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Effects of Process Parameters on the Microstructural Properties of MIG and FSW Joints

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Abstract: The present research work is undergone to investigate the effect of weld parameters on the microstructural behavior of metal inert gas welding (MIG) and friction stir welding (FSW) joints. The selection of process parameters is important in the welding process to produce the best quality of welded joints. The process parameters of nozzle to plate distance, torch angle and Arc voltage for metal inert gas welding and rotational speed, tool tilt angle and Feed rate for friction stir welding processes are considered. The microstructural study is carried out on the welded joints using scanning electron microscope and the microstructure of friction stir welding process gives the better and defect free welded joints compared to microstructures of Metal inert gas welding process.

Keywords: Aluminium alloy; Titanium alloy; Process parameters; Microstructure; Metal inert gas welding; Friction stir welding.

I. INTRODUCTION

Aluminium alloys and titanium alloys are widely used in various industrial applications such as aerospace, automotive, marine industries because of its properties of low weight, corrosion resistance and suitable for all fusion welding processes. Nowadays the dissimilar welding is important to make material joining. The fusion welding is mainly considered for dissimilar materials joining effectively due to the variations of melting temperature of the materials. Metal Inert Gas (MIG) welding is done by using Argon or Helium as a shielding gas and consumable electrode as a conductor and also it is versatile, gives very little loss of alloying elements. The high power density of plasma arc welding is becoming prominent to exhibit quick fusion between metals. Even though this fusion welding of dissimilar weldments is weak in the transition region and it has fumes, crack and spatter and this will be overcome by the solid state welding process. Friction stir welding is the new and innovative method to make similar welded joints. The investigations are made on the tensile and impact strength of GTAW and FSW joints of interstitial free steel and the higher tensile and impact strength of FSW joints are unveiled and enrichment in strength and toughness are 24 % and 39% respectively by comparing the GTAW process [1].

This investigation is made in pulse MIG welding by changing the waveform periodically repeated by DCEP and DCEN to control the wire melting speed and heat input and the better bead appearance of welding is attained at high speed and when the increment of the En-ratio in welding is applied, then the wire melting speed and the heat input increases and decreases respectively [2]. It is perceived that the effects of welding parameters on the strength and hardness of the joint increase with the decrease in heat input and the toughness increases while the hardness and tensile strength of the joint decreases [3]. The Friction stir butt welded joints of AA 8011 aluminium alloys are successfully made using rotatable central composite design [4]. The good quality of welded joint exposed on the strength and hardness and also the highest relative efficiency of friction stir welding responses gives the optimum conditions of process parameters. In dynamically controlled PAW process, the keyhole is intentionally endorsed for a suitable period on the weldments to shrink the heat input and the reduction of formation of prior-beta (β) grain size and eliminating the creation of martensite phases in FZ and also the micro hardness in the welded zone develops the ductility of the welded joint in titanium alloys [5]. The defect-free joints of super duplex stainless steel are made by PAW with no filler metal and established that the impact test outcomes has good in weld metal zone and heat affected zones [6]. Due to increase in heat input, the hardness at the heat affected zone is increased. The improved weldability of super duplex stainless steel with the suitable welding conditions of heat input and ferrite/austenite stability lead to produce higher productivity during welding in industries.



The study is made on tensile properties and fracture location of the FSW joints and the presence of micro-voids are important in the NZ with the heat input of RP greater than around 0.333 mm/rev. The fracture is happening in the HAZ for low RP which gives the weakest region in the welded joint while the RP increases or the heat input decreases, the fracture appears in the weld centre [7]. The investigation showed that the optimum FSW process parameters of tool rotational speed of 1400 RPM, welding speed of 60 mm/min, axial force of 8 kN yielded higher tensile strength properties compared to other joints and also found the defect free fine grained microstructure occur at the weld nugget zone [8].

