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Sound Assisted Fluidized Bed and its Effects on Micro Particles

M. Shakebuddin¹, Dr. Akash Langde²

¹Research Scholar MIET, Gondia

²Prof. Mechanical department A.C.E.T Nagpur

Abstract: *The aim of this research work is to improve the quality of fluidization of fine powders (cohesive powder) with the help of sound assisted fluidization. The work presents the main results obtained in the field of sound assisted fluidization of fine particles. Our aim is to emphasize on the role of acoustic fields in enhancing the gas-solid contact efficiency, we have characterized the fluidization behavior of bentonite powders in terms of pressure drops, minimum fluidization, bed expansion, and velocity as affected by acoustic fields of different intensity and frequency. Remarkable effect was noted after application of sound intensity with decrease in minimum fluidization velocity and with good bed expansion.*

Keywords: *Fluidization, acoustics, agglomerates, micro particles*

I. INTRODUCTION

Fluidization is the operation by which solid particles are transformed into a fluid-like state through suspension in a gas or liquid. One of the most prominent features of fluidized beds is their ability to mix. According to the fluidization of fine powders (diameter of the primary particles less than 100 μ m) is complex. Due to the cohesive structure and, in particular, to the physical forces between the primary particles it is difficult to suspend these particles in fluidizing gas. This is due to the unpredictable behavior of the cohesive powders. This strong interaction between the powders affects the flow properties of the powders; these tend to form agglomerates of random size and shape by the action of the inter particle forces between the primary particles. In many industrial processes, the cohesive powders are fluidized in the form of agglomerates. For this, it is necessary to break the strong inter particle bond by applying external energy like magnetic pulsation, vibration, acoustic energy and by using binary particles. The smooth fluidizations of gas-solid particles are the result of equilibrium between the hydrodynamic, gravitational and inter particle forces. This is of great importance for many industrial processes.

II. LITERATURE REVIEW

Initially the work is done by Morse [1] who studied the effect of sound on a fluidized bed. During research, the loudspeaker was kept at the bottom of the bed. Sonic energy of sufficient intensity (above 110dB) of low frequency (from 50 to 500Hz) would cause non-easy to fluidize group C particles to fluidize well, so that fluidization is possible without channeling and stagnation.

Chirone et al. [2] formulated the cluster/sub cluster oscillator model based on the theory that the cluster is due to the effect of cohesive Vander Waals forces, which fuse to each other and forms large agglomerates. As a result, the bed has been structured in clusters that can break up into sub clusters, due to the sound intensity.

Nowak et al. [3] Developed the correlation sound assisted minimum fluidization and used the sound at the top as well as bottom of the unit. The measurement was done at variable frequencies and decrease in min. fluidization velocity occurred at 97, 157, and 894Hz. The heat transfer improves characteristic of non-fluidized solid at low acoustic frequency.

Levy et al. [4] determined the effects of acoustic waves in fluidized beds. Sound pressure measurements within the bed showed the presence of acoustic standing waves throughout the bed. According to acoustic standing wave theory, the bed behaves as a 1-D, quasifluid and establish the parameter kh , where k is the wave number and h is the bed depth, determines the amplitude of sound pressure throughout the bed.

Chirone et al. [5] suggested the effect of an acoustic field on different cohesive particles, ranging from 0.3 to 1 μ m up to SPL of 150dB. It was observed that, under electron micro scope the solid showed different particle surface geometries. Sound-assisted aeration promotes to bubble free fluidization. Sound-assisted aeration gave rise to bubble free fluidization only in case of catalyst, ash, and talc. The word aeration instead of fluidization reflects the fact that in spite of the presence of an acoustic field, the gas is unable to flow homogeneously through the bed. A correlation was obtained for bed expansion and fluidizing curve.

Levy et al. [6] investigated the effect of sound intensity on gas-fluidized bed for separation of the bed materials into low and high-density component. The experimentation performed with fly ash particles and showed the strong effect.

Russo et al. [7] reported the effects of bed weight and intensity of the acoustic field (from no sound to sound pressure level-SPL, at 140 dB). The maintained constant frequency 120 Hz in all the experiments. The results of the experiment showed, for a certain bed weight, an acoustic field of appropriate SPL changes the channeling typically observed with group C cohesive powders into the homogeneous bubble free bed.

In his latter studies, Lev yet al. [8] investigated the effect of sound, promoting more homogeneous fluidization and bed expansion. In his study, by using fiber optic probe they found the combined effects of gas frequency, velocity and intensity of sound waves on bubble dynamics..

