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Design, Modelling & Simulation Analysis of Electromagnetic Pulse (EMP) Coupling to Microstrip

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Abstract: This paper is to analyze the EMP coupling to microstrip using 3D EM Modeling and Simulation Analysis. Developed bounded wave transmission line structure as per MIL-STD 461, RS105 EMP requirement in terms of peak electric field of 50KV/m with rise time-2.3ns and pulse width-25ns. Microstrip is modeled. EMP Coupling to cables was carried out by placing the microstrip under generated EMP field in terms of induced voltage and currents due to EMP fields.

Keywords: Electromagnetic pulse (EMP), Bounded wave Transmission line, microstrip, EMP field, Coupling.

I. INTRODUCTION

A. Electromagnetic Pulse

An electromagnetic pulse is a short burst of electromagnetic energy. EMP arises from two principal sources, the first of which is the gamma rays emitted by the nuclear detonation. The second significant type of EMP from high altitude bursts is a low frequency, low amplitude field caused by explosion plasma motion in the upper atmosphere. This environment is commonly referred to as magneto-hydrodynamic EMP or MHD EMP. EMP have devastating effect on the unprotected electronics systems.

Gamma rays represent about 1/1000th of the total bomb energy and are emitted within ten billionths of a second. The amount of gamma emitted by a one- megaton detonation is about 4 X 10¹² Joules. The gamma rays, by a process known as the “Compton Effect,” strip electrons from air molecules to create a large-scale electron current in the upper atmosphere. This electron current is deflected by the earth’s magnetic field and thereby radiates an intense electromagnetic pulse (EMP) over extensive portions of the earth’s surface. Effects extend to ground areas within the line-of-sight of the burst as shown in fig.

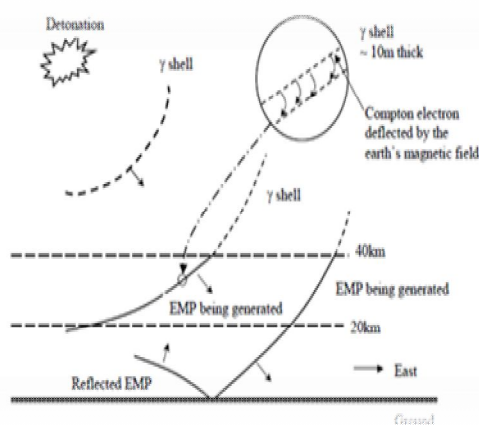


Fig. 1 Mechanism of gamma-induced EMP from a high-altitude burst

The second significant type of EMP from high altitude bursts is a low frequency, low amplitude field caused by explosion plasma motion in the upper atmosphere. This environment is commonly referred to as Magneto hydrodynamic EMP or MHD EMP. The plasma created by the explosion perturbs the earth’s magnetic field which, in turn, generates electric fields on the Earth’s surface and the upper layers of the ground.

B. Microstrip

Microstrip is used for transmission of microwave-frequency signals. Substrate separates the conductor and the ground plane. From microstrip, Microwave components can be formed such as antennas, power dividers, couplers, filters etc. with the entire device existing as the pattern of metallization on the substrate. As compared to other traditional waveguide technology Microstrip is less expensive, lighter weight and more compact. Microstrip lines are used in high-speed digital PCB designs, where signals need to be routed from one part of the assembly to another with minimal distortion, and avoiding high cross-talk and radiation.

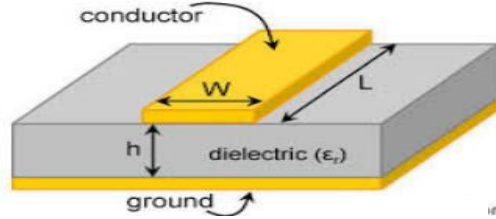
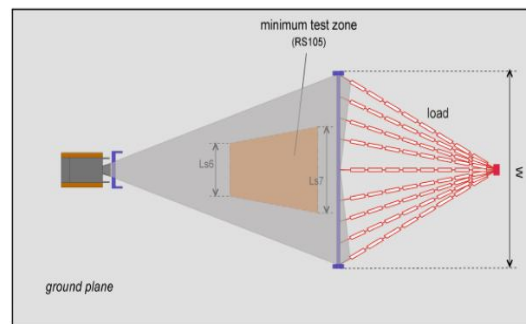
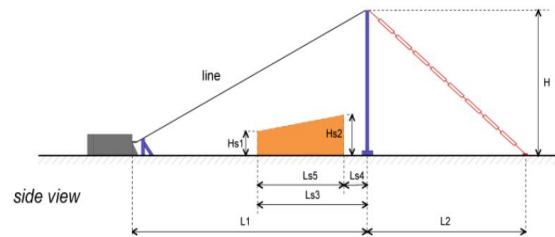


Fig.2 Microstrip

II. BOUNDED WAVE TRANSMISSION LINE STRUCTURE

Transverse electromagnetic (TEM) cell type of triangular transmission line with a matching termination resistor bank will be best structure for generating EMP pulse with minimum distortions. Generally radiating lines will be made with multiple metal wires terminated with distributed load resistors. Bottom ground plane resistors will of metallic mesh for simulation the TEM cell type structure.



top view

Fig.3 Radiation Line (Triangular)

In the triangular radiation line, the pulse produced by the HV generator is transformed into a TEM electromagnetic field travelling in the direction of the load. Because there is no discontinuity along the line, no other electromagnetic modes than TEM are exited. Some reflections are induced due to the construction of load.

In the parallel plate, between the slope (triangular part) and the flat part the wave is travelling up to the transition placed. In this region other modes than TEM are produced that induce reflections and field distortions. At the end of the flat part process is repeated and finally the reflections are influenced by terminated load.

Hence we are going to consider the triangular plate structure for the EMP test set up to perform RS105 tests according MIL-STD 461-E/F.

A. Modeling Of Bounded Wave Transmission Line Structure

Modelled bounded wave transmission line structure with matched terminated resistors for generating standardized EMP field. As an input Double Exponential voltage pulse is given and measured at equipment zone area.