]	Mechanic	cal Properties					Chen	nical C	omposi	tion (V	Vt.%)			
Base Metal	Tensil e Strengt h (Mpa)	Densit y (kg/m ³)	Thermal Conductivi ty (W/m ^o K)	Meltin g Point (°C)	Si	Fe	Mn	Mg	Ti	Al	С	Н	V	Zn	Cr
AA80 11	110	2689	237	660. 3	0.1 4	-	-	-	Re m	2.8	0.0 4	0.01 6	2. 6	-	-
Ti alloy (Grd 9)	690	4480	8.3	1668	0.5 1	0.7 3	0.4 5	0.2 7	0.0 3	Re m	-	-	-	0.0 9	0.0 4

Process Parameters	FSW	MIG
Welding Current/ Amp		120
Arc Voltage/ Volt		20 - 30
Travel Speed/ mm/s		3
Polarity		AC
Shielding Gas		99 % Argon
Gas flow rate/ lpm		6 - 10
Nozzle to plate distance/ mm		1 - 6
Torch angle/ deg		80 - 100
Rotational speed/ rpm	800-1600	
Welding speed/ mm/min	20-75	
Axial feed/ mm	3	
Tilt angle/ deg	80 - 100	
FSW Tool Details	Cam profiled pin	
Pin length/ mm	5.7	
Pin diameter/ mm	6	
Shoulder diameter/ mm	18	



The increase in rotating speed leads to increase the strain rate and for a constant traverse speed, lower rotating speed leads to lower strain rates [9]. When the rotating speed is kept constant, defect-free welds are obtained while at constant traverse speed, the groove-like defect is occurring. The welding speed of FSW affects the tensile strength of the joint and found that by increasing the travel speed, the increase in tensile strength of the Ti and Al alloy joints and at the mixed regions of the Ti alloy and Al alloy, the intermetallic compound are formed which affects the tensile strength joints [10]. In this investigation, comparative study of effects of process parameters on microstructural behavior between MIG and FSW joints are considered.



Fig. 1 Schematic diagram of Friction stir welding Process

II. MATERIALS AND METHODS

A.Selection of Work Piece Materials

The AA 8011 aluminium alloy and Titanium alloy (grade 9) plates with a thickness of 6 mm are used for metal inert gas welding and similar aluminium alloy plates are considered for the friction stir welding shown in Fig. 1. The mechanical properties and chemical compositions of both materials are listed in Table 1. The surfaces of both plates are properly dressed with a steel brush and acetone before welding process. All welds are made in butt joint configuration.

B. Selection of Welding process and process parameters

In MIG, the workplace setup with workplace properly covered and shielded with helium gases, which is used to protect the oxidation in titanium alloy plates. The process parameters of the MIG and FSW are listed in Table 2. In MIG, the EN4043 aluminium filler material is used to join the two different materials, while in FSW the Cam profiled HC-HCr steel which is used to produce proper joints using a Universal milling machine. The microstructural analysis are applied on the samples using standard metallographic procedures with the standard dimensions of 16 mm x 6 mm x 6 mm, with fine polishing using diamond paste of 0.5 μ m particle sizes and the samples are etched using Keller's solution which reveal the good microstructure of the weldments. The microstructural analysis is performed using Scanning electron microscope at weld centre.

III.RESULTS AND DISCUSSIONS

A.Microstructural analysis of dissimilar mig welded joints at the weld centre

The observations are made on Fig. 2 by analyzing the microstructure of MIG welding based on the process parameters Nozzle to plate distance (NPD), Torch angle (TA) and Arc Voltage (AV) at the weld centre. The defect free welds are determined from the microstructural observation on MIG welded joints. From the Fig. 2a, the blow holes are formed at the weld interface for the process settings of nozzle to plate distance 2 mm and torch angle 5° which is in aluminium side with arc voltage of 20V whereas the cavities are formed by increasing the arc voltage due to the excess heat input in Fig 2b. The defect free welds are identified by observing the microstructure of the welded joints with the process settings of 3.5 mm nozzle to plate distance, arc voltage of 25 V with maximum



torch angle from the weld centre is presented in Figs. 2 c-d. The grains formation in the welded region of the dissimilar MIG welding mainly depends upon the proper process settings with proper selection of electrode material. The MIG welding process parameters in the range of 3 to 4 mm nozzle to plate distance, 7 to 8° deviation from the weld centre with the 25V arc voltage are observed to produce the defect free welds by examining the microstructures of the welded joints.