Xu et al. [9] suggested that, with the assistance of a sound field, fluidization quality of fine particles can be enhanced. By applying sound field results, in higher pressure drop and lower minimum fluidization velocity. In study, application of an acoustic field was attempted to identify Geldart groups C and A particles. For the first time sound field is used to distinguish group C particles from group A particles.

Leu et al. [10] studied the behavior of eight different types of Geldart group C particles in the sound vibrated fluidized bed and estimated the inter particle force.

Guo et al. [11] investigated the fluidization behaviors of ultrafine particles in an acoustic fluidized bed with one type of micron particles and two types of nanoparticles ($d_p = 500\text{nm} - 10.69\text{mm}$).

Xu et al. [12] reported the effects of vibration on fluidization of fine particles (4.8-216 μm average in size) show that the fluidization quality of fine particles can be enhanced under mechanical vibration, leading to larger bed pressure drops at low superficial gas velocities and lower values of U_{mf} .

Levy et al. [13] studied the combined effects of mechanical and acoustic vibrations on fluidization of cohesive power. With the introduction of acoustic and mechanical vibrations, both the minimum fluidization velocity and agglomerate size got reduced. They came to the conclusion that, acoustic vibrations were more effective compared to mechanical vibration.

III. EXPERIMENTAL SETUP

Experiments were performed at room temperature and atmospheric conditions. The fluidization gas was air, provided by an air compressor. The compressor has capacity to deliver the air up to 8 bar. A gate valve was provided to maintain uniform inlet rot meter pressure. The experimental works were carried out on two clear Plexiglas column of inner diameters 100mm and heights of 500mm, respectively. A porous distributor located at the bottom of the column, distributes air uniformly into the bed. Water manometer was used to measure the pressure drop across the distributor and bed.

The sound source includes a sound amplifier, a function signal generator and a loud speaker 8". The speaker was located at the top of the bed to generate sound as the source of acoustic field.

A signal generator was used to produce different types of electric pulse waves. the sound frequency was controlled by simply adjusting the function generator.

The sound pressure level measured with the microphone attached to a movable attachment at the proper height.

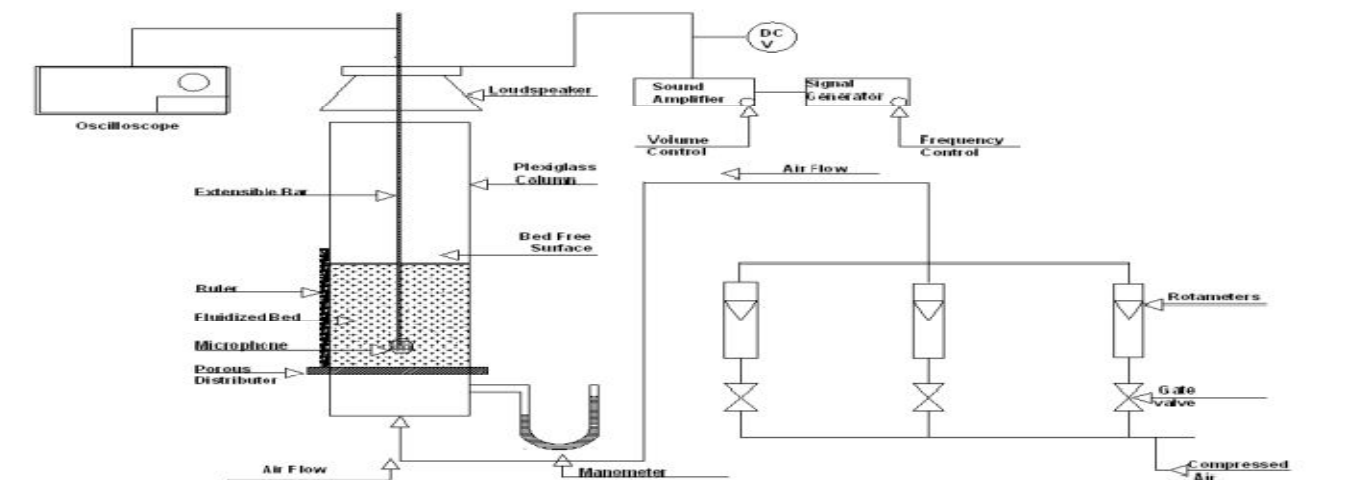


Fig 1 The Experimental Setup

Table 1: Shows the specification of the material used
Sound-assisted fluidization of Bentonite powder

