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Study on RC Jacketed Rectangular Column under Axial load

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Abstract: One strategy for the jacketing of reinforced concrete column is to target the improvement of local vulnerabilities in columns related to inadequate strength (compressive & Flexural) or poor ductility. Theoretical analysis have been carried out in the present study for different column sections of jacket thickness of 75mm and 100mm for jacketed RC columns subjected to axial compressive loading for rectangular column. The axial load carrying capacity along the major axes has been carried out under balanced section condition. Linear static finite element analysis has been carried out for the jacketed RC columns to compare the confined concrete strength (fcc) of finite element analysis with that of theoretical analysis, to plot the variation of stresses at the central core concrete and at the interface of old and new concrete. The displacements at core with respect to both major and minor axis are also plotted. Considerations have been given for variations in the properties of different types concretes used in the jacket and the original column. In order to find out the increase in the confined capacity of jacketed columns due to strengthening with respect to original column, theoretical analysis has been carried out.

Keywords: axial load, NISA Display IV, Jacketing, confined compressive strength.

I. INTRODUCTION

Reinforced concrete is a composite in which steel reinforcement bars ("rebar's"), reinforcement grids, plates or fibers have been incorporated to strengthen the concrete. It was invented by French Joseph Monier in 1849 and patented in 1867. The term Ferro Concrete refers to concrete that is reinforced with iron or steel. Other materials used to reinforce concrete are organic and inorganic fibers as well as composites in different forms. Concrete is strong in compression, but weak in tension, thus adding reinforcement increases its strength in tension. In addition, the failure strain of concrete in tension is so low that the reinforcement has to hold the cracked sections together.

II. OBJECTIVES OF THE PRESENT STUDY

- A. The Primary Objectives of the Present Study are
- 1) To find the confined and unconfined capacity of the jacketed RC columns subjected to axial load using the method based on Sheikh and Usurer's model.
- 2) To obtain the strength gain factor K using the confined and unconfined capacity for Axial loaded columns for rectangular columns.

III. METHODOLOGY

To study the variation of stresses at the central core concrete, at the interface of old and new concrete and at the column surface and lateral displacement along the length of the column, first theoretically calculate the axial compression convert it to the pressure and apply that load on the FEM model and execute it. Then plot the variation of stresses and displacement. Then also compare the increases in the confined capacity of jacketed columns with respect to the original column



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Table 1: Dimensions of rectangular columns for Axial load (Both Theoretical and FE M Analysis)

		Percentage of steel		Longitudinal Steel Provided	
				Original	Jacketed
Column Dimension	Spacing	Original	Jacketed	column	column
		Column	Column		
				,	(number and
				diameter of	diameter of main
				main bars)	bars)
					0.11.5
230x230	100				8#16
230x300	150	20/	10/		4#16+8#12
		-	_	9#20	111010112
300x450				8#20	12#12
		_	area		
300x600		Column			16#25
					12#25
450x600	300				12#25
	230x230 230x300 300x450 300x600	230x230 100 230x300 150 300x450 200 300x600 250	Column Dimension Spacing Original Column 230x230 100 230x300 150 2% gross area of original column 300x450 200 original column	Column Dimension Spacing Original Column Jacketed Column 230x230 100 2% gross area of original column 1% gross jacketed area 300x450 200 original column area	Column Dimension Spacing Original Column Jacketed Column Original column 230x230 100 2% gross area of 300x450 1% gross jacketed original column 8#20 300x600 250 column 8#20

A. Theoretical Analysis of Jacketed RC Axial Rectangular Columns

The method based on Sheikh and Usurer's has been used for the theoretical analysis of jacketed RC column subjected to axial load. The grade of the original column concrete considered is 25MPa and that of jacket concrete are 30MPa. From below table it can be noticed that in case of rectangular columns of different dimensions the confined capacity of jacketed column, strength gain factor(k) and confined concrete strength (fcc) decreased considerably as the spacing of bars increased. In turn the unconfined capacity of jacket column remains constant irrespective of varied spacing and thickness of jacket.

Table 2: Comparison of axial compression component of original and jacketed column

		100mm jacket, 1	6#25, fci=25, fco=30Mpa		Confined
Column Dimension (mm)	Spacing (mm)	Confined capacity of Jacketed column (KN)	Unconfined capacity of Jacketed column(KN)	Strength gain factor (K)	concrete Strength (fcc) in MPa
230x300	100	10433.82	5806.55	1.79	39.98
230x300	150	10397.93	5806.55	1.79	38.98
230x300	200	10347.88	5806.55	1.78	37.59
230x300	250	10280.91	5806.55	1.77	35.73
230x300	300	10204.47	5806.55	1.75	33.61
230x450	100	12488.99	7569.05	1.65	40.36
230x450	150	12445.62	7569.05	1.64	39.63
230x450	200	12383.89	7569.05	1.63	38.58
230x450	250	12285.38	7569.05	1.63	36.95
230x450	300	12123.08	7569.05	1.60	34.23
300x450	100	14103.90	8776.55	1.60	40.83
300x450	150	14070.35	8776.55	1.60	40.44
300x450	200	14027.65	8776.55	1.59	39.95
300x450	250	13970.96	8776.55	1.59	39.29



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300x450	300	13893.71	8776.55	1.58	38.39
300x600	100	16599.18	10801.55	1.53	40.95
300x600	150	16560.77	10801.55	1.53	40.63
300x600	200	16512.67	10801.55	1.52	40.23
300x600	250	16448.98	10801.55	1.52	39.70
300x600	300	16360.53	10801.55	1.51	38.96

B. Finite Element Modeling

Finite element modelling is described as the representative of the geometrical model in terms of a finite number of elements and nodes, which are the building blocks of the numerical representation of the model. In addition to information about elements and nodes, model also contains information about material and other properties, loading and boundary conditions. The most important step in the finite element method of structural analysis is to generate, using finite number of discrete elements, a mathematical model which should be as near as possible equivalent to the actual continuum. Such a formation of a model is referred to as structural idealization or discretization. The geometrical and material properties of the jacketed RC columns considered for analysis are given in below table.