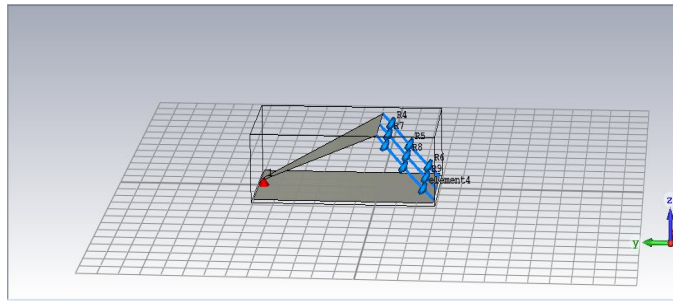


Fig.4 CAD model of Bounded Wave Transmission Line structure

We placed probes at the place of EUT to measure the E.F at each probe. As shown in figure below-

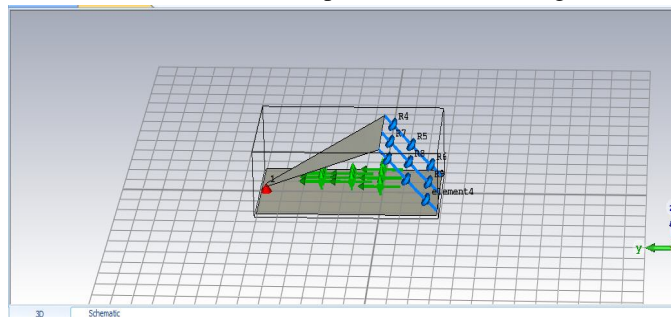


Fig.5 CAD model of Bounded Wave Transmission Line structure with probes

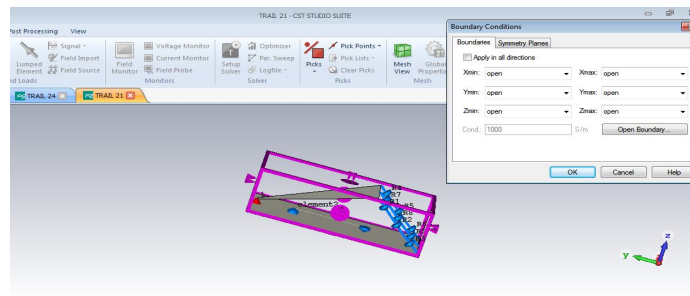


Fig.6 Boundary condition applied in all directions

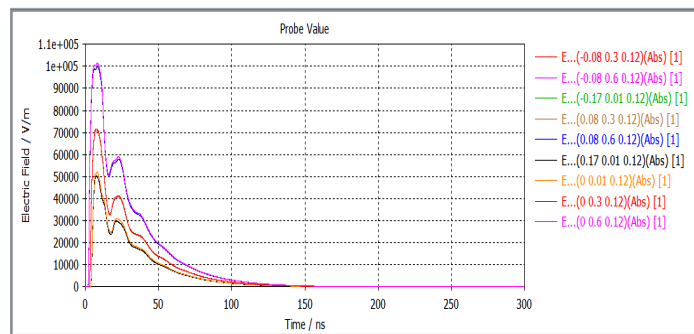


Fig.7 Electric field obtained at different probes

Input here given is 25KV, as the upper plate is kept at height 0.50 m. E.F obtained at EUT zone is more than 50 KV/m as per MIL-STD 461, RS105 EMP requirement.

III.SIMULATION

A. Microstrip Inside Bounded Wave Transmission Line Structure

In this we have placed microstrip inside Bounded Wave Antenna Structure at EUT and observe the coupling effect. There are four resistors- source resistor, near end resistor, far end resistor and load resistors, R_s , R_{ne} , R_{fe} , R_l 50 ohm each respectively as shown in figure. As an input Double Exponential voltage pulse is given and measured at equipment zone area.

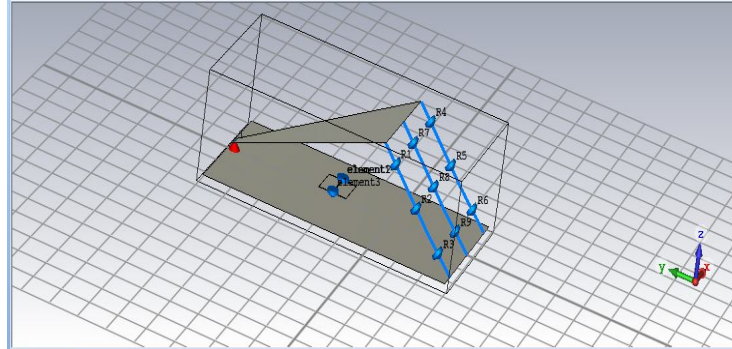


Fig 8 CAD model of Microstrip placed inside Bounded Wave Transmission Line Structure

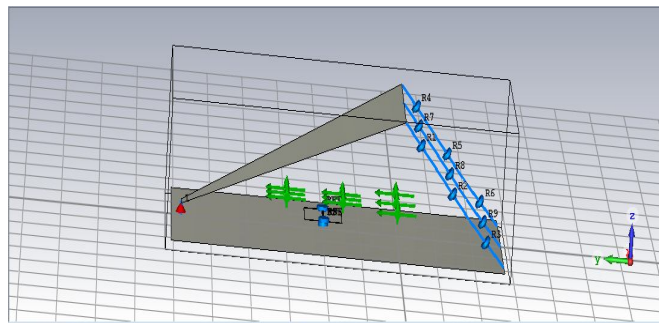


Fig .9 CAD model of Microstrip placed inside Bounded Wave Antenna Structure with probes

