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Parametric Effects and Optimization of Machining Parameters in Hard Turning: A Literature Review

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Abstract- In today's rapidly changing state in metal cutting industries, applications of optimization techniques in hard turning processes is essential for a manufacturing unit to replace grinding/finishing operations due to the development of advanced tool materials and rigid machine tools, which can ensure the same accurate geometrical and dimensional tolerances. The complex machining process gets influenced by multiple process parameters, particularly in a finish hard turning operation, which often determines the final quality of the parts. This article presents a brief review of the techniques of modeling and optimization that have significant influence in hard turning. The main objectives of this study investigate and evaluate the effect of different machining parameters on surface roughness, tool wear, tool life, cutting forces, power consumption, material removal rate and cutting temperature and chip morphology during turning of different hard steels with hardness more than 45 HRC.

I. INTRODUCTION

The quality of design can be improved by improving the quality and productivity in companywide activities. Those activities concerned with quality, include in quality of product planning, product design and process design [1]. The traditional method of machining the hardened steels (<45HRC) includes rough turning, heat treatment, and then grinding process. Recently, hard machining is an emerging technology and an attractive alternative to conventional grinding due to its potential benefits such as short cycle time, process flexibility, higher material removal rate, compatible surface roughness and less environmental problems without the use of cutting fluid (Fig. 1). In hard turning, there are many factors affecting the cutting process behavior such as tool variables (tool materials, cutting edge geometry, clearance angle, nose radius, etc.), workpiece variables (materials and hardness), cutting conditions (cutting speed, feed and depth of cut), machining time, tool vibrations, cutting environments (dry and wet)and chip morphology. In order to achieve good surface finish closer to cylindrical grinding, improve cutting efficiency (minimum tool wear, less cutting force and power consumption, maximum MRR, low cutting temperature) and process at low cost. It is essential to understand the parametric effects and to optimize the various machining parameters. Several experimental investigations have been carried out over the years in order to study the effects of cutting parameters and machining time, the influence of workpiece hardness, tool geometry, tool materials and cutting fluid on machinability aspects using several workpieces in hard turning is presented in Table I.
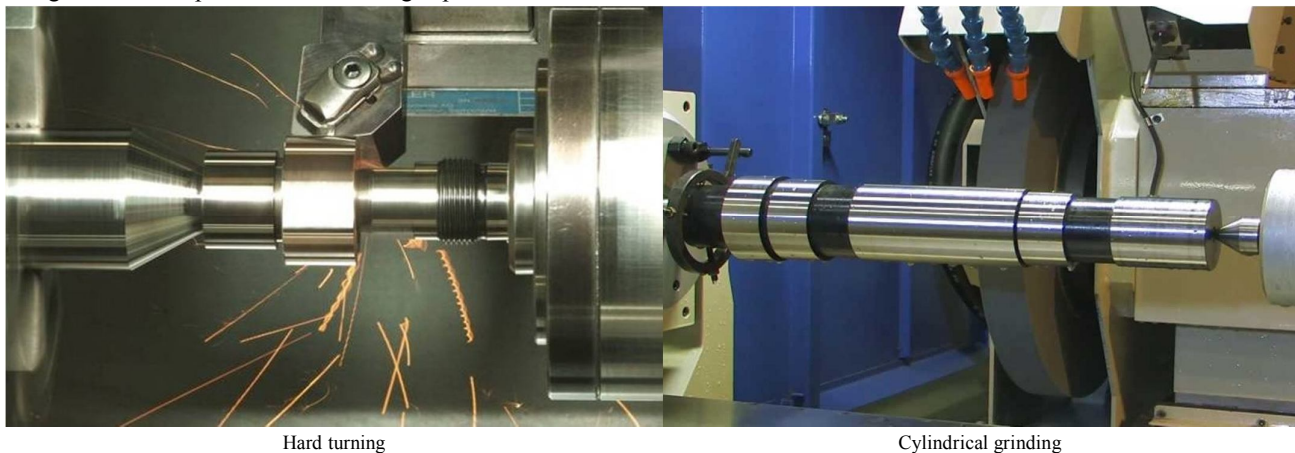

| Hard turning | Cylindrical grinding |

Fig. 1 Hard turning versus cylindrical grinding process

TABLE I

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OVERVIEW OF DIFFERENT WORK MATERIALS AND MACHINING PARAMETERS WITH VARIOUS OPTIMIZATION TECHNIQUES USED IN HARD TURNING.

