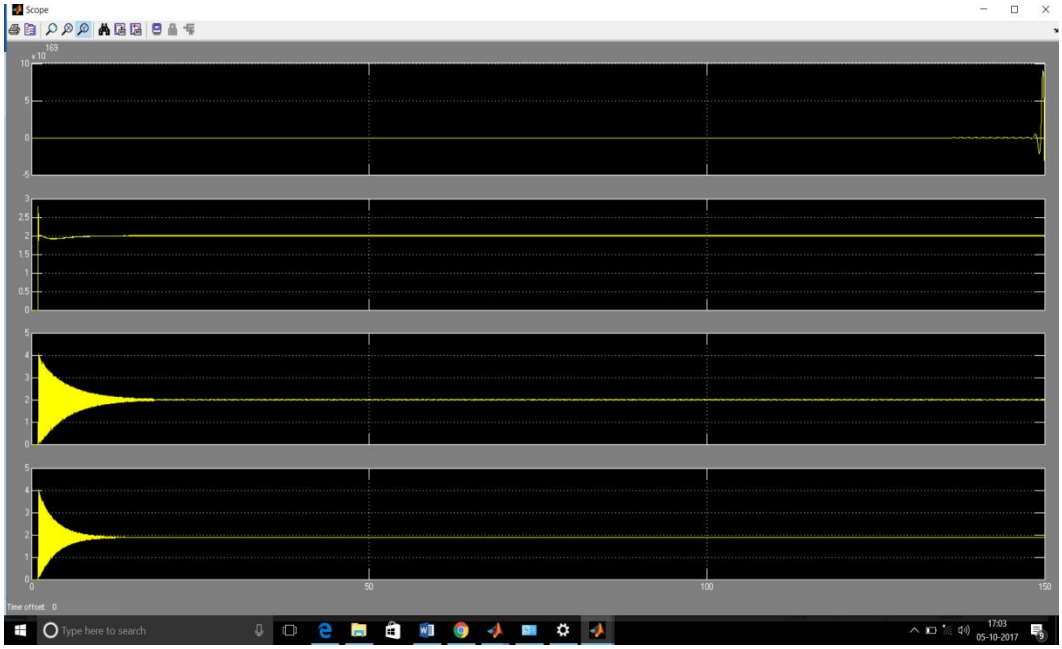
P changes the gain of the system. Increase in K_p value lowers the stability and have larger overshoot. K_i changes the response speed and adjust the time. K_d changes the response speed and the error of the system. Such that the value of the derivative should be greater than integrator. If K_d is too large the system becomes instable.



Simulation OfPid, Pi, I And Fuzzy Controllers

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Output of Fuzzy, Pid, Pi And P Controllers

V. DESIGNOFLQR CONTROLLER

LQR is a linear quadratic regulator. Based on the linear state space mode.

$\dot{x} = Ax + Bu$

and the control law is given as

$u = -Kx$

K = state feedback gain

X=state vector

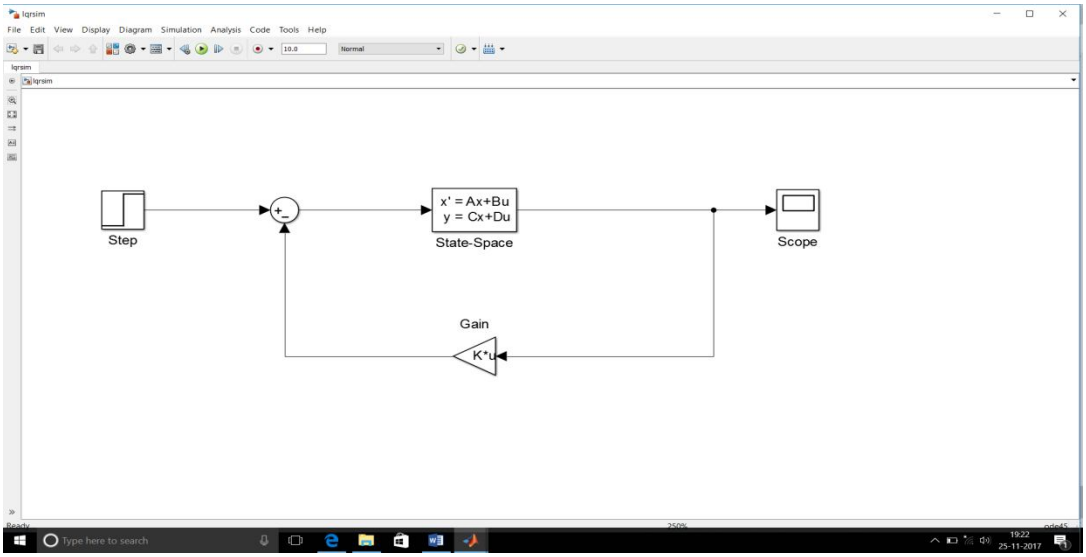
Closed loop state space model of the system is given as