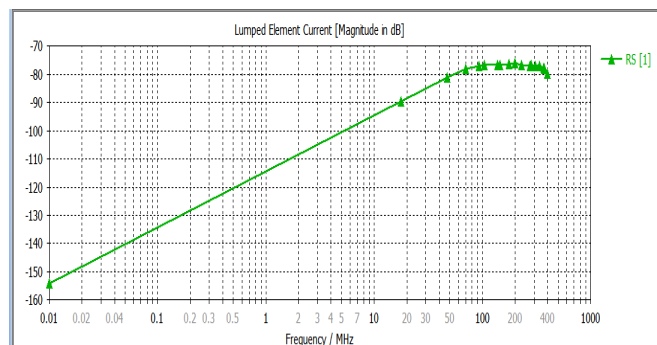


Fig .10 Current across lumped element R_s

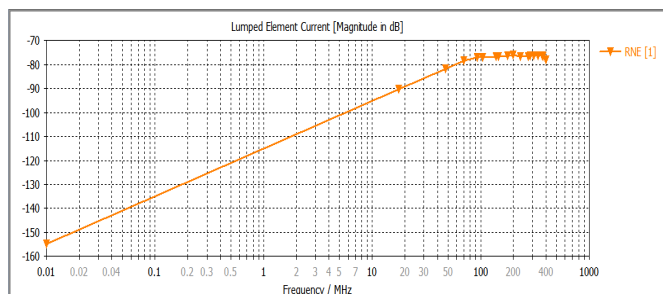


Fig .11 Current across lumped element R_{ne}

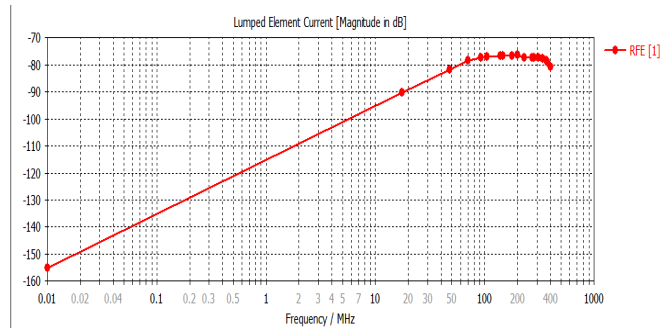


Fig .12 Current across lumped element RfE

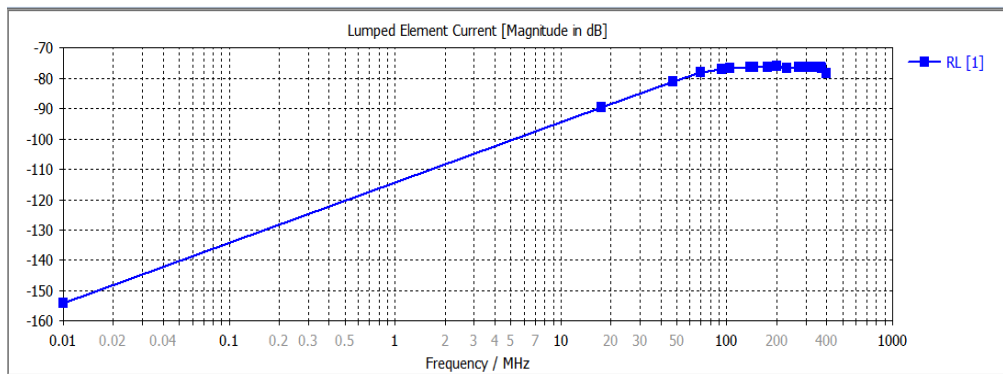


Fig .13 Current across lumped element RL

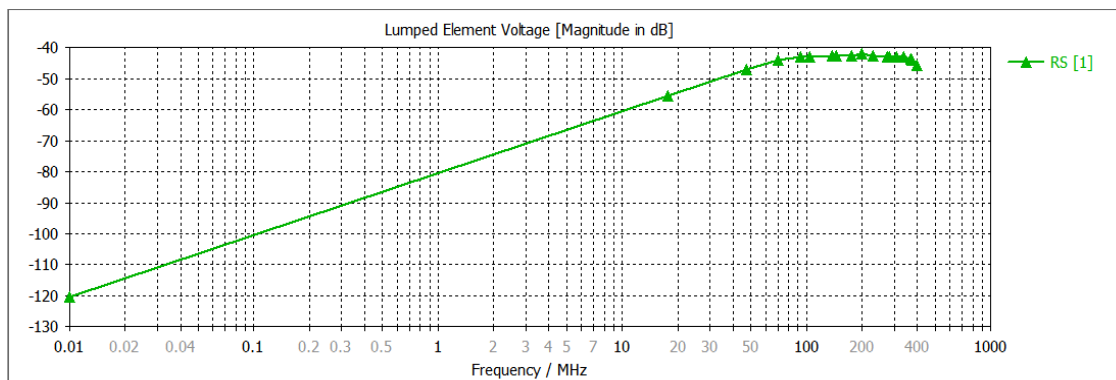


Fig.14 Voltage across lumped element Rs

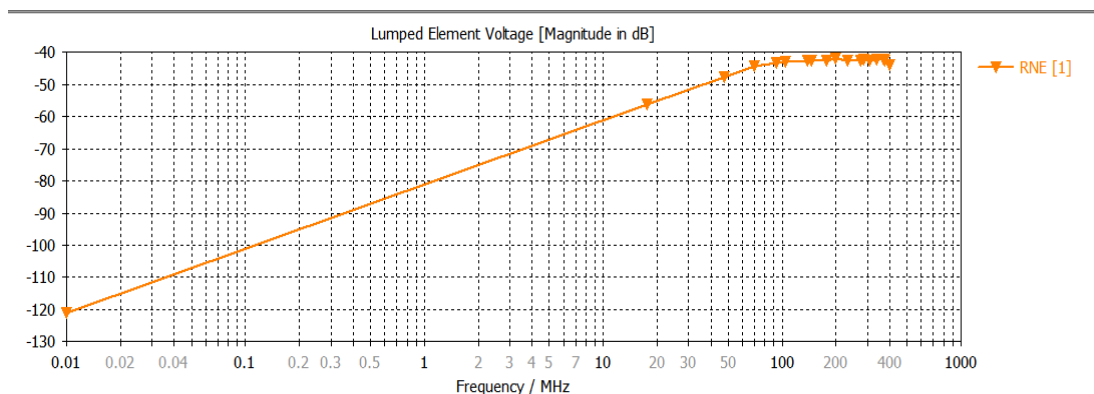


Fig .15. Voltage across lumped element Rne

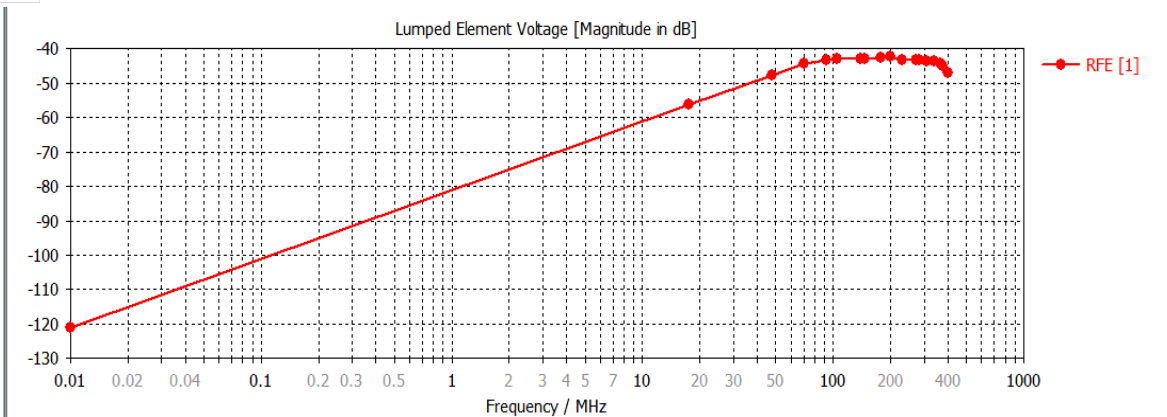


Fig .16 Voltage across lumped element Rfe

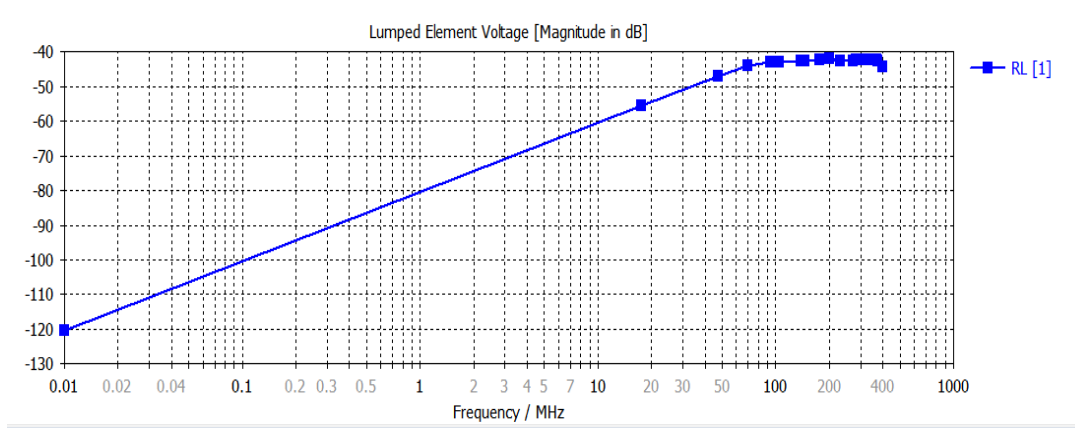


Fig .17 Voltage across lumped element RL

B. Microstrip With Source Inside Bounded Wave Transmission Line Structure

In this we have placed microstrip inside Bounded Wave Antenna Structure at EUT and observe the coupling effect. There are 2 ports. Port 1 is discrete port which is connected between the ground plate and upper plate and port 2 is a waveguide port which is connected to one of the strip and the ground of the microstrip. Rest three are connected with resistors- near end resistor, far end resistor and load resistors , Rne, Rfe, RL 50 ohm each respectively as shown in figure. As an input Double Exponential voltage pulse is given and measured at equipment zone area.

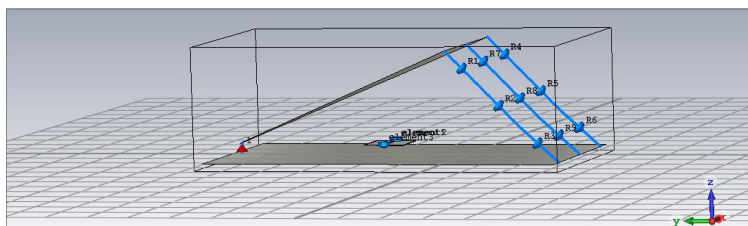


Fig 18 CAD model of Microstrip placed inside Bounded Wave Transmission Line Structure

