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Fatigue Analysis of Lug Joint in the Nose Landing Gear

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Abstract: The objective of this project is to design a lug joint in the nose landing gear. During take-off and landing, static and dynamic loads are acting on the lug joint in the nose landing gear which leads to the structural failure of the component. The take-off and landing loads are calculated by using aerodynamic calculations. The dimensions of the lug in nose landing gear is obtained by strength of material approach for the aluminium alloy materials. Finite element analysis will be carried out in order to estimate the maximum local stress which will be required in the fatigue analysis of the lug joint. Fatigue life and maximum deformation of the lug joint in the nose landing gear at the region of high stress during the time of take-off and landing are estimated.

I. INTRODUCTION

An aircraft is a machine which is used for good air transport system. It is used to travel one place to another place (long or short distance) in a short period of time and it can able to carry high load i.e., in commercial aircraft passengers, cargo, flight crew, fuel tank, scientific instruments or equipment., in military aircraft warheads, bombs etc., Landing gear is the most important component of the aircraft. It can able to carry the whole weight of an aircraft at the time of takeoff, landing and taxing. Many types of landing gears are used. There are single, main, tricycles, quadricycle, tricycle, tail gear, multi bogey, releasable rail and skid. In most of the commercial aircraft, tricycle landing gear is used. It can be retractable or fixed. In modern aircraft to minimize the drag, retractable landing gear is used. Tri cycle landing gear has one nose landing gear and two main landing gears. In landing gear, lug joint is the most important structure. Lug is the structural member which can able to absorb high impact load at the time of takeoff and landing. And then the load is transvers through other components or members. So, the design of the lug joint is very much important. When design the lug joint of the main land gear, considered takeoff configuration. While takeoff, total weight of the aircraft is carried by the main landing gear

II. MATHEMATICAL APPROACH

A. Load Calculation

Distance between the aircraft center of gravity and the ground will be

$$H_{CG} = \Delta H_{clear} + D_{prop}$$
$$= 1.2 + \frac{3.95}{2}$$
$$H_{CG} = 3.175 \text{ m.}$$

Attach nose gear to the fuselage landing gear height will be,

$$H_{CG} = H_{CG} - \frac{D_{FUSE}}{2}$$
$$= \frac{3.175 - 2.5}{2}$$
$$H_{CG} = 1.925 \text{ m.}$$

Wing mean aerodynamic chord

$$B = \sqrt{\frac{S.AR}{2}}$$
$$= \sqrt{61 \times 12}$$
$$= \sqrt{732.05}\text{m}$$
$$= 27.05 \text{ m.}$$
$$\overline{C} = S\backslash b$$
$$= \frac{61}{}$$

$$27.05$$
$$= \ 2.25 \ m$$

$T_{w = }(t\backslash c)_{max} \ C \ = \ 0.12 \times 2.25$

$T \ w = 0.27m.$

B. *Landing Gear Height*

$H_{CG =} H_{CG +} t_w$

$$= 3.175 + 0.27$$

$$\underline{ 2 }$$

$$= 304 \ m.$$

$X_{CWF =} X_{mg \ - (}X_{ac \ - } X_{cg \ fuel \ )} \ C$

$$= x_{mg} - (0.22 - 0.18) \times 2.25$$

$$= x_{mg \ - } 0.09$$

$X_{h =} X_{ach} - X_{mg}$

$$= L_h + (\ X_{ac} + X_{cg \ fuel} \ ) \ C - x_{mg}$$

$$= 13 + (0.22 \times 0.18) \times 2.25 - x_{mg}$$

$$= 13.09 - x_{mg}$$

$H_{D =} H_{cg =} h_T = 3.175$

$$K = \quad 1$$

$$\underline{\quad \pi \rho AR \quad}$$

$$= \quad \frac{1}{3.14 \times 0.9 \times 12}$$

$$= 0.029$$

$$C_{LC \ =} \quad \frac{2 \ W}{\rho V L^2 S}$$

$$= \quad \frac{2 \times 23000 \times 9.81}{0.512 \times (127.8)^2 \times 61}$$

$$= 0.88$$

$C_{CTo} = C_{LC} + \Delta C_{L \ FLAP}$

$$= 0.88 + 0.9$$

$CTo \quad = 1.78$

$C_{DTo} = C_{DoTo} + KC^2_{CTo}$

$$= 0.03 + 0.029 \times (1.78)^2$$

$C_{DTo} = 0.12$

NOTE:

$V_R = 1.1 \times V_S \ = 1.1 \times 140 = 154 \ Km\backslash hr$

$V_R \ = 42.7 \ m\backslash s$

$D_{To} = 1\backslash 2 \rho v^2 R \ SC_{DTo}$

$$= 1\backslash 2 \times 1.225 \times (42.7)^2 \times 61 \times 0.12$$

$D_{To} \ = 8174.7 \ N.$

$L_{To} = 1\backslash 2 \times \rho v^2_R \ S_{REF} C_{LTo}$

$$= 1\backslash 2 \times 1.225 \times (42.7)^2 \times 61 \times 1.78$$

$L_{To} = 121258.3 \ N.$

$L_H = 1\backslash 2 \times \rho V_R^{\ 2} \ S_h C_{Lh}$

$$= \ 1\backslash 2 \times 1.225 \times (42.7)^2 \times 14 \times (-0.8)$$

$L_H \ = -12507.7N.$

$M_{ACref} = 1\backslash 2 \times \rho v_R^{\ 2} C_{Mac} \ ref \ S_{ref} \ C$

$$= 1\backslash 2 \times 1.225 \times (42.7)^2 \times 61 \times (-0.03) \times 2.25$$

$Mac_{ref} \quad = -4598.2N.$

$L_{WF} = L_{To} - L_H$

$= 121258.3 - (-12507.7)$

$L_{wf} = 133766.05 N.$

Friction force :

$F_F = \mu\ (W - L_{To})$

$= 0.04\ (23000 \times 9.81 \times - 121258.3)$

$F_f = 4174.8 N.$

$T = P\eta p$ $\qquad = 69854.7 - 4564.2 - 4174.8$

$\overline{V_R}$ $\qquad\qquad \overline{-23000}$

$A = 2.65\ m\backslash s^2$

C. *Contributing moment*

$M_W = W\ (x_{mg} - x_{cg})$

$= 23000 \times 9.81 (x_{mg})$

$M_D = D\ (Z_D - Z_{MG})$

$= 4564.2 \times 3.1$

$= 14149.02\ Nm.$

$M_T = T\ (Z_T - Z_{MG})$

$= 69854.7 \times 3.1$

$= 216549.5\ Nm.$

$M_{CWF} = L_{WF}\ (X_{MG} - X_{ac\ wf\ TO\ cg})$

$= 133766.05\ (x_{mg} - 0.09)$

$M_{CH} = L_h\ (X_{ac\ h} - X_{mg})$

$= -12507.7\ (13.09 - X_{mg})$

$M_a = M_a - (Z_{cg} - Z_{mg})$

$= 23000 \times 2.65 \times 3.1$

$X_{mg} = I_{yy\ mg}\ \emptyset\ - (Z_D - Zmg) + (Z_T - Z_{MG}) - Mac_{wf} - ma\ (Zcg - Zmg) - Wx_{cg} + Lwf + Xac_{wf} + \qquad Lh_{ach}$

$\overline{\qquad}$

$Lwf + Lh + W$

$= \quad 23000 \times 9\backslash57.3 - 14149.02 + 216549.5 = (-4598.2) - 188945 + 0 + 133766.05 + \qquad (12507.7 \times 13.09)$

