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# Study of Pushover Analysis and Column Removal in Multi-Storey Building

Dr. S. G. Makarande<sup>1</sup>, S. P. Bezalwar<sup>2</sup>, Prof. G. D. Dhawale<sup>3</sup>, Prof. M. M. Lohe<sup>4</sup>

<sup>1, 2, 3, 4</sup>Department of Civil Engineering, Bapurao Deshmukh College of Engineering, Sewagram, India

**Abstract:** In this paper, a 3D finite element modelling is used to analysis the consecutive column removal scenario of multi storey steel building with composite steel frames. The nonlinear static analysis procedure was performed to check the behavior of structure under consecutive column removal scenarios. The analysis of the structure was detailed examined and displacement, base shear, plastic hinges are analysed in details.

**Keywords:** Finite element, Consecutive column removal, Modelling, Displacement, Base shear, Plastic hinges.

## I. INTRODUCTION

The structural components in a typical multi-storey building, consists of a floor system which transfers the floor loads to a set of plane frames in one or both directions. The floor system also acts as a diaphragm to transfer lateral loads from wind or earthquakes. The frames consist of beams and columns and braces. As the height of the building increases beyond ten stories (tall building), it becomes necessary to reduce the weight of the structure for both functionality and economy. For example a 5% reduction in the floor and wall weight can lead to a 50% reduction in the weight at the ground storey. This means that the columns in the lower storeys will become smaller leading to more availability of space and further reduction in the foundation design.

## II. LITERATURE REVIEW

The earlier research carried out by various authors are studied in brief as follows,

Suraj B. Gaikwad, Prof. Mukund M. Pawar (2017)<sup>[1]</sup> present study is to analysis the progressive collapse of regular and irregular steel structure. For this G+15 regular as well as irregular building with missing column at different locations has been taken. For this linear static analysis, linear dynamic analysis, nonlinear static and nonlinear dynamic analysis of structure has been carried out. To compare the progressive collapse responses 2D and 3D models are prepared. Percentage change in the values of base shear, demand capacity ratio and roof displacement considering progressive collapse effect of structures has been carried out.

C. R. Chidambaram, Jainam Shah, A. Sai Kumar and K. Karthikeyan (2016)<sup>[2]</sup> paper has analyzed G+7 moment resisting steel frame residential building was analyzed using ETABS to predict the sensitivity of the structure to progressive collapse due to fire loads. Columns at different levels were Lekhraj Pandit, R. R. Shinde (2015)<sup>[3]</sup> given a temperature of 550°C with reduced material properties and yield strength as per code IS 800. Progressive collapse load combination was adopted as per GSA guidelines. Corner, edge, intermediate and re-entrant columns were removed separately at alternate storeys. The lower storeys were found to be more susceptible than the upper storeys. Lekhraj Pandit, R. R. Shinde (2015)<sup>[3]</sup> paper aims to investigate the performance of steel bracing steel structure. In this project a steel building model is taken, this model is compared in different aspects such as axial force and bending moment in column and story displacement. Using different sections as bracing at critical storey Among these numbers of trials which type of bracing at critical section is more suitable from the observed results would be selected for the structure.

H. R. Tavakoli, F. Kiakojouri (2013)<sup>[5]</sup> present the study about progressive collapse capacity of steel moment frames was first investigated using alternate load path method, then a nonlinear dynamic analysis was carried out to examine the response of the steel moment frames in blast and sudden column loss scenario. The structural response of the building under sudden loss of column for different scenarios of column removal, with or without external blast loading was assessed in detail.

Feng Fu (2009)<sup>[8]</sup> paper presents a 3-dimensional finite element modelling technique developed by the author was used to analyse the progressive collapse of multi-storey buildings with composite steel frames. The nonlinear dynamic analysis procedure was performed to examine the behaviour of the building under consecutive column removal scenarios.

Kapil Khandelwal, Sherif El-Tawil, Fahim Sadek (2009)<sup>[9]</sup> study is conducted on previously designed 10-story prototype buildings by applying the alternate path method. In this methodology, critical columns and adjacent braces, if present, are instantaneously removed from an analysis model and the ability of the model to successfully absorb member loss is investigated. Member removal in this manner is intended to represent a situation where an extreme event or abnormal load destroys the member.