$\dot{x} = (A-BK)x$

Aim of LQR controller is to locate each eigen values of the matrix (A-BK) in the left half of the plane s. such that the dynamic system becomes stable.

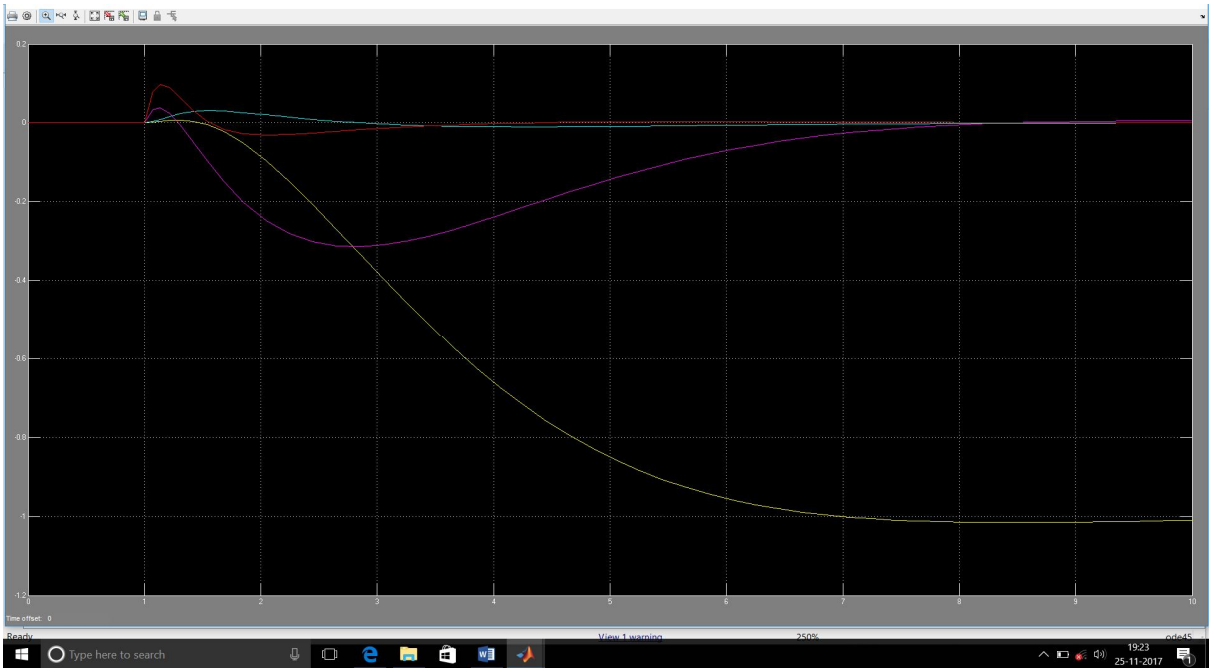
$$J = \frac{1}{2}\int (x^T(t)Q\,x(t)+u^T(t)Ru(t))dt$$