$133766.05 + (-12507.07) - 23000 \times 9.81$

$= \quad 130020.6 \qquad\qquad = \quad 1.250\ m.$

$\overline{-104371.65}$

$X_{mg} = 1.25 m.$

Check tip back requirement

$\Delta x_{cg} = X_{cg} - X_{cg\ aft}$

$= (0.30 - 0.18)\ C$

$= 0.12 \times 2.25$

$= 0.27 m$

Distance between mg and aft

Xmg_{aft} $Xmg\ aft = Xmg - \Delta xmg$

$= 1.25 - 0.27$

$= 0.98 m.$

Tip back angle

$\propto tb = \tan^{-1} (Xmg\backslash Hcg)$

$= \tan^{-1} (0.98\backslash3.175)$

$\propto tb = 17.15 deg.$

This angle is greater than aircraft take off rotation angle (14 deg)

$17.15 > 14$

$Fn_{max} = B\ m_{max}\qquad W$

$$0.15 = \frac{1.25}{B} \quad W$$

$$B = \frac{1.25}{0.15}$$

B = 8.33 (Distance between mg and ng)

$F_n = F_{n_{max}} + F_{n \; dynamic}$ (due to breaking)

$$= \frac{W B \; max}{B} + \frac{W \setminus ac \setminus H}{g \; B}$$

$$= \left\{ (23000 \times 9.81) + \frac{1.25}{8.33} \right\} + \left\{ \left(\frac{23000 \times 9.81 \times 3 \times 3.175}{9.81 \times 8.33} \right) \right\}$$

$$= 33858.04 + 26299.5$$

$F_n = 60157.5$ N .

D. *Dimension calculation of the nose landing gear joint*

Vertical load is applied on the wheel is ,

$F \; vn = FOS \times F$

$= 1.5 \times 60157.5$

$= 90236.25$ N

Material used : AL 7075

Yield stress :

$$\sigma yt = \frac{P}{(2\pi d^{2} \setminus 4)}$$

$$503 = \frac{90236.25}{\frac{2 \times 3.14 \times d^{2}}{4}}$$

$$503 \times 1.57 = \frac{90236.25}{d^{2}}$$

$d^{2} = 114.2$

Bearing stress:

$$\sigma \; bearing = \frac{P}{D \times t}$$

σ bearing = 0.5 $\times$ ultimate stress

$= 0.5 \times 572$

$\sigma b = 286$ Mpa .

$$\sigma \; bearing = \frac{90236.25}{11 \times t}$$

$$3146 = \frac{90236.25}{t}$$

$$t = \frac{90236.25}{3146}$$

t = 28.68 mm.   or 29 mm.

h = 2d   ;   b = t

h=2$\times$11   ;   b = 28.68

h =22mm   ;   b = 29mm

Material used : AL 7050

$\sigma_{yt} = 470$ Mpa

$$\sigma_{yt} = \frac{P}{(2\pi d^{2} \setminus 4)}$$

$$470 = 90236.25$$

$$2\pi d^2\backslash 4$$

d^2 = 122.28

d = 11mm.

$\sigma_b = 0.5 \times 470$

σ_b = 235 Mpa

$\sigma bearing = \dfrac{P}{D \times t}$

$235 = \dfrac{90236.25}{11 \times t}$

$2585 = \dfrac{90236.25}{t}$

t = 3.5 mm,

h = 22mm,

b = 35mm.

Material used : AL 7178

σyt = 538 Mpa

$\sigma yt = \dfrac{P}{(2\pi d^2\backslash 4)}$

$1.57 \times 538 = \dfrac{90236.25}{d^2}$

d^2 = 106.83

d = 10.33

d = 11mm.

$\sigma_b = 0.5 \times 538$

σ_b = 269 Mpa

$\sigma_b = \dfrac{P}{D \times t}$

$269 = \dfrac{90236.25}{11 \times t}$

$2959 = \dfrac{90236.25}{t}$

t = 30.49 , t = 31mm.

E. Final Values

t = 30mm,

b = 30mm,

d = 10mm,

h = 25mm.

III. MATERIAL SELECTION

The material of lug joint must be carefully selected. So that
it can able to withstand for high applied load. Thus there are
Several materials can be used for manufacturing the lug joint.
Considered the strength and weight is very much important.
The strength must be high and weight must be less to reduce
dead weight of the aircraft during fly . Here Aluminium
Alloy is considered to design the Lug joint. Selection of material depends upon

1) Stiffness
2) Strength
3) Durability
4) damage tolerance

5) Corrosion.

Al 7075-T6 has high strength, lower fracture toughness.

Used for tension application where fatigue is not critical. It

also has low short transverse properties and low stress corrosion resistance.

IV. MATERIAL PROPERTIES

ALUMINIUM ALLOYS	Al – 7050	Al – 7178	Al – 7175	Al – 7075
Density, ρ	2830 Mpa	2830 Mpa	2800 Mpa	_____
Elastic modulus, E	71.7 Gpa	72 Gpa	_____	_____
Ultimate tensile stress , σ_t	525 Mpa	607 Mpa	552 Mpa	572 Mpa
Yield stress, σ_y	470 Mpa	538 Mpa	503 Mpa	503 Mpa
Fatigue strength	200 Mpa	150 Mpa	160 Mpa	159 Mpa
Poisson's Ratio v	0.33	0.33	0.33	0.33

V. MODELING OF LUG

2D view of nose landing gear
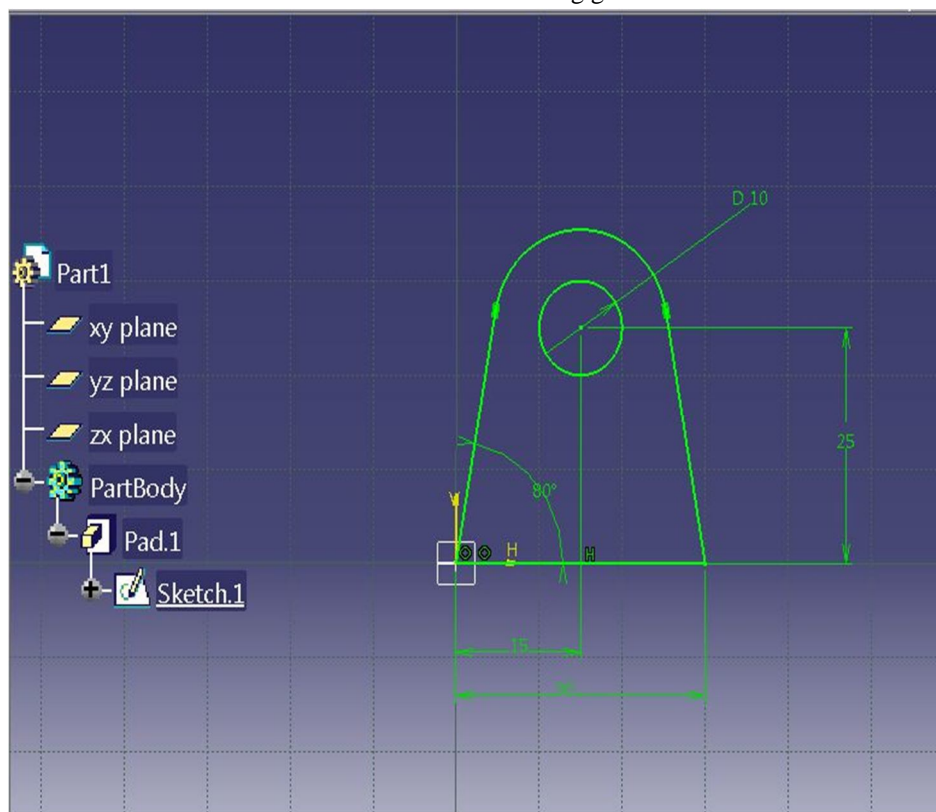
3D view of nose landing gear
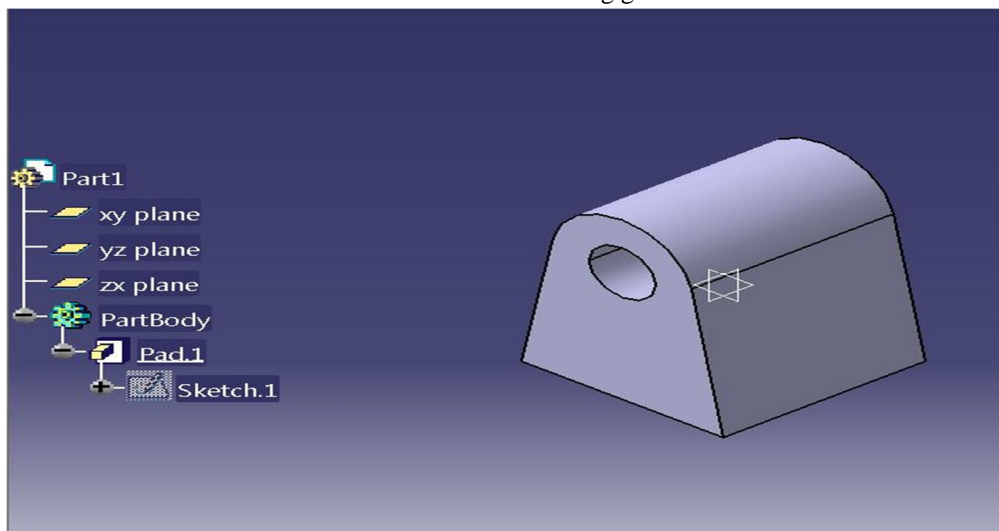
A. *Fatigue Analysis Of Al 7050*