Title	Author(s)	Journal Name, Volume, Issue& Year	Material and Hardness	Cutting Tool/Insert	Working Condition				Output Response(s)	Method or Techniques
Analysis of surface roughness and cutting force components in hard turning with CBN tool: Prediction model and cutting conditions optimization.	H. Aouici, M. A. Yallese, K. Chaoui, T. Mabrouki, J.F. Rigal.	Measurement 45, 2012	AISI H11 steel	CBN tool.	v 120 180 240	f 0.08 0.12 0.16	d 0.15 0.30 0.45	H 40 45 50	Surface roughness, Cutting forces	Box-Behnken design, ANOVA, RSM.
Surface roughness and cutting forces modeling for optimization of machining condition in finish hard turning of AISI 52100 steel	M.W. Azizi, S. Belhadi, M. A.Yallese, T. Mabrouki, J.F. Rigal	Journal of Mechanical Science and Technology 26 (12), 2012	AISI 52100 steel	Coated Al$_2$O$_3$/TiC mixed ceramic insert.	v 85 120 170	f 0.08 0.12 0.16	d 0.1 0.2 0.3	H 46 52 62	Surface roughness, Cutting forces	Taguchi method, ANOVA, Regression analysis
Determining the effect of cutting parameters on surface roughness in hard turning using the Taguchi method.	I. Asiltürk, H. Akkus	Measurement 44, 2011	AISI 4140 and 51 HRC.	Al$_2$O$_3$+TiC coated carbide insert.	v 90 120 150	f 0.18 0.27 0.36	d 0.2 0.4 0.6		Surface roughness	Taguchi method, ANOVA.
Machinability investigations in hard turning of AISI D2 cold work tool steel with conventional and wiper ceramic inserts.	V.N. Gaitonde, S.R. Karnik, L. Figueira, J. P. Davim	International Journal of Refractory Metals and Hard Materials 27 (4), 2009	AISI D2 cold work tool steel and 59/61 HRC.	Ceramic inserts with TiN coating.	v 80	f 0.10	d 0.2 0.4 0.6	t 5 10 15	Machining force, power, specific cutting force, surface roughness and tool wear.	FFD, ANOVA, RSM.
Mathematical modeling of surface roughness for evaluating the effects of cutting parameters and coating material.	M. C. Cakir, C. Ensarioglu, I. Demirayak	Journal of materials processing technology 209, 2009	AISI P20 cold work tool steel and 52-54 HRC.	CVD coated (TiCN/Al$_2$O$_3$/TiN) and PVD coated (TiAlN) carbide inserts.	v 120 160 200	f 0.12 0.18 0.22	d 1 1.5 2		Surface roughness.	Regression analysis.
Experimental investigations of cutting parameters influence on cutting forces and surface roughness in finish hard turning of MDN250 steel.	D.I. Lalwani, N.K. Mehta, P.K. Jain	Journal of Materials Processing Technology 206(1–3), 2008	MDN 250 steel and 50 HRC.	Coated ceramic inserts.	v 55 74 93	f 0.04 0.08 0.12	d 0.1 0.15 0.2		Cutting forces, surface roughness.	RSM, ANOVA.
Investigating the machinability evaluation of Hadfield steel in the hard turning with Al$_2$O$_3$/TiC mixed ceramic tool based on the response surface methodology.	J.T. Horng, N.M. Liu, Ko-Ta Chiang.	Journal of Materials Processing Technology 208 (1–3), 2008	Hadfield steel and 210 HV.	Uncoated Al$_2$O$_3$/TiC mixed ceramic tool.	v 100 175 250	f 0.05 0.1 0.15	d 0.25 0.50 0.75	r 0.8 1.0 1.2	Flank wear, Surface roughness.	RSM, SAO method, ANOVA.
Estimating the effect of cutting parameters on surface finish and power consumption during high speed machining of AISI 1045 steel using Taguchi design and ANOVA.	A. Bhattacharya S. Das, P. Majumder, A. Batish	Prod. Eng. Res. Devel. 3 (1), 2009	AISI 1045 steel and 50 HRC.	(TiCN+TiN) multilayer coated carbide insert.	v 58 96 151 240	f 0.045 0.1 0.125 0.160	d 1.0 1.2 1.5 2.0		Surface roughness, power consumption.	Taguchi design, ANOVA.
A surface roughness prediction model for hard turning process.	D. Singh, P.V. Rao	International Journal of Advanced	AISI 52100 steel and 58-60 HRC.	Al$_2$O$_3$+TiCN mixed ceramic tools.	v 100 150	f 0.10 0.20	d 0.2	r 0.4 0.8	α 6 16	Surface roughness	FFD, ANOVA, RSM.