### III. METHODOLOGY

Analysis was done using ETABS 2016 software

- A. Analysis was done assuming that the building is a Steel building.
- B. Footing was idealized as fixed support.
- C. The load cases adopted are dead load and live load, wind load and the seismic load.
- D. Analysis was done for the load combinations given below:
  - 1) Dead load + live load
  - 2) Dead load + live load + wind load in (+ve) x – direction
  - 3) Dead load + live load + wind load in (- ve) x – direction
  - 4) Dead load + live load + earthquake load in (+ ve) x – direction
  - 5) Dead load + live load + earthquake load in (- ve) x – direction
- a) *General details*
  - i) Total storey: 20
  - ii) Height per storey: 3m
  - iii) Base plan area: 52.5 m x 52.5 m (7.5 m x 7.5 m bay)
- b) *Structural Details*
  - i) *Column Size*
    1. For 1 to 7 storey: 2 ISMB 600 + 20mm Plate
    2. For 8 to 20 storey: 2 ISMB 600
  - ii) *Beam Size*
    1. For all storey: ISMB 500
- iii) *Loads on Structure*
  1. Live load: 1.5 kN/m<sup>2</sup>
  2. Dead Load: 1.5 kN/m<sup>2</sup>
  3. For Linear Static:
  4. Zone factor = 0.24 (Zone IV)
  5. For WIND LOAD:
  6. Basic wind speed: 44 m/s
  7. Terrain category : 2
  8. Risk coefficient (K1) : 1
  9. Topography factor (K2): 1
  10. STEEL : Fe250
  11. CONCRETE : M30
  12. REBAR STEEL: HYSD415

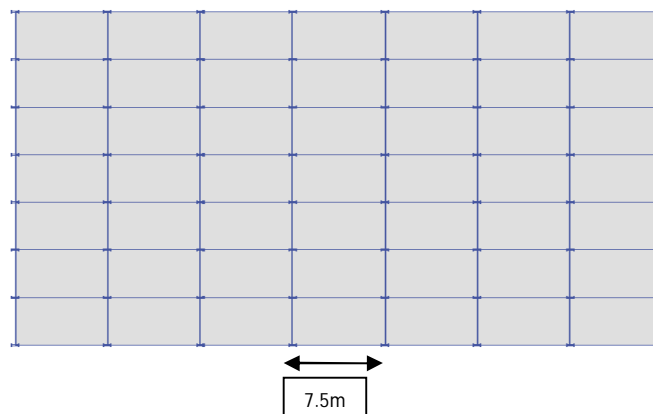


Fig -1: Typical plan of 20-story prototype building

Study of column removal scenario is mainly to get more occupancy. There are other more reason which are explained and sorted out in the United States, the Department of Defence (DoD) and the General Services Administration (GSA). Both employ the alternate path method (APM). The methodology is generally applied in the context of a ‘missing column’ scenario to assess the potential for progressive collapse and used to check if a building can successfully absorb loss of a critical member. FEMA 2002 and NIST 2005 also provide some general design recommendations, which require steel-framed structural systems to have enough redundancy and resilience, allow for alternative load paths and additional capacity redistributing gravity loads when structural damage occurs. Table 1 shows the list of analysis cases considered in this study.

Table -1: Different Column Removal Scenarios

|        | Level of Removal | Removed Column              |
|--------|------------------|-----------------------------|
| Case 1 | Ground Floor     | One Corner Column           |
| Case 2 | Ground Floor     | Two Adjacent Corner Columns |
| Case 3 | 15 th Floor      | One Corner Column           |
| Case 4 | 15 th floor      | Two Adjacent Corner Columns |