Total deformation of Al 7050
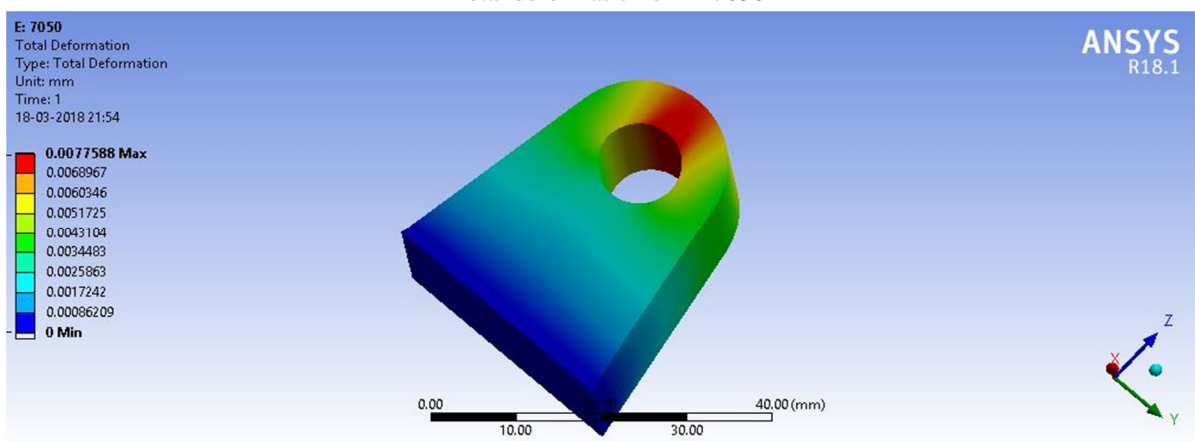
Equivalent stress of Al 7050
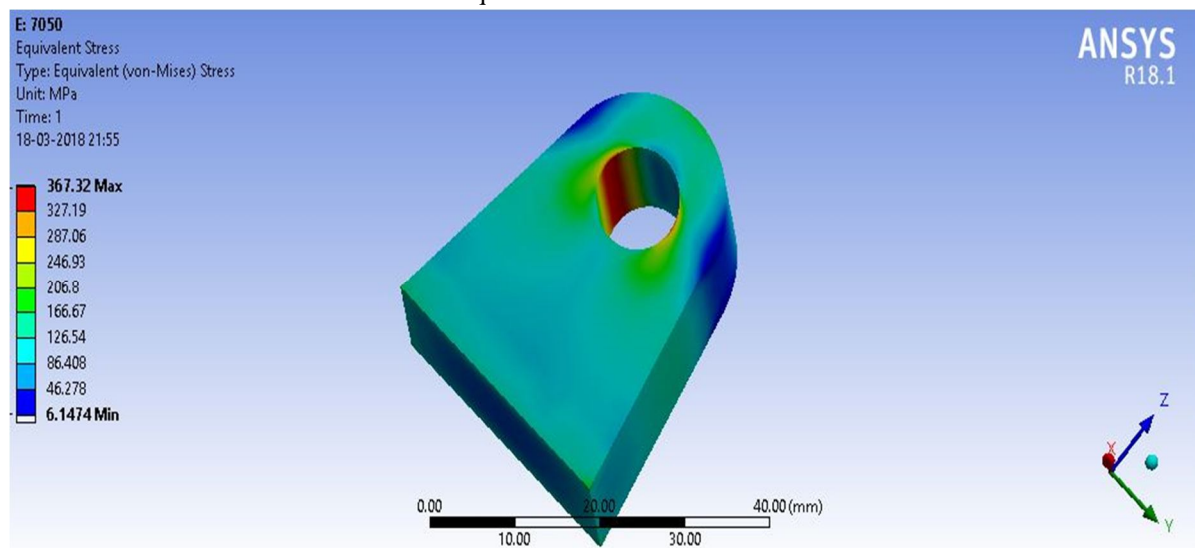
Fatigue life of Al 7050
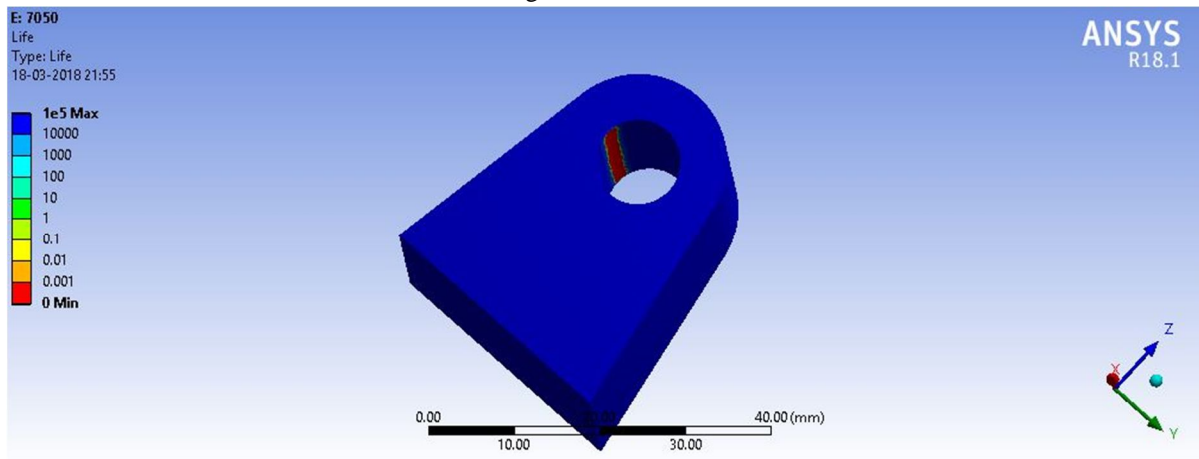
Damage of Al 7050