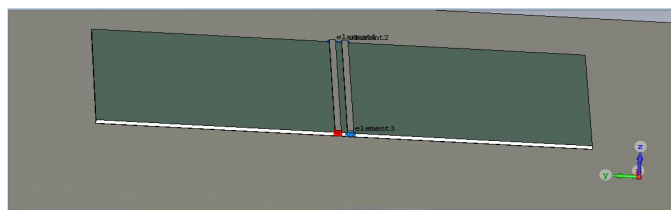


Fig 19 Microstrip

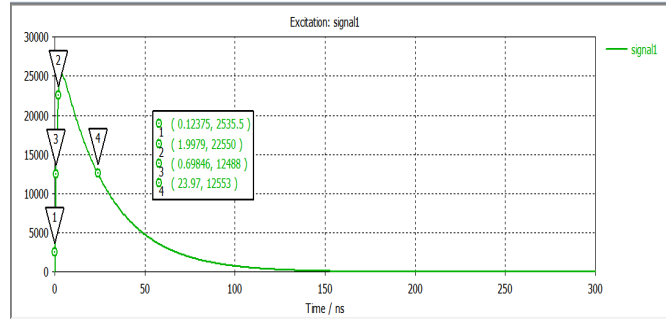


Fig 20 Double exponential Pulse

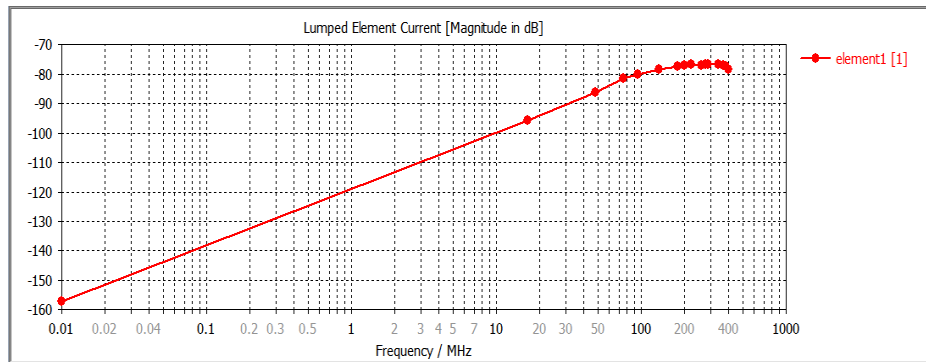


Fig .21 Current across lumped element Rl

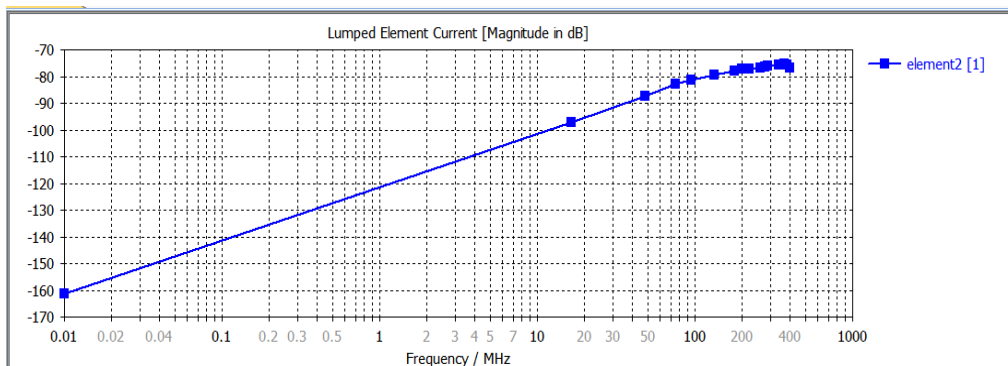


Fig .22 Current across lumped element Rfe

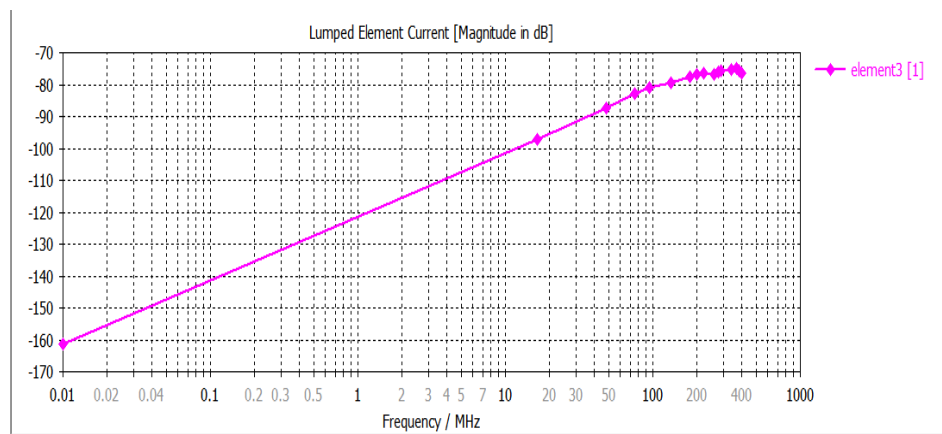


Fig .23 Current across lumped element Rne

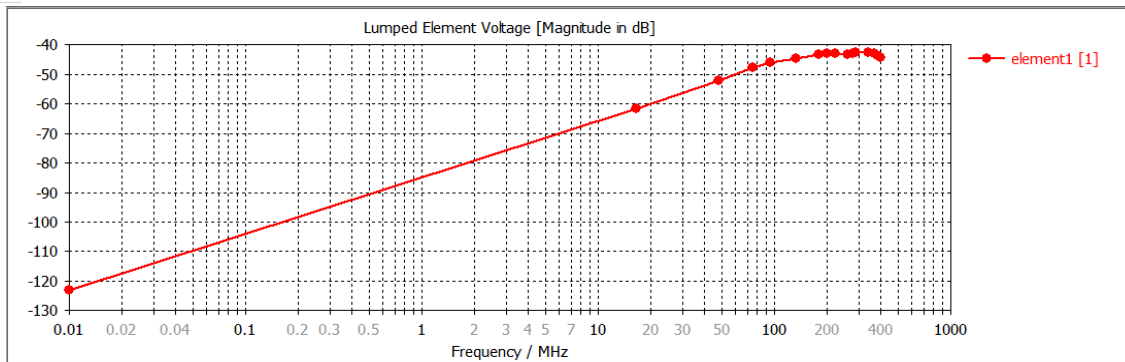


Fig.24 Voltage across lumped element Rl

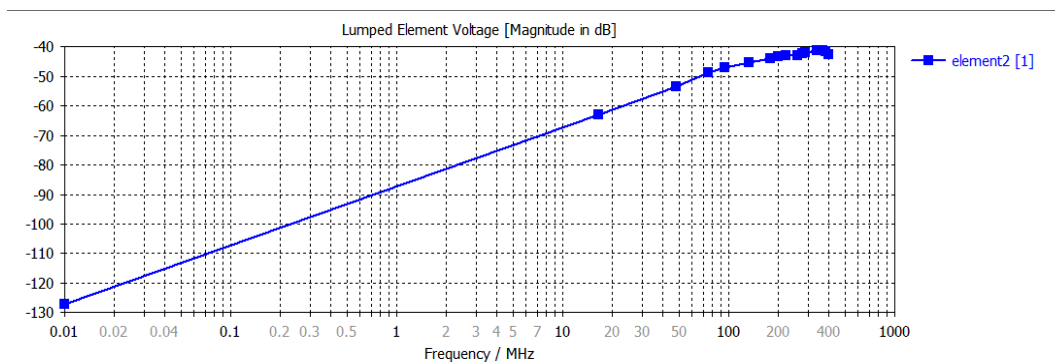