Sr. No.	Name of Material	Mean Diameter “ d_p ”	L/D ratio	Weight of Material (kg)	Density (kg/m^3) “ ρ_p ”	Fluidizing bed diameter “D”	Cohesive/Non Cohesive
1	Bentonite	64 μm	0.7	500gm	980	10 cm	Cohesive

IV. RESULTS AND DISCUSSION

Table 2: Depicts the values of U_{mf} (cm/s) at no sound and sound condition with variation of frequency(Hz) and SPL (dB)

$U_{mf0}=1.5$		U_{mfs}			
		90Hz	120Hz	140Hz	170Hz
	120dB	1.1	1	1.2	1.3
	130dB	1.05	0.9	1.05	1.09
	140dB	0.85	0.8	0.91	0.85
	145dB	0.75	0.72	0.76	0.9

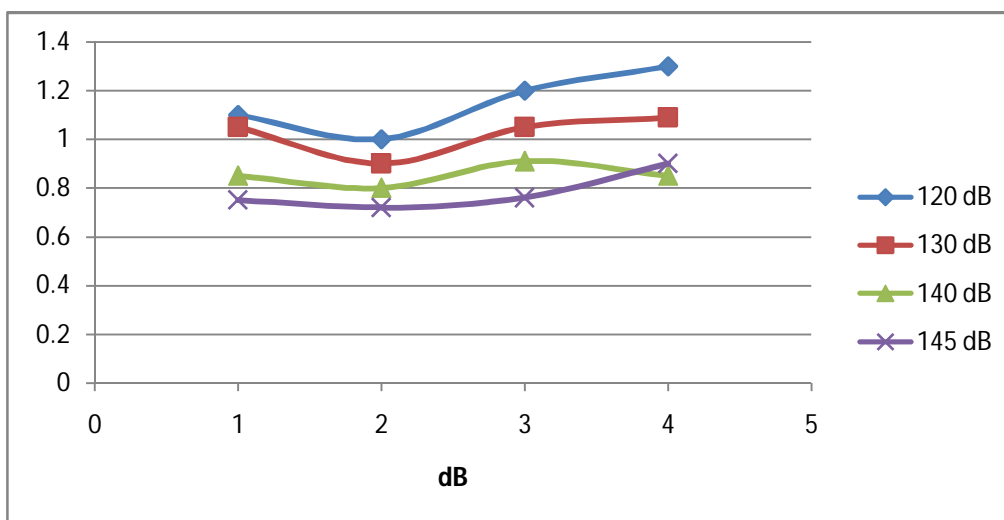


Figure 2 Graph of U_{mf} v/s SPL dB

Table 3: Depicts the values of U_{mf} (cm/s) at no sound and sound condition with variation of frequency(Hz) and SPL (dB)

$U_{mf0}=1.5$		U_{mfs}			
		90Hz	120Hz	140Hz	170Hz
	120dB	1.1	1.05	0.85	0.75
	130dB	1	0.9	0.8	0.72
	140dB	1.2	1.05	0.91	0.76
	145dB	1.3	1.09	0.85	0.9