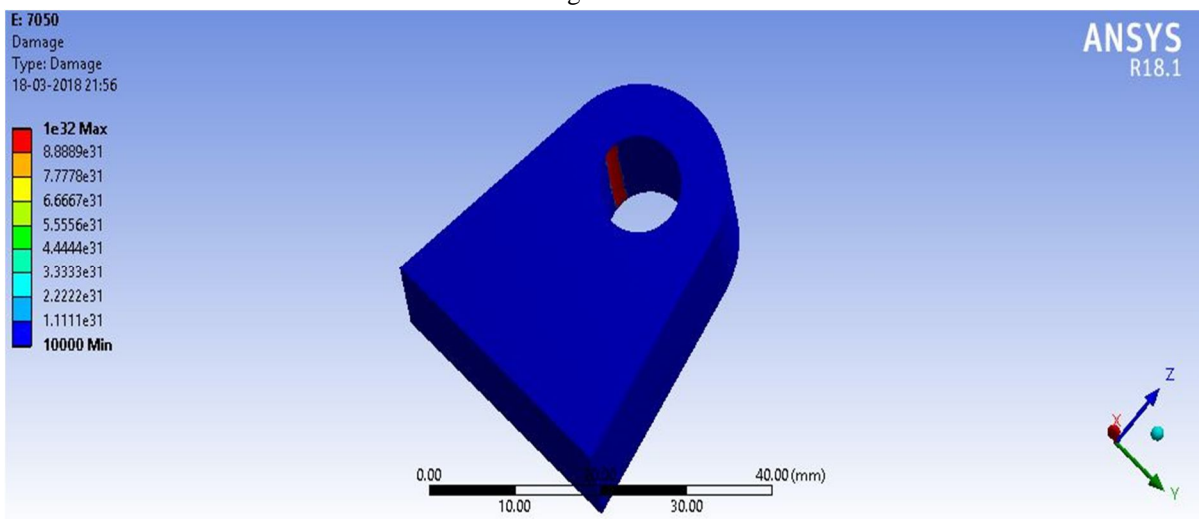
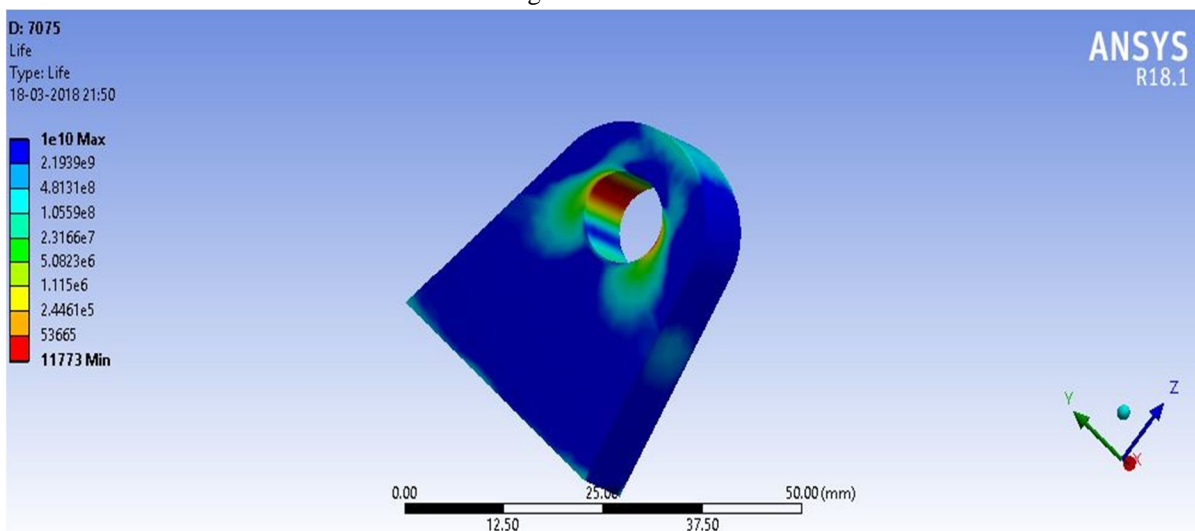Factor of safety of Al 7050
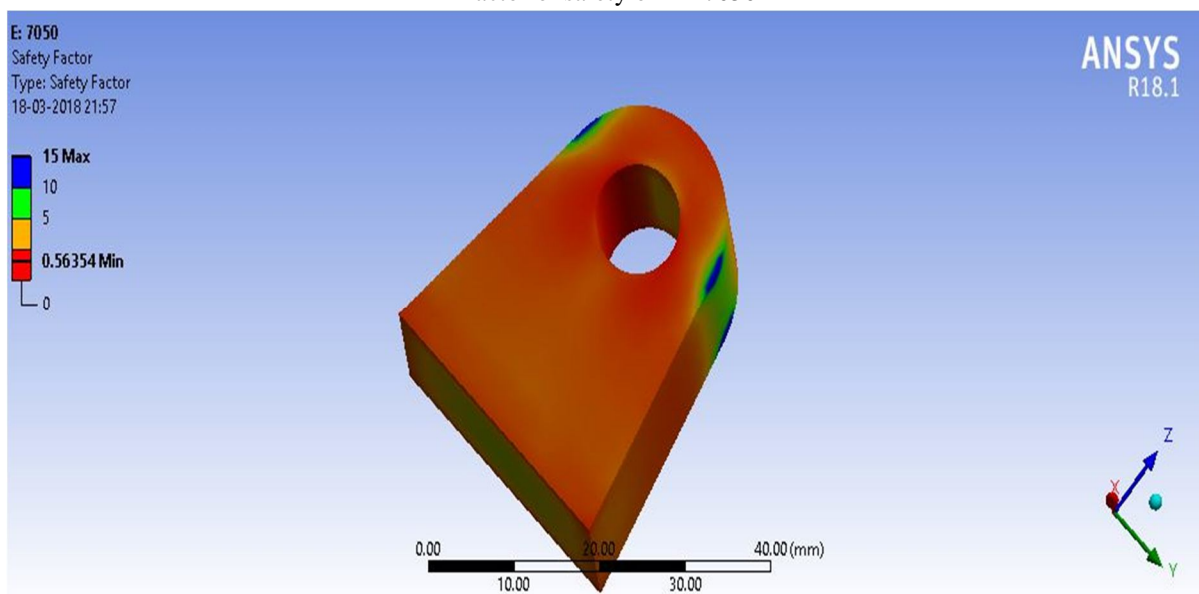
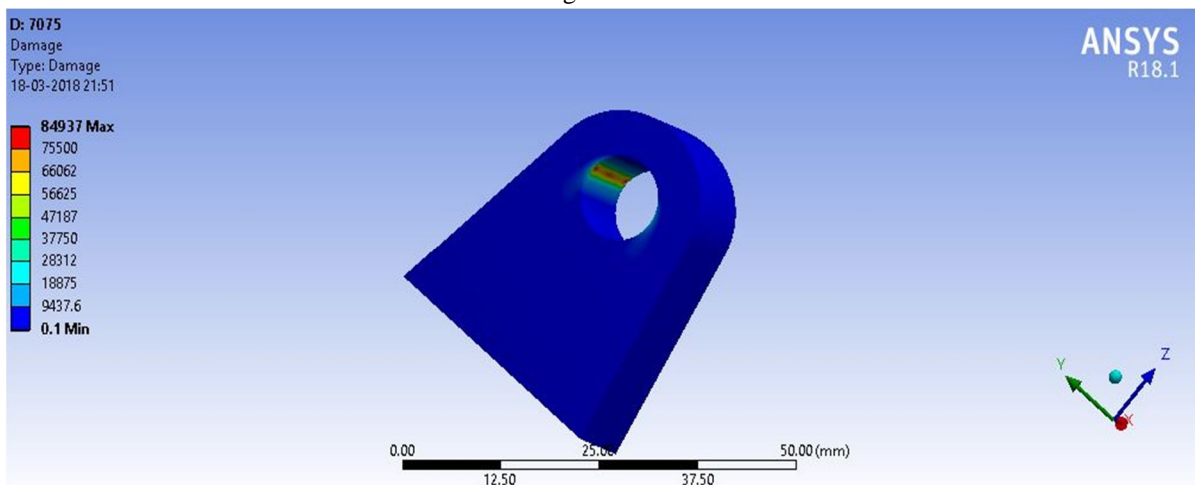*B. Fatigue analysis of al a 7075*