Fig.25 Voltage across lumped element Rfe

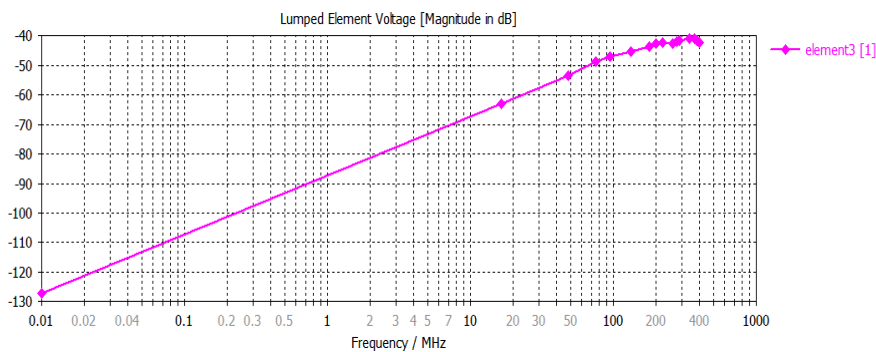


Fig.26 Voltage across lumped element Rne

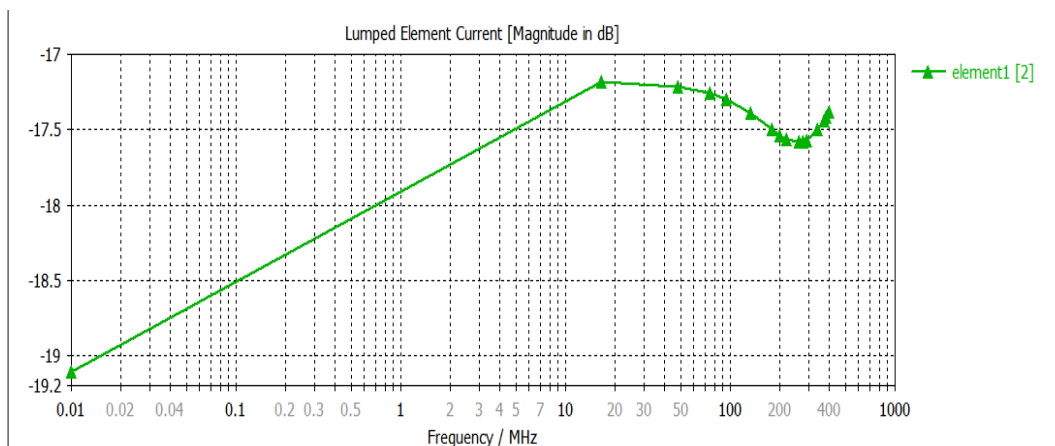


Fig.27 Current across lumped element Rl due to port2

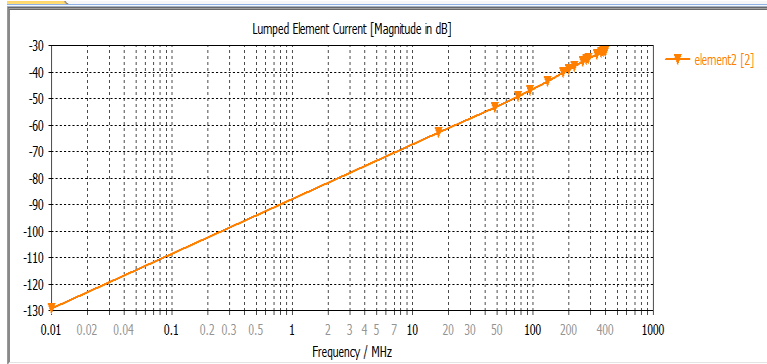


Fig .28 Current across lumped element Rfe due to port2

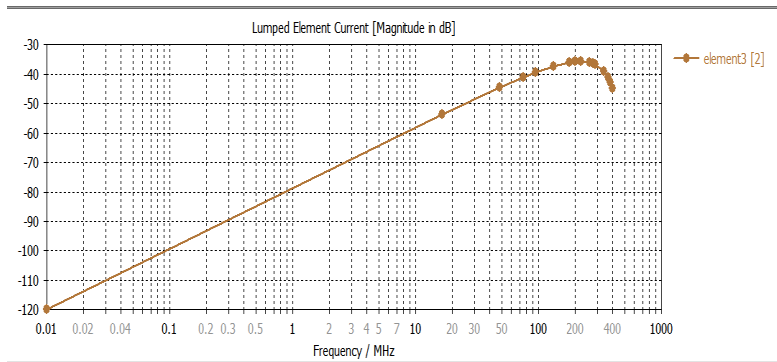


Fig.29 Current across lumped element Rne due to port2

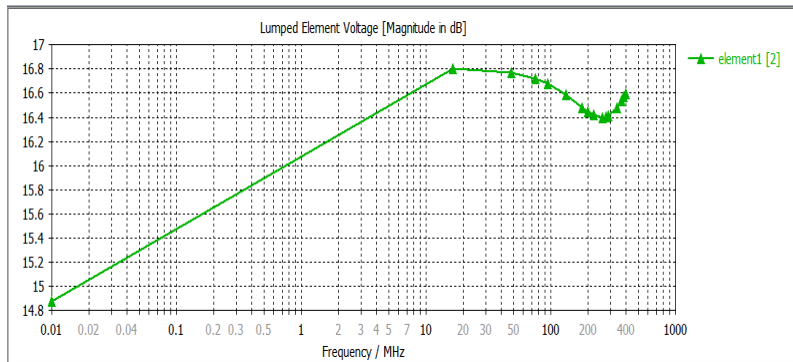


Fig.30 Voltage across lumped element RI due to port2

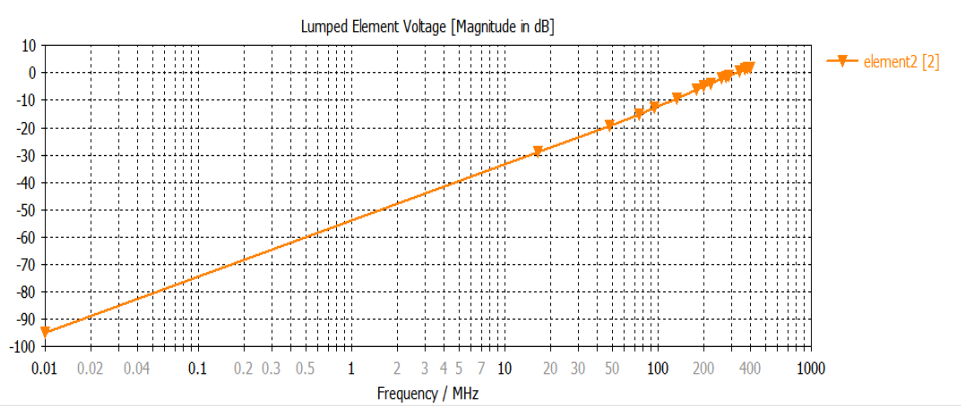