WhereQ = positive semidefinitematrixR = positive value



Simulation OfLqr

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Lqr Output

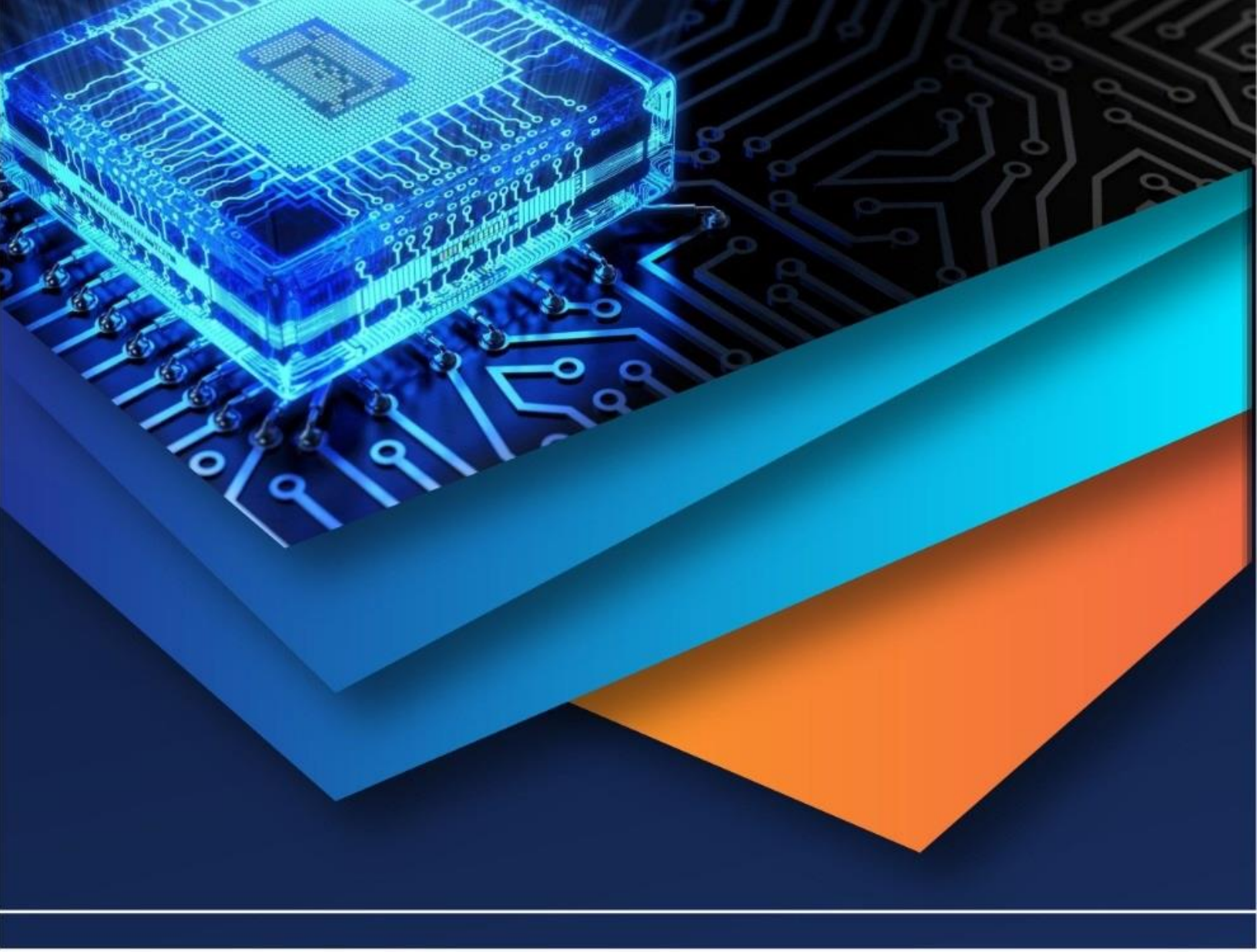
VI. CONCLUSION

The system becomes unstable without the controller. It is necessary to control the system such that by controlling we attain a stable state, which does not make the vehicle fall down. There are many controllers to control the system. But the stability also plays a major role in the system. Such that the controller should be selected in a way that provides a good stability. In this paper the stability of the vehicle is determined by state space equation and it is shown that the output of LQR is more stable than PID and fuzzy.

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