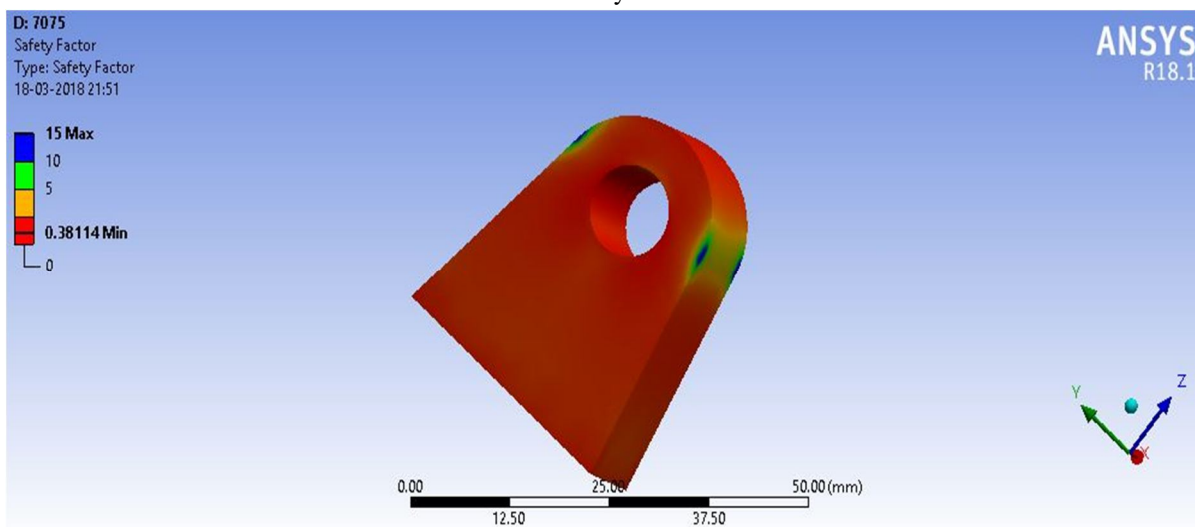Total deformation of Al 7075
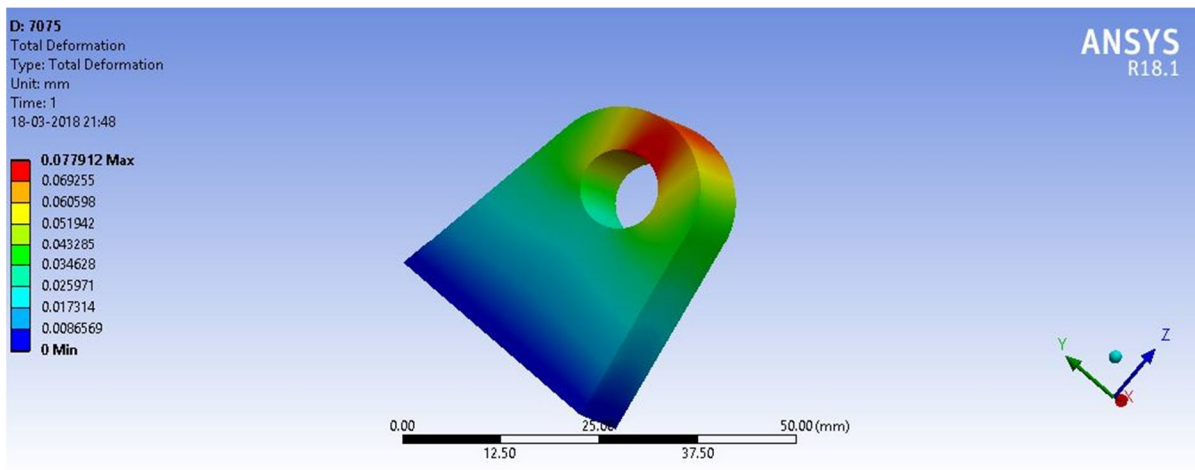
Equivalent stress of Al 7075
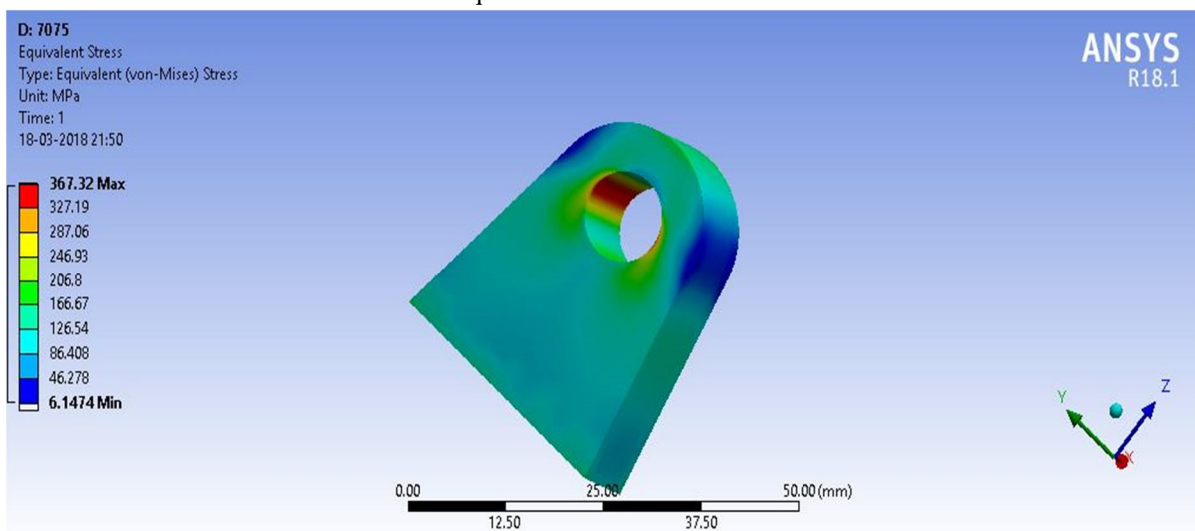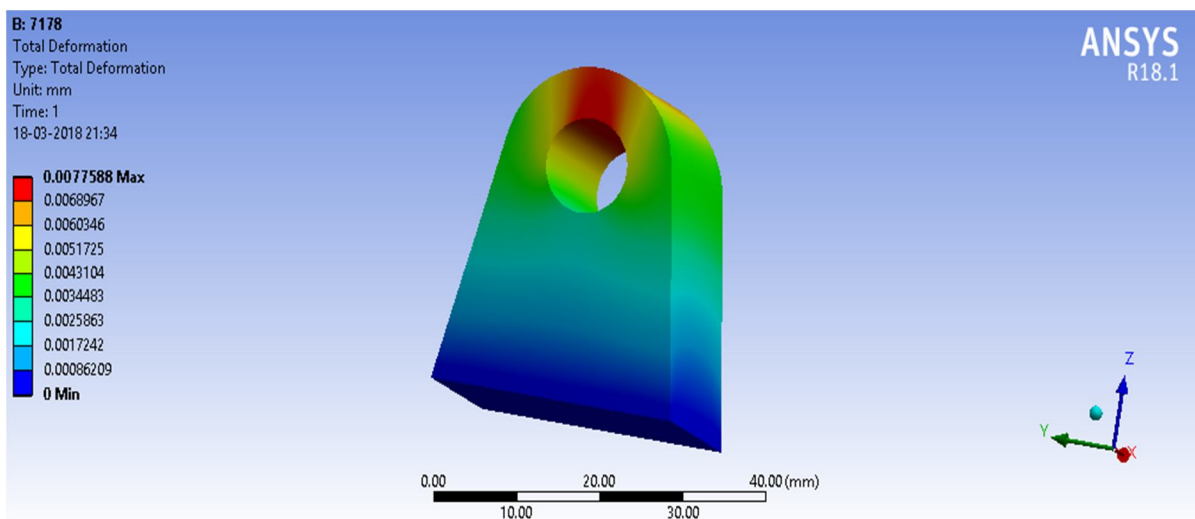