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Title	Authors	Source	Material	Tool	Parameters				Responses	Methods
		Manufacturing Technology 32 (11-13), 2007			200	0.32		1.2 26		
Design optimization of cutting parameters when turning hardened AISI 4140 (63 HRC) with Al_2O_3+TiCN mixed ceramic tool.	E. Aslan, N. Camuscu, B. Bingoren	Materials & Design 28 (5)2007	AISI 4140 steel and 63 HRC.	Al_2O_3+TiCN mixed ceramic tools.	*v* 100 175 250	*f* 0.05 0.1 0.2	*d* 0.25 0.5 1.0		Flank wear, surface roughness.	Taguchi's technique, ANOVA, regression analysis.
Statistical analysis of surface roughness and cutting forces using response surface methodology in hard turning of AISI 52100 bearing steel with CBN tool	K. Bouacha, M.A. Yallese, T. Mabrouki, J.F. Rigal	Int. Journal of Refractory Metals & Hard Materials 28, 2010	AISI 52100 steel and 64 HRC	CBN tools	*v* 125 176 246	*f* 0.08 0.12 0.16	*d* 0.15 0.30 0.45		Surface roughness, Cutting forces	Taguchi's OA, ANOVA, RSM
Performance studies of multilayer hard surface coatings (TiN/TiCN/Al_2O_3/TiN) of indexable carbide inserts in hard machining: Part-II (RSM, grey relational and techno economical approach)	A.K. Sahoo, B. Sahoo	Measurement 46 (8), 2013	AISI 4340 Steel (47±1 HRC)	(TiN/TiCN/Al_2O_3/TiN) multilayer coated carbide insert	*v* 60 90 120 150	*f* 0.05 0.10 0.15 0.20	*d* 0.2 0.3 0.4 0.5		Flank wear, Surface roughness	FFD, ANOVA, Taguchi design, Grey relational analysis, regression analysis, RSM
Surface roughness model in turning hardened hot work steel using mixed ceramic tool	B. Fnides, M.A. Yallese, T. Mabrouki, J.F. Rigal	MECHANIKA. 3 (77), 2009	AISI H11 steel (X38CrMoV5-1) and 50 HRC	Al_2O_3/TiC mixed ceramic tools.	*v* 90 120 180	*f* 0.08 0.12 0.16	*d* 0.15 0.30 0.45		Surface roughness	Factorial DOE, ANOVA, Regression analysis, RSM
On the prediction of surface roughness in the hard turning based on cutting parameters and tool vibrations	Z. Hessainia, A. Belbah, M.A. Yallese, T. Mabrouki, J.F. Rigal	Measurement 46, 2013	42CrMo4 steel and 56 HRC	Al_2O_3/TiC mixed ceramic tools.	v 90 120 180	f 0.08 0.12 0.16	d 0.15 0.30 0.45		Surface roughness, Tool vibrations	DOE, ANOVA, RSM
Machinability evaluation in hard turning of cold work tool steel (D2) with ceramic tools using statistical techniques.	J. P. Davim, L. Figueira	Materials & Design 28 (4), 2007	AISI D2 cold work tool steel and 60 HRC.	Ceramic tools	*v* 80 150 220	*f* 0.05 0.1 0.15	*d* 0.2	*t* 5 10 15	Tool wear, specific cutting pressure, surface roughness.	Taguchi's OA, ANOVA.
Machinability investigations on hardened AISI 4340 steel using coated carbide insert	R. Suresh, S. Bsavarajapa, V.N. Gaitonde, G.L. Samuel	Int. Journal of Refractory Metals and Hard Materials 33, 2012	AISI 4340 steel and 48 HRC	(TiN/MT-TiCNAl_2O_3) multilayer coated carbide insert	*v* 80 140 200 260	*f* 0.10 0.18 0.26	*d* 0.8 1.0 1.2	*t* 2 4 6 min	Machining force, Surface roughness, Tool wear, Chip analysis	FFD, ANOVA, RSM
Effects of cutting edge geometry, workpiece hardness, feed rate and cutting speed on surface roughness and forces in finish turning of hardened AISI H13 steel.	T. Özel, T.K. Hus, E. Zerne	Int J Adv Manuf Technol 25, 2005	AISI H13 steel and 51.3 & 54.7 HRC.	CBN insert.	*v* 100 200	*f* 0.1 0.2	*d* 0.254	*H* 51.3 54.7 *E* Honed Chamfered	Surface roughness, cutting forces.	Factorial design, ANOVA.
Turning of hardened 100Cr6 bearing steel with ceramic and PCBN	G.C. Benga, A.M. Arabo	Journal of Materials Processing	100Cr6 bearing steel and 62-64	Mixed alumina, Whiskers reinforced alumina inserts.	*v* 100 140	*f* 0.06 0.14	*d* 0.25		Tool life, surface finish.	FFD