Fig.31 Voltage across lumped element Rfe due to port2

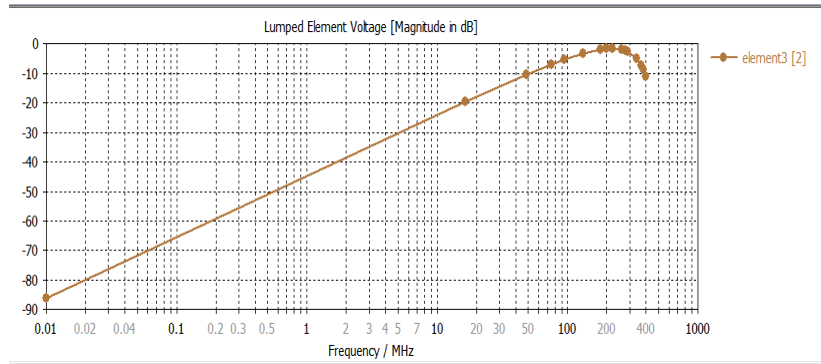


Fig.32 Voltage across lumped element Rne due to port2

C. Microstrip

In this we have modelled microstrip. Microstrip consists of three layers- conductor, dielectric layer, and ground. There are two strips. In one strip one side is connected to port 2 (waveguide port) and other side with load resistor and other strip both the side is connected with both the resistors near end resistor and far end resistors with all the resistor 50 ohms each.