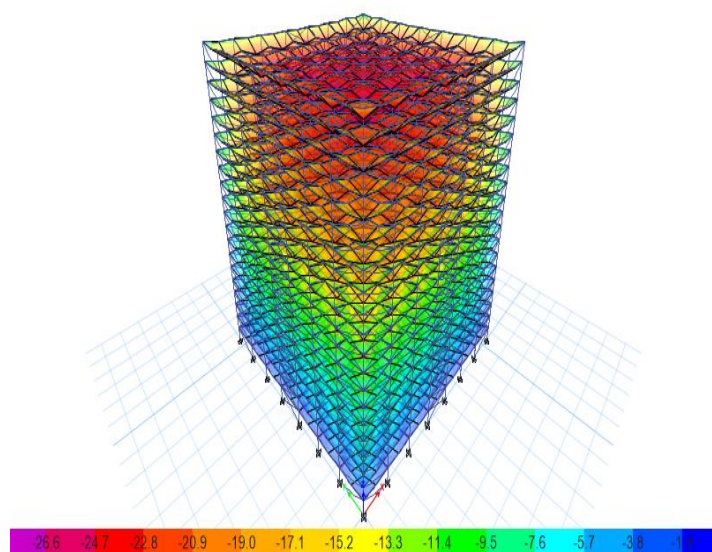


Fig -2: Vertical displacement of model

As shown in Fig. 2, as looking from top floor it shows top floor is in hogging condition and as going to the bottom it is becoming less hogging or in sagging condition.

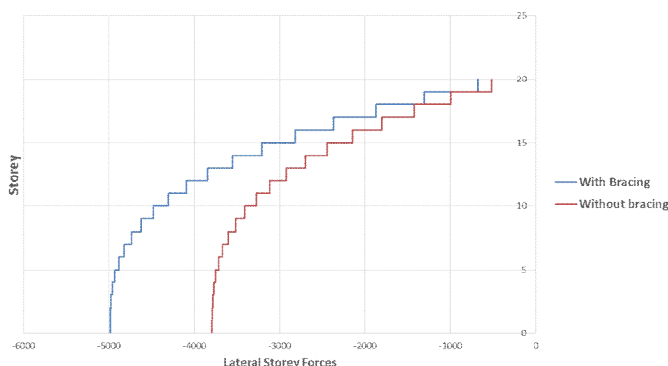


Chart -1: Base Shear



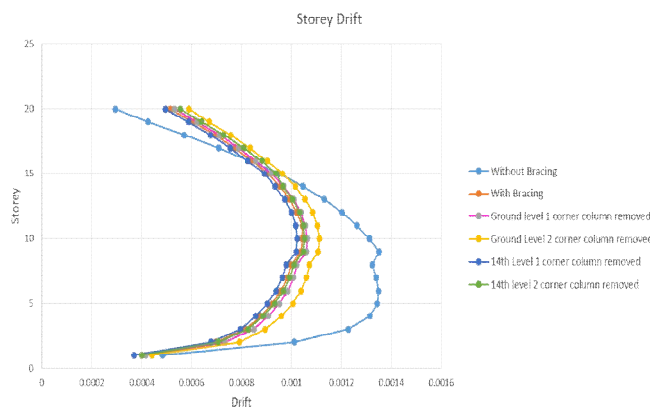


Chart -2: Storey Drift

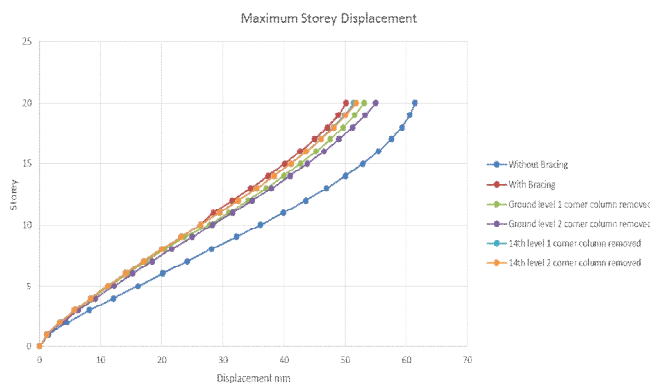


Chart -3: Maximum Storey Displacement

In case 1, the column at ground floor was first removed. It is shown in Chart 3 that, node reached a peak vertical displacement of 54 mm. In case 2, with the 2<sup>nd</sup> column removal from ground level, the vertical deflection started to increase again and reached a peak vertical displacement of 56 mm.