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cutting tools.		Technology	HRC.		180	0.22			
		143–144, 2003							

II.   LITERATURE REVIEW

Bartarya and Choudhury [2] had developed an interesting review on hard machining and on key issues related to the process performance. The review shows that tool material grade, cutting edge geometry and cutting parameters affect the process efficiencies in terms of tool forces and surface integrity evolution. Aslan et al. [3] optimized the cutting parameters (v, f, d) for flank wear and surface roughness using Taguchi orthogonal array when turning hardened AISI 4140 steel (63 HRC) with Al_2O_3 + TiCN mixed ceramic tool. The relationship between the parameters and the responses were determined using multiple linear regression analysis. Bhattacharya et al. [4] have investigated the effect of cutting parameters on surface finish and power consumption during high speed machining of AISI 1045 steel using Taguchi design and ANOVA. The result showed a significant effect of cutting speed on surface roughness and power consumption, while the other parameters have not substantially affected the response. Lalwani et al. [5] attempted to investigate the effect of cutting parameters (cutting speed, feed rate and depth of cut) on cutting forces (feed force, thrust force and cutting force) and surface roughness in finish hard turning of MDN250 steel (equivalent to 18Ni (250) maraging steel) using coated ceramic tool through response surface methodology (RSM) and sequential approach using face centered central composite design. The results show that the depth of cut is most significant factor for feed force and feed rate is most significant factor for surface roughness. Fnides et al. [6] Conducted experimental study to determine statistical models of surface roughness criteria in turning hardened AISI H11 (X38CrMoV5-1) steel (50 HRC) with mixed ceramic tool. Mathematical models were elaborated based on the software Minitab in order to express the influence degree of each cutting regime on surface roughness. The results indicate that feed rate is the dominant factor affecting surface roughness, followed by cutting speed. As for the depth of cut, its effect is not very important. Asilturk and Akkus [7] focused an optimization of turning parameters based on the Taguchi method to minimize surface roughness (Ra and Rz) in dry turning of hardened AISI 4140 (51 HRC) using Al_2O_3+TiC coated carbide cutting tools. The statistical methods of signal to noise ratio (SNR) and the analysis of variance (ANOVA) are applied to investigate effects of cutting speed, feed rate and depth of cut on surface roughness. Results indicate that the feed rate has the most significant effect on Ra and Rz. In addition, the effects of two factor interactions of the feed rate-cutting speed and depth of cut-cutting speed appear to be important. Bouacha et al [8] investigated the effect of cutting speed, feed rate and depth of cut on surface roughness and cutting forces using three level factorial design (3^3) during machining of bearing steel (AISI 52100) with CBN tool. Results show how much surface roughness is mainly influenced by feed rate and cutting speed and that the depth of cut exhibits maximum influence on the cutting forces as compared to feed rate and cutting speed. Sahoo and Sahoo [9] presented the mathematical modeling and parametric optimization on flank wear and surface roughness based on response surface methodology and grey based Taguchi method in finish hard turning of AISI 4340 steel (47±1 HRC) using multilayer coated carbide (TiN/TiCN/Al_2O_3/TiN) insert under dry environment. The economical feasibility of utilizing multilayer TiN coated carbide insert has been described. Model adequacy has been checked using correlation coefficients. Davim and Figueira [10] investigated the machinability evaluation in hard turning of cold work steel (D2) by ceramic cutting tools, using statistical techniques. Results showed that the tool wear was highly influenced by the cutting speed, and in a smaller degree, by cutting time. The specific cutting pressure was also strongly influenced by the feed rate. The surface roughness is influenced by feed rate (29.6%) and cutting time (32%).Their tests also show that with the appropriated choice of cutting parameters it is possible to obtain a surface roughness (Ra <0.8 μm) that allows cylindrical grinding operations to be eliminated. Suresh et al [11] have analyzed the effects of process parameters (v, f, d, and t) on machinability aspects such as machining force, surface roughness and tool wear by using multilayer hard coatings (TiC/TiCN/Al_2O_3) on cemented carbide substrate for machining of hardened AISI 4340. The analysis of results concluded that, low feed rate and depth of cut and high cutting speed was beneficial for minimizing the machining force and surface roughness and they also observed reduced tool wear with lower cutting speed and lower feed rate. Azizi et al. [12] conducted an experiment to analyze the effect of cutting parameters (cutting speed, feed rate and depth of cut) and workpiece hardness in finish hard turning of AISI 52100 steel with coated Al_2O_3+TiC mixed ceramic cutting tools by employing Taguchi's orthogonal array, ANOVA and regression analysis. The analysis reveals that the feed rate, workpiece hardness and cutting speed have significant effects in reducing the surface roughness; whereas the depth of cut, workpiece hardness and feed rate are observed to have a statistically significant impact on the cutting force components than the cutting speed. Aouici et al. [13] have applied response surface methodology (RSM) to optimize the effect of cutting parameters (v, f, d) at the different levels of workpiece hardness on surface roughness and cutting force components in hard turning of AISI H11 with CBN tool. Results showed that the cutting force components were influenced principally by depth of cut and workpiece hardness; however, both feed rate and workpiece hardness had statistical significance on surface roughness. In the