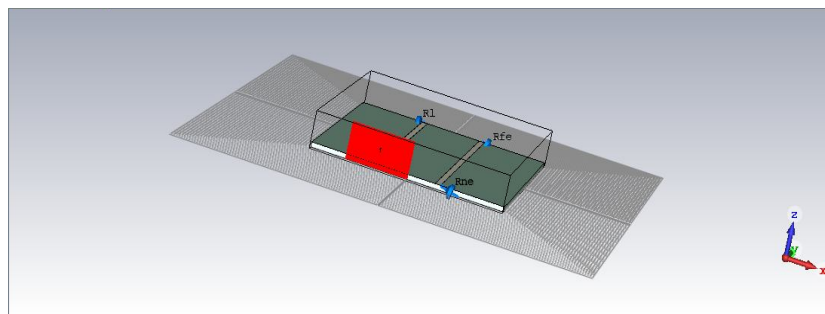


Fig.33 CAD model of Microstrip

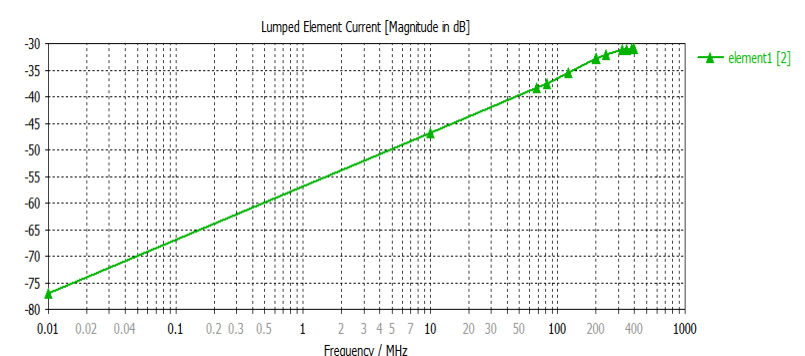


Fig .34 Current across lumped element Rl

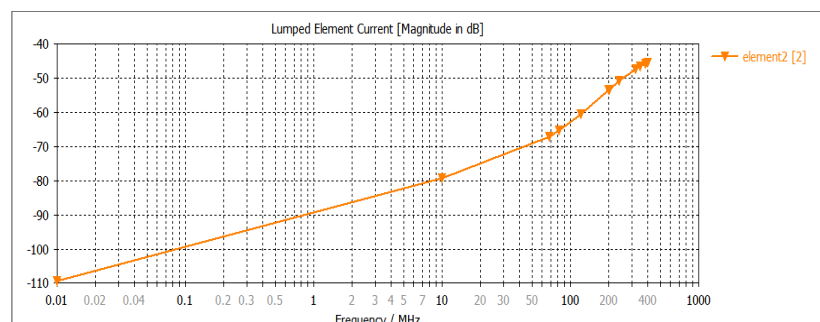


Fig .35 Current across lumped element Rfe

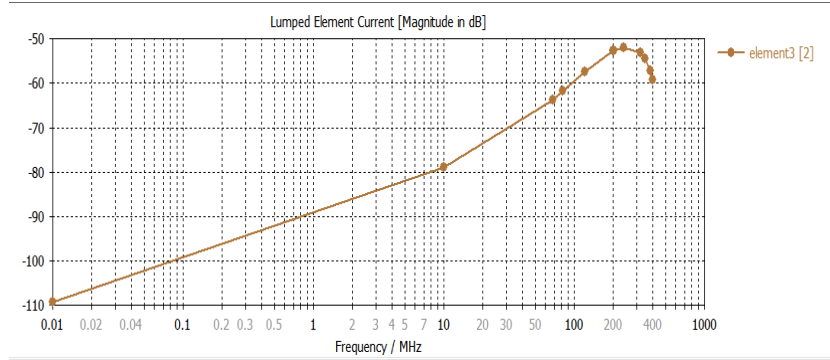


Fig .36 Current across lumped element Rne

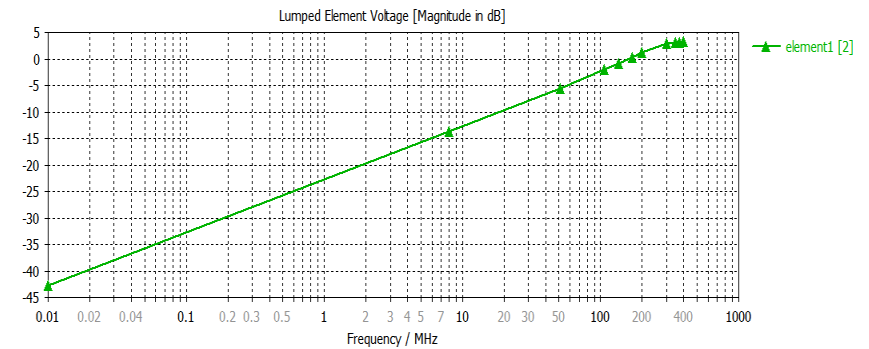


Fig .37 Voltage across lumped element Rl

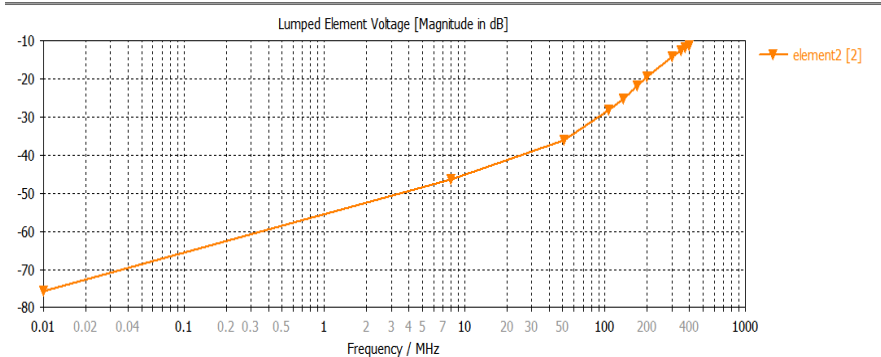


Fig .38 Voltage across lumped element Rfe

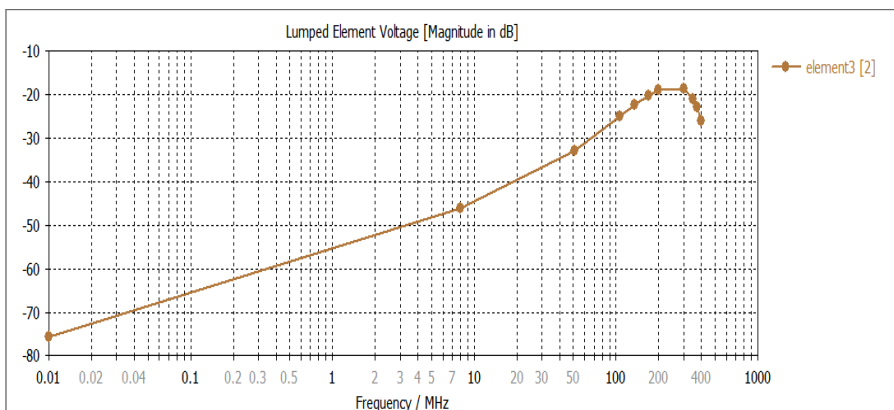


Fig .39 Voltage across lumped element Rne

IV. RESULT

Table1. Comparison of current and voltage (in dB) at 100MHz

RESISTORS	MICROSTRIP (with source) (at 100MHz)		MICROSTRIP PLACED INSIDE THE BWT (at 100MHz)		MICROSTRIP WITH SOURCE PLACED INSIDE THE BWT (at 100 MHz)			
	Voltage (in dB)	Current (in dB)	Voltage (in dB)	Current(in dB)	Due to port 1		Due to port 2	
					Voltage (in dB)	Current (in dB)	Voltage (in dB)	Current (in dB)
Rs	-	-	-42	-78	-	-	-	-
R ne	-25	-37	-42	-78	-50	-80	-5	-40
R fe	-30	-67	-42	-78	-50	-80	-15	-45
R l	-2.5	-37	-42	-78	-50	-80	16.7	-17.25

V. CONCLUSION

Bounded Wave Transmission Line Structure is modeled. The electric field at different positions ($h/3$, $w/2$) within EUT volume is measured using E-Field probe. EMP Coupling to microstrip was carried out by placing the microstrip under generated EMP field in terms of induced voltage and currents due to EMP fields. The microstrip coupling was analyzed with both EMP and without EMP as well as with and without source. Thus from the analysis it can be said that microstrip under the EMP will have more coupling as compared to the microstrip without EMP with source connected to one of the strip of the microstrip. Whereas coupling is less in the microstrip in which both the strips are connected to the four resistors.

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