Fatigue life of Al 7075

Damage of Al 7075

Factor of safety of Al 7075
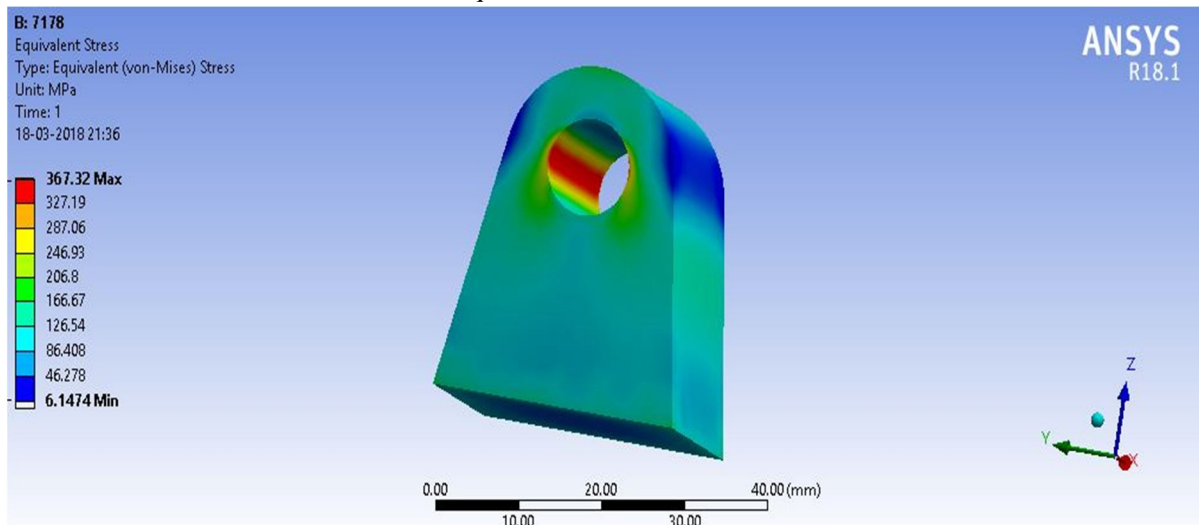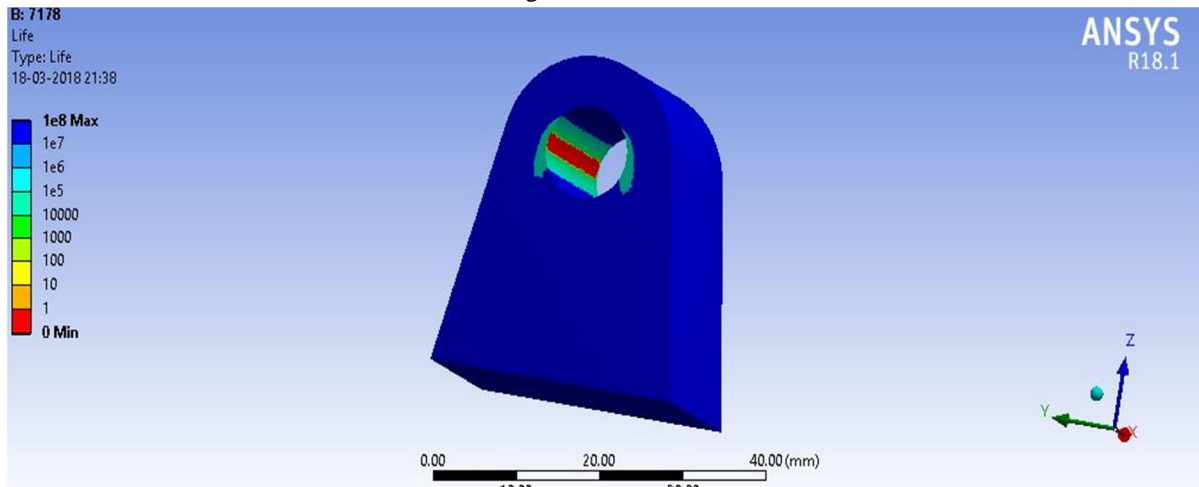

C. Fatigue Analysis Of Al 7178
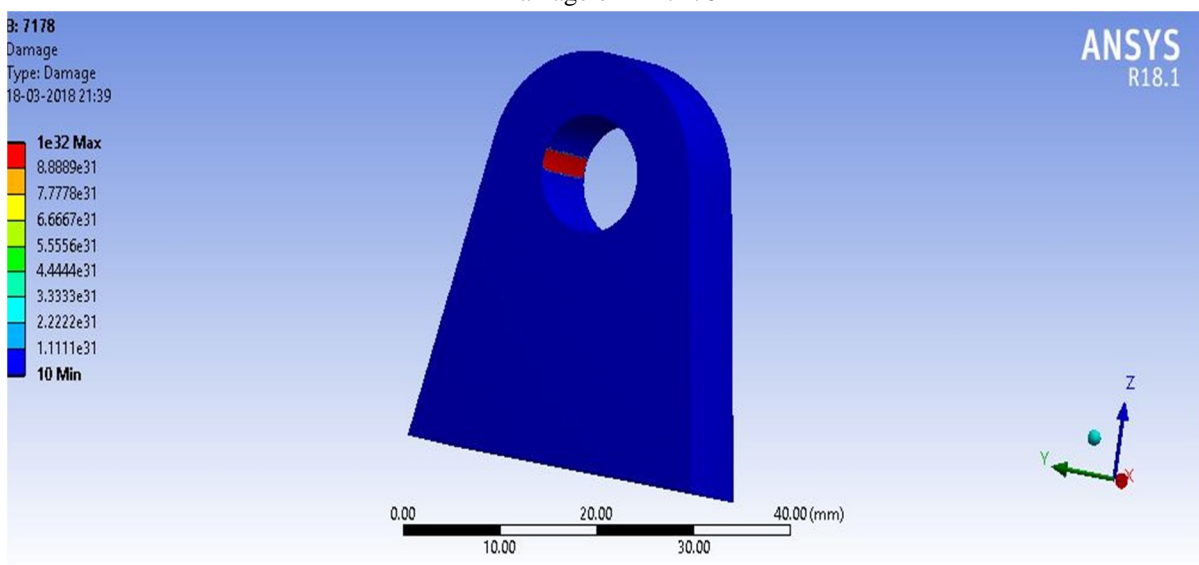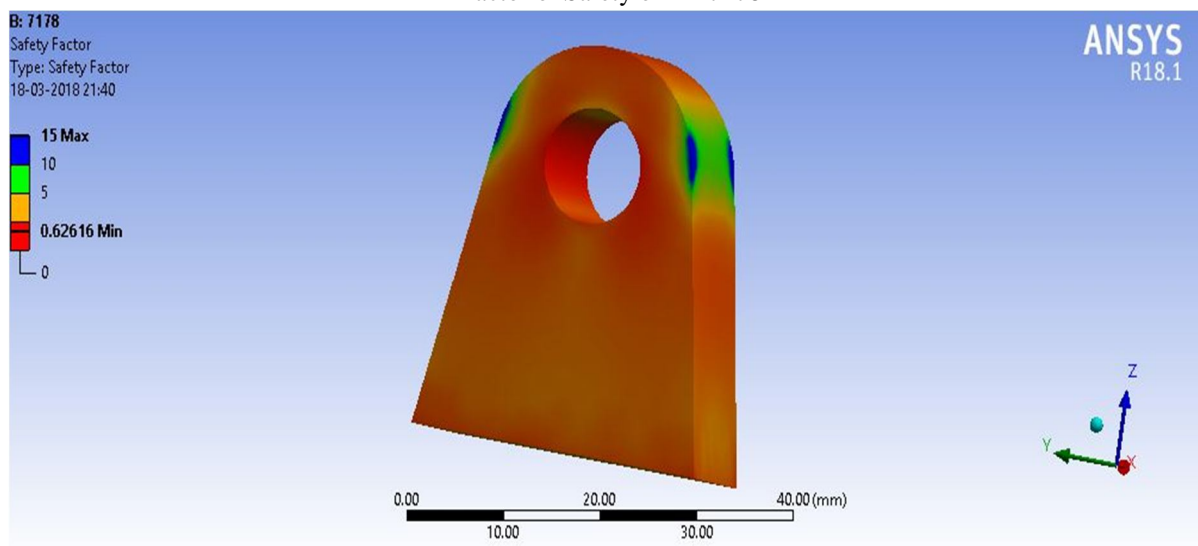
Total deformation of Al 7178