similar way, Dureja et al. [14] applied RSM to investigate the effect of cutting parameters on flank wear and surface roughness in hard turning of AISI H11 steel with a coated-mixed ceramic tool. The study indicated that the flank wear is influenced principally by feed rate, depth of cut and workpiece hardness whereas, feed rate and workpiece hardness are the most significant factors affecting the surface roughness. Ozel et al. [15] conducted a set of analysis of variance (ANOVA) and performed a detailed experimental investigation on the surface roughness and cutting forces in the finish hard turning of AISI H13 steel. Their results indicated that the effects of workpiece hardness, cutting edge geometry, feed rate and cutting speed on surface roughness are statistically significant; besides, the effects of two-factor interactions of the edge geometry and the feed rate, and the cutting speed and the feed rate are also important. They reported that especially, small edge radius and lower workpiece hardness increased surface roughness in their experiments. Singh and Rao [16] conducted an experimental investigation to determine the effects of cutting conditions (cutting speed and feed) and tool geometry (effective rake angle and nose radius) on the surface roughness in the finish hard turning of the bearing steel (AISI 52100). Mixed ceramic inserts made up of aluminum oxide (Al_2O_3) and titanium carbon nitride (TiCN) coated tools were used. The study indicated that the feed is the dominant factor determining the surface finish followed by nose radius and cutting velocity. The effective rake angle has very little influence on surface finish, but the interaction effects of nose radius and effective rake angle are significant. Horng et al. [17] developed RSM model using CCD in the hard turning using uncoated Al_2O_3/TiC mixed ceramics tool for flank wear and surface roughness. Flank wear was influenced principally by the cutting speed and the interaction effect of feed rate with nose radius of tool. The cutting speed and the tool corner radius affected surface roughness significantly. Sharma et al. [18] studied machining variables such as cutting forces and surface roughness which are measured during turning at different cutting parameters such as approaching angle, speed, feed and depth of cut. The data obtained by experimentation is analyzed and used to construct model using neural networks and reported the following results: (i) approaching angle influences cutting force and feed force positively but thrust force negatively, (ii) speed influences thrust force and feed force positively but tangential force negatively, (iii) feed rate influences tangential force, feed force, and thrust force positively and (iv) depth of cut influences tangential force, thrust force, and feed force positively. Benga and Abrao [19] studied the machinability of hardened 100Cr6 bearing steel (62–64 HRC) when dry turning using mixed alumina, whisker reinforced alumina and PCBN inserts. The best tool life results were obtained with the CBN compact followed by the mixed alumina at low feed rates and by the whisker reinforced alumina when feed rate was increased. Cakir et al. [20] studied the effects of cutting parameters on surface roughness in hard turning of AISI P20 steel (52-54 HRC) using CVD coated carbide (TiCN/Al_2O_3/TiN) and PVD TiAlN coated carbide inserts. CVD coated inserts demonstrated higher values of surface roughness, which further increased at higher cutting speed. However, PVD coated inserts showed almost no variation in surface roughness at higher cutting speeds. Higher feed rates produced higher surface roughness values, whereas cutting speed had a contrary effect and cutting depth did not significantly affect. The authors have indicated necessity to investigate the tool life aspects. Gaitonde et al. [21] explored the effects of depth of cut and machining time on machinability aspects such as machining force, power, specific cutting force, surface