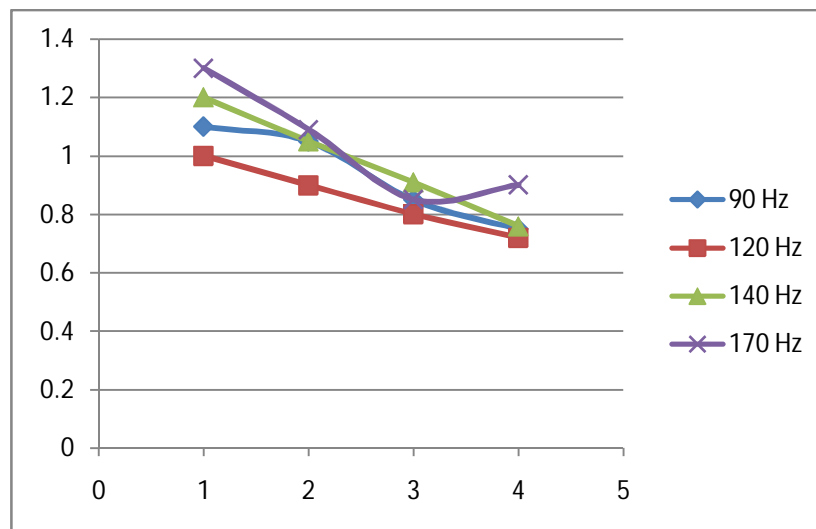
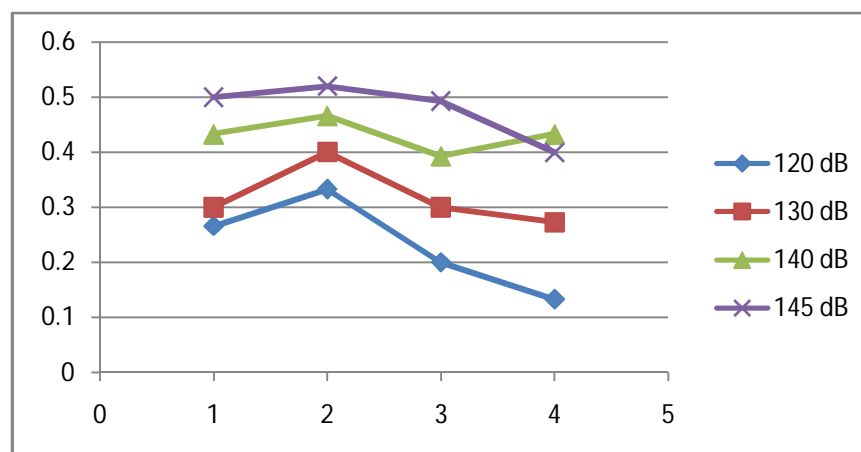


Figure 3 Graph of Umf v/s frequency

Table4: Depicts the values of $(U_{mfo} - U_{mfs})/U_{mfo}$ with variation of frequency(Hz) and SPL (dB)

	(Umfo- Umfs)/Umfo			
	90Hz	120Hz	140Hz	170Hz
120dB	0.266	0.333	0.2	0.133
130dB	0.3	0.4	0.3	0.273
140dB	0.433	0.466	0.393	0.433
145dB	0.5	0.52	0.493	0.4


Figure 4 Graph of $(U_{mfo} - U_{mfs})/U_{mfo}$ v/s SPL(dB)

The characteristic parameter in this case is as follows:

- 1) The bed aspect ratio (L/D) at minimum fluidization, which is related to the total amount bed material.
- 2) The properties of the fluidized bed system which are independent of particle properties. These include
 - a) Fluidized bed dimension, such as the bed diameter and the height.

b) The bed operating conditions such as superficial gas velocities.

Benton idée ($d_p = 64\mu\text{m}$) are difficult to fluidized in absence of sound intensity with elutriation loss at higher gas velocity. When acoustic field was applied their fluidization quality improved with homogeneous fluidization. It was also observed that, material responds to the sound intensity from 120dB.

A. Effect of sound intensity on minimum fluidization velocity

It has been observed that, material with particle size $d_p = 64\mu\text{m}$, gave good response to the sound intensity with decrease in U_{mf} .

B. Effect of sound intensity on minimum bubbling velocity

Minimum bubbling velocity recorded when first bubble appeared on the surface of bed by visual observation. The observation was noticed for most of the material is that, minimum value of U_{mb} seen at 120Hz due to the maximum response of column to this frequency.

C. Bed expansion in presence of acoustic field

It has been also noted that, bed expansion increased with the application of acoustic field. Bed expansion of bentonite gave best response to the sound intensity. The bed expansion was almost twice and small amount of air was sufficient to expand the bed at 145dB.

V. CONCLUSIONS

The remarkable effect was observed, when acoustic field was applied on bentonite powder. Experiment was done on bentonite powder having approximately the size in between the range of $37\mu\text{m}$ to $90\mu\text{m}$. the average size of the particle considered for experiment purpose is $64\mu\text{m}$.

The experimentation is carried out at room temperature and air as fluidizing gas in presence of sound assisted variable acoustic field. The experiment was performed for the L/D ratio of 0.7

As sound intensity increases U_{mf} decreases from 1.1 dB to 0.7 dB. The range of frequencies is between 90Hz and 170Hz. It was also seen that, U_{mf} decreases with increase in frequency and then increases.

The material which was very difficult to fluidized with the supply of high velocity of air flow, fluidized very easily with low velocity of air with the application of acoustic field. It has been also seen that the size of the agglomerates decreases and shows good bed expansion in presence of acoustic field.

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