Table 3: Geometrical and material properties

Original column dimensions (mm)	230x230, 230x300, 230x450, 230x600, 300x300, 300x450, 300x600			
Column height (m)	3			
Jacket thickness (mm)	50, 75 and 100			
Original column concrete				
Modulus of Elasticity(MPa)	22360, 25000 and 27386			
Poisson's ratio	0.15			
Jacketing concrete				
Modulus of Elasticity(MPa)	27386 and 31623			
Poisson's ratio	0.15			
Longitudinal Reinforcement				
Modulus of Elasticity(MPa)	200000			
Poisson's ratio	0.3			
Stirrups				
Modulus of Elasticity(MPa)	200000			
Poisson's ratio	0.3			

C. 3-d Models for Square and Rectangular column of Axial Loaded Column

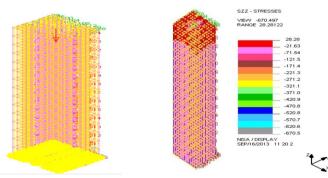


Fig 1: Modelling of jacketed RC column the

Fig 2: Isometric view of normal stress distribution in jacketed RC column



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Table 4: FCC Results of Axial Loaded Rectangular Column

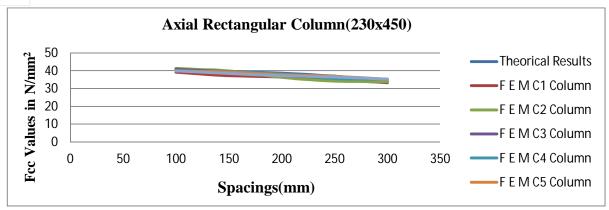
Column Section	Spacing	Confined concrete strength (fcc) in MPa values		
		100mm jacket, 16#25, fci=25, fco=30Mpa		
230x300	100	39.38		
230x300	150	37.98		
230x300	200	36.49		
230x300	250	34.85		
230x300	300	34.23		
230x450	100	39.13		
230x450	150	37.24		
230x450	200	36.45		
230x450	250	35.13		
230x450	300	33.18		
300x450	100	39.45		
300x450	150	39.13		
300x450	200	37.13		
300x450	250	36.43		
300x450	300	36.20		
300x600	100	39.24		
300x600	150	39.13		
300x600	200	38.43		
300x600	250	38.14		
300x600	300	36.25		

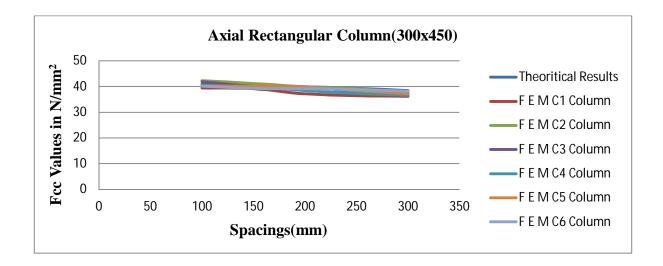
IV. RESULTS AND DISCUSSION

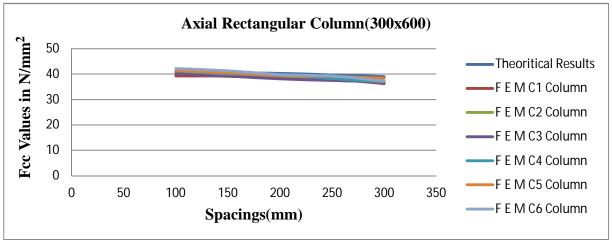
Due to confinement of core concrete by both inner and outer sets of stirrups, its original strength gets increased. In order to validate the theoretical results, the same has been compared with that of the finite element analysis results. The theoretical and finite element results obtained for the different column sections having different spacing of outer stirrups has been taken up for the comparison. The theoretical results obtained from the analysis of jacketed column of different thickness and varying concrete strength have been considered. That the results of theoretical and finite element analysis are approximately matching with some percentage of errors. Comparative errors are as shown in below graphs for with respect to theoretical analysis.

Graph 1: Comparison of Theoretical FCC Value to FEM FCC Value Axial Rectangular Column(230x300) 50 Fcc Value in N/mm² Theoritical Results 40 F E M C1 Column F E M C2 Column 20 F E M C3 Column 10 F E M C4 Column 0 F E M C5 Column 0 50 100 150 200 250 300 350 F E M C6 Column Spacings(mm)

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From the Above graph results of theoretical and finite element analysis are approximately matching with some percentage of errors. The percentage of errors is mentioned in the conclusion.

V. CONCLUSIONS

The object of investigation is to study the confined and unconfined capacity of jacketed R.C column. In turn to compare confined concrete strength by theoretical and F E M analysis. The conclusions are discussed in the respective chapters with results for all the aspects considered for study.



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- A. R. C Jacketing can be considered for rehabilitation of column member. In which special design and construction techniques are not essential.
- B. The K and fcc of axial loaded square and rectangle column will considerably decrease with increase in spacing of bars.
- C. The theoretical and FEM analysis reveals that axial rectangular column the maximum error varied from positive 3.26 to negative 8.17.

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