roughness, and tool wear by using second-order mathematical models during turning of high chromium content AISI D2 cold work tool steel with CC650, CC650WG and GC6050WH ceramic inserts. Their results revealed that CC650WG wiper insert performed better with respect to surface roughness and tool wear, whereas the CC650 conventional insert was useful in reducing the machining force, power, and specific cutting force. Gunay and Yucel [22] used Taguchi technique for determining optimum surface roughness in turning of high-alloy white cast iron. They machined high –alloy white cast iron on CNC lathe using ceramic and cubic boron nitride (CBN) cutting tools. Taguchi's signal-to-noise ratio were used to determine the optimum cutting conditions which was calculated for surface roughness (Ra). Aggarwala et al. [23] investigated the power consumption in hard turning of AISI P-20 tool steel (32-36 HRC) using TiN coated carbide insert with Taguchi's and RSM technique. Cryogenic environment was the most significant factor in minimizing power consumption followed by cutting speed and depth of cut. The effects of feed rate and nose radius were found to be insignificant. RSM technique was found to be better than Taguchi's method. Shihab et al. [24] investigated the effect of cutting parameters on cutting force components and material removal rate (MRR) in dry and wet hard turning of AISI 52100 steel with coated carbide tool. Hessainia et al. [25] used Taguchi DOE method and RSM to investigate the effect of machining factors (i.e., cutting speed, depth of cut, feed rate) and cutting phenomenon (i.e, cutting tool vibration) on surface roughness in turning of 42CrMo4 hardened steel. The results indicate that the feed rate is the dominant factor affecting the surface roughness, whereas vibrations have a low effect on it. Das et al. [26] experimentally investigated the machinability (surface roughness, flank wear and chip morphology) of hardened AISI 4140 steel (51 HRC) using PVD-TiN coated Al_2O_3 + TiCN mixed ceramic inserts under dry environment. The machined surface characterization, tool wear mechanism and chip morphology were investigated, along with optimization and development of mathematical models for surface roughness and flank wear. Chip morphology indicates the formation saw-tooth/serrated chips at higher feed due to reduction of chip thickness, results in degradation of surface finish.

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III.   CONCLUSIONS

A. The present study has overviewed on turning of hardened steels that are used by ball bearings, automotive, gear, and die-making industries. Hard turning offers a number of potential benefits over traditional form grinding, including lower equipment costs, shorter setup time, fewer process steps, greater part geometry flexibility, and elimination of the use of cutting fluid.

B. The review has been organized in terms of role of machining parameters on machinability of hard steel. The cutting tool geometry, workpiece hardness, tool vibrations, tool materials, chip morphology, cutting environment and cutting parameters significantly affect the cutting forces, power consumption, surface roughness, MRR, tool wear, tool life and cutting temperature.

C.   From above study it was found that for surface roughness feed is the most significant factor, for tool wear cutting speed is the most significant factor and for cutting force feed rate is the most significant factor. With a little help choosing the right application, right machine and right tooling, hard turning can quickly enhance the profitability of a variety of tight tolerance applications.

D.   In hard turning, Taguchi method and ANOVA have proved to be efficient tools for controlling the effect on machining performances. Response surface methodology (RSM) presented the desired criteria optimization for determining the relationship between the various factors and the responses.

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