Equivalent stress of Al 7178

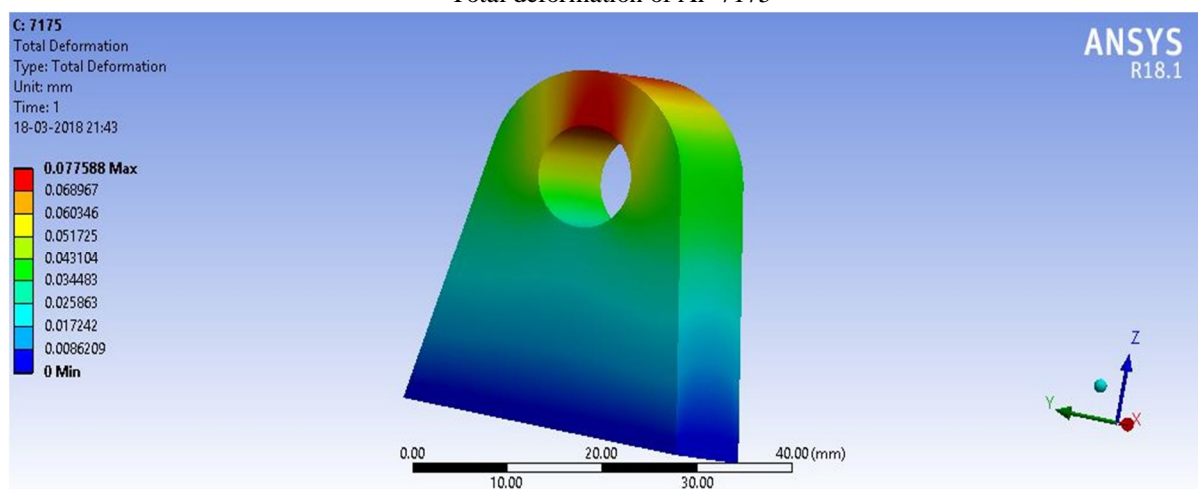Fatigue life of Al 7178

Damage of Al 7178

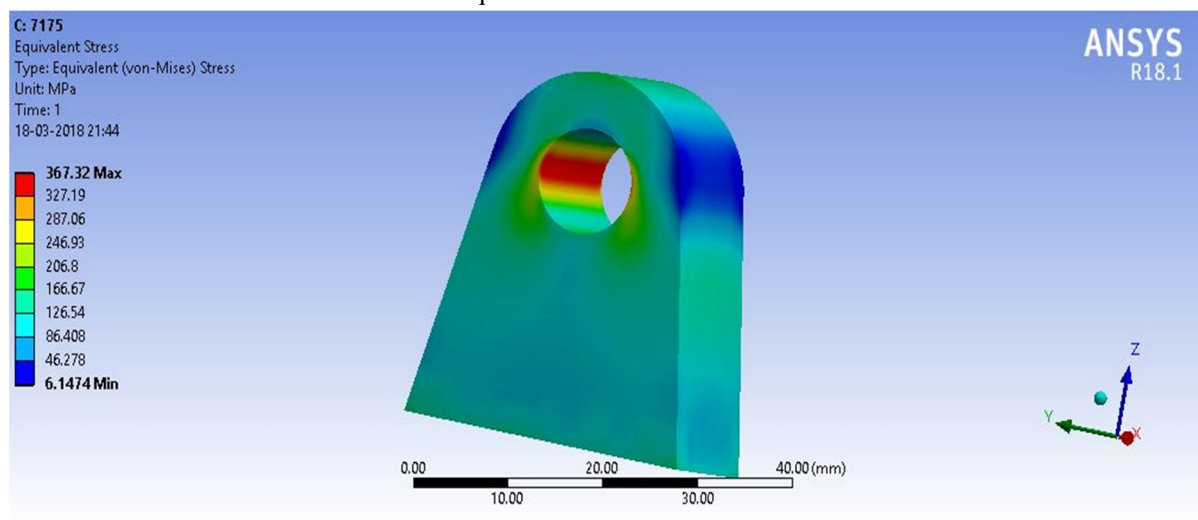Factor of Safety of Al 7178
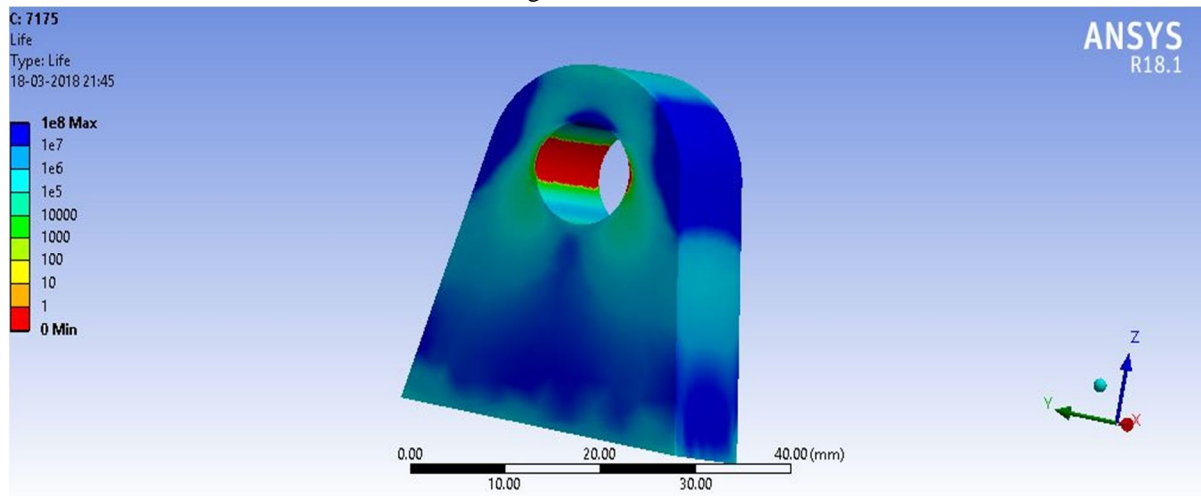