In case 3, the column at 15<sup>th</sup> floor was first removed. It is shown in Chart 3 that, node reached a peak vertical displacement of 51 mm. In case 4, with the 2<sup>nd</sup> column removal from 15<sup>th</sup> level, the vertical deflection started to increase again and reached a peak vertical displacement of 52 mm.

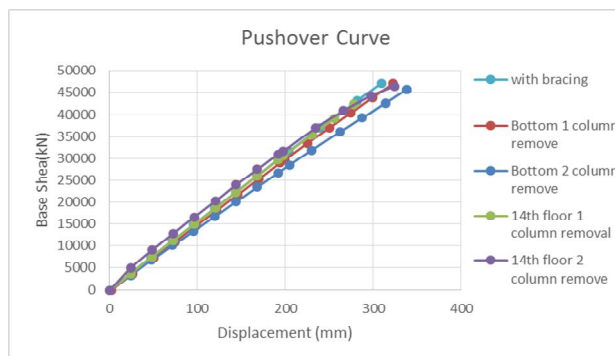


Chart -4: Pushover Curve

Chart 4 shows Pushover curve of every situation. Here Base shear force at performance point is 4986 kN shown in Chart 1 which is checked with value of base shear force (7446 kN) of step no. 3 of Table 2 of pushover analysis. Hence it is required to see hinge formation at step no. 3.

Table -2: Base shear vs. Monitored Displacement

| Step | Monitored Displ | Base Force | A-B  | B-C | C-D | D-E | >E | A-IO | IO-LS | LS-CP | >CP | Total |
|------|-----------------|------------|------|-----|-----|-----|----|------|-------|-------|-----|-------|
|      | m               | kN         |      |     |     |     |    |      |       |       |     |       |
| 0    | 0               | 0          | 7680 | 0   | 0   | 0   | 0  | 7680 | 0     | 0     | 0   | 7680  |
| 1    | -0.024          | 3722.92    | 7680 | 0   | 0   | 0   | 0  | 7680 | 0     | 0     | 0   | 7680  |
| 2    | -0.048          | 7445.84    | 7680 | 0   | 0   | 0   | 0  | 7680 | 0     | 0     | 0   | 7680  |
| 3    | -0.072          | 11168.76   | 7680 | 0   | 0   | 0   | 0  | 7680 | 0     | 0     | 0   | 7680  |
| 4    | -0.096          | 14891.68   | 7680 | 0   | 0   | 0   | 0  | 7680 | 0     | 0     | 0   | 7680  |
| 5    | -0.12           | 18614.6    | 7680 | 0   | 0   | 0   | 0  | 7680 | 0     | 0     | 0   | 7680  |
| 6    | -0.144          | 22337.52   | 7680 | 0   | 0   | 0   | 0  | 7680 | 0     | 0     | 0   | 7680  |
| 7    | -0.168          | 26060.45   | 7680 | 0   | 0   | 0   | 0  | 7680 | 0     | 0     | 0   | 7680  |
| 8    | -0.192          | 29783.38   | 7680 | 0   | 0   | 0   | 0  | 7680 | 0     | 0     | 0   | 7680  |
| 9    | -0.203857       | 31622.64   | 7674 | 6   | 0   | 0   | 0  | 7680 | 0     | 0     | 0   | 7680  |
| 10   | -0.239504       | 36968.75   | 7652 | 28  | 0   | 0   | 0  | 7680 | 0     | 0     | 0   | 7680  |
| 11   | -0.281407       | 43065.85   | 7640 | 40  | 0   | 0   | 0  | 7680 | 0     | 0     | 0   | 7680  |
| 12   | -0.309106       | 47012.23   | 7622 | 58  | 0   | 0   | 0  | 7680 | 0     | 0     | 0   | 7680  |

#### IV. CONCLUSIONS

It may be concluded that optimally braced frames are stiff, strong, and an economical structural system. At the same time optimally braced one have least forces induced in the structure and produce maximum displacement but within prescribed limit.

Base shear force at performance point is 4986 kN which is checked with value of base shear force (7446 kN) of step no. 3 of pushover analysis. Hence it is required to see hinge formation at step no. 3. From fig. and pushover curve table it is clear that hinges formed in beams and columns are below immediate occupancy level. For a structure to be safe to use it requires no hinge formed above immediate occupancy level in governing step.

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