D. *Fatigue Analysis Of Al A 7175*

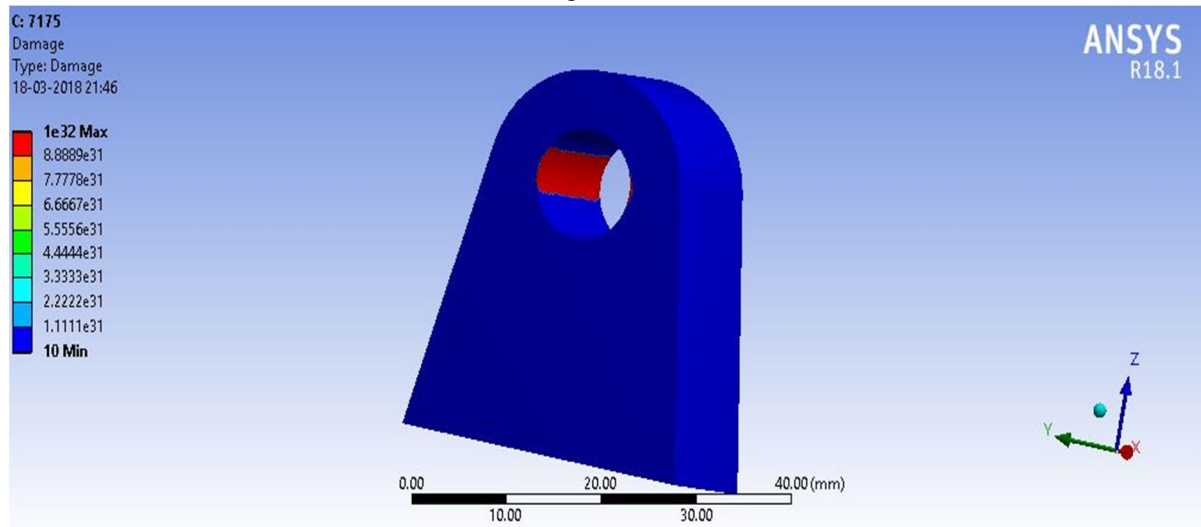Total deformation of Al 7175

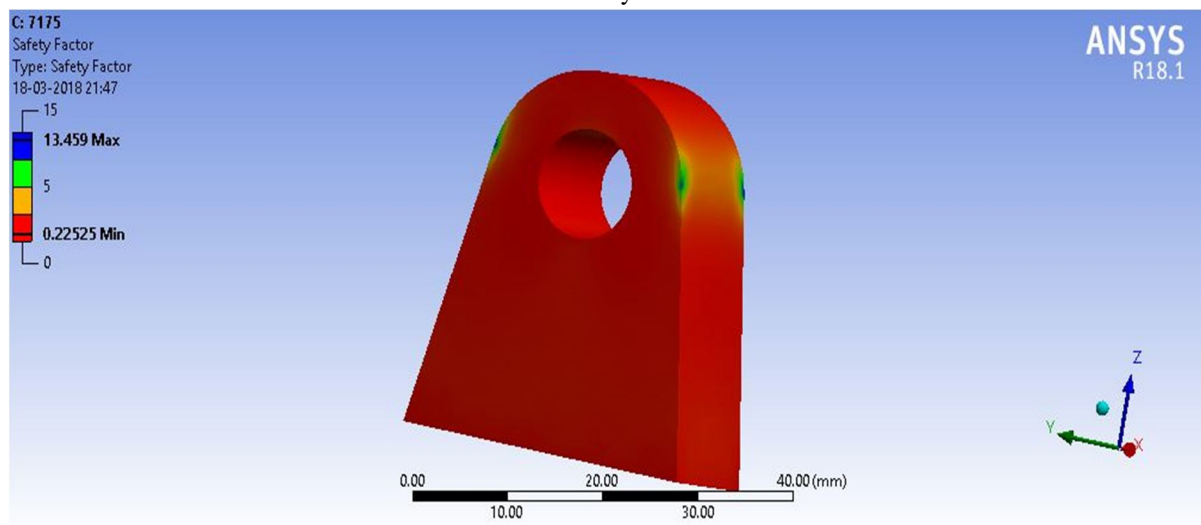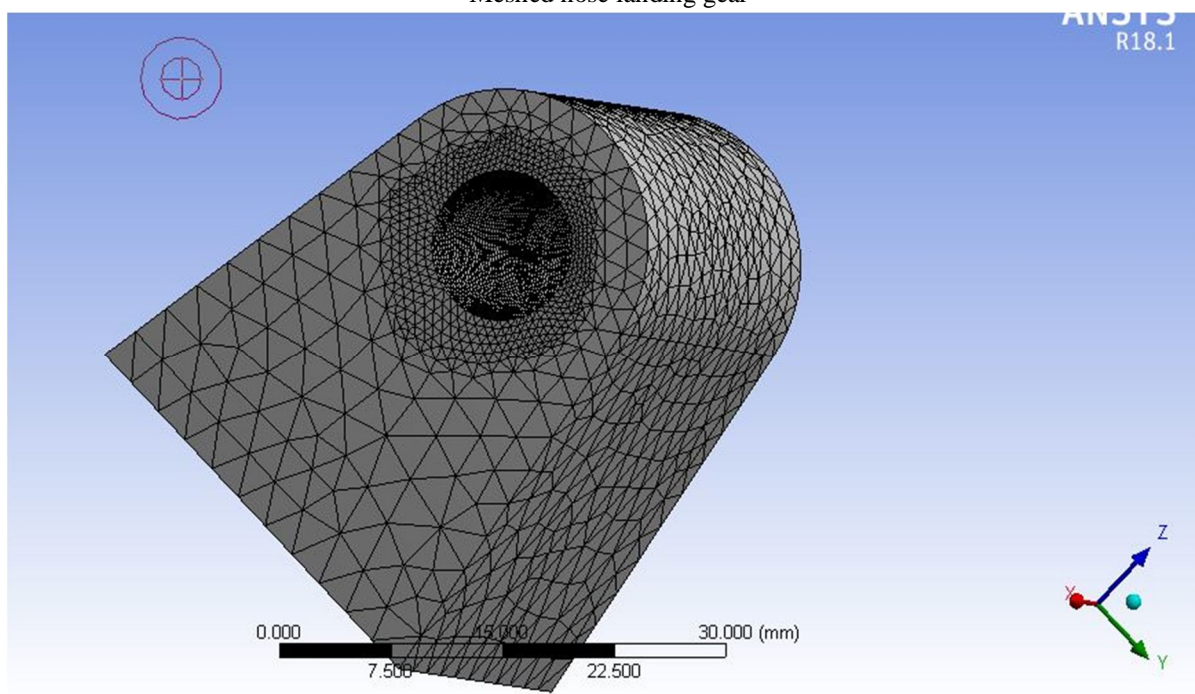Equivalent stress of Al 7175

Fatigue life of Al 7175

Damage of Al 7175

Factor of safety of Al 7175

Meshed nose landing gear

VI. CONCLUSION

This project work present a computational model for the fatigue analysis of the lug joint in the nose landing gear. The dimensions of the proposed model are obtained by the strength of material approach and the stress analysis and the fatigue life is estimated. For this estimation finite element analysis tool is used. Stress analysis of the lug is carried out and maximum stress is identified around the hole of lug which is found out to be lower than yield strength of material. So, the lug design is safe. For this design, life of the lug in the nose landing gear is $1*10^{10}$ cycles for Al T6 7075 which is greater than other aluminium alloys like Al 7050, Al 7178, Al 7175 through comparison of fatigue analysis.

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