MIG Welding	Microstructure	Observations	Reasons
*NPD = 2 mm *TA = 95° *AV = 20 V	Al Blow holes formation Ti	Blow holes formation occurred at the aluminium welded region whereas the thin curved needle structure is formed in Titanium side	The improper heat generation occurred due to the torch angle deviates from the weld centre to the aluminium side
$NPD = 2 mm$ $TA = 95^{\circ}$ $AV = 30 V$	Cavities Ti Al	Cavities are formed in aluminium alloy side which is near by the weld interface	Due to high arc voltage with torch angle, the improper solidification occurred in the welded region
NPD = 3.5 mm TA = 82° AV = 25 V	C Al Fe particles Silicon particles	Defect free Welds are found	Due to proper process settings of MIG welding
$NPD = 3.5 \text{ mm}$ $TA = 98^{\circ}$ $AV = 25 \text{ V}$	AI Grain Boundaries Silicon particles Ti Mag= 500 X	Defect free Welds are found and coarse grain boundaries are formed in the aluminium alloy region	Due to proper process settings of MIG welding

* NPD – Nozzle to Plate Distance in mm, *TA – Torch angle in degree, *AV – Arc Voltage in Voltage Fig. 2 SEM images on microstructure of MIG welded joints at weld centre

A.Microstructural analysis of FSW joints at the Stir zone

By analysing the microstructure of FSW at the weld centre (Stir/Nugget Zone) from the Fig. 3, the following observations are made. The defects of a large mass of flash due to the excess heat input and improper process setting are occurred with different proportions of process parameters and it can be overcome by changing the suitable parameters of the rotational speed (RS), tilt angle (TA) and Feed rate (FR). In Fig. 3a, the defect of large masses of flash is found by considering the lower rotational speed and feed rate with tilt angle deviates from the weld centre. The defect free welds are examined in the microstructure of the welded joint is presented in Fig. 3b with the higher rotational speed, lower feed rate with the vertical position of the Cam profiled tool pin and it has higher strength compared other joints. The excess tilt angle of the tool makes the variation of the frictional heat and material flow, whereas



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the higher rotational speed produces the cavities or groove like structure due to insufficient stirring and mixing of the base materials in Fig. 3d. From the Figs. 3 c and 3e, the higher rotational speed with lower feed rate with the vertical position of the friction stir welding tool produces the defect free welds with sufficient strength of the welded joints.

By comparing all the microstructures in Stir/Nugget Zone, it is seen the defects like large masses of flash, cavities or groove like defects and cavity caused by abnormal stirring can overcome by adjusting the tilt angle, rotational speed and welding speed. The parameters with 1250-2150 RPM rotational speed, tilt angle of 85-90 degrees and Feed rate of 24-30 mm/min are giving better results compared to other process parameters in the Stir/Nugget Zone.

FSW Welding Parameters	Microstructure	Observations	Reasons
*RS = 1250 rpm *TA = 95° *FR = 50 mm/min	Bilicon Particles Grain Boundaries Large mass of flash CEG 15.0kV 11.8mm x2.50k SE	Large mass of flash occurred	The improper frictional heat generated due to the tilt angle of the tool
RS = 2900 rpm TA = 85° FR = 30 mm/min	Silicon Particles Grain Boundaries CEQ 15 OKV 10.0mm x2.50% SE20.0um	Defect free welds are found	Proper heat generation and material flow
RS = 3500 rpm TA = 82° FR = 40 mm/min	Silicon Particles Fe Particles CEG 15 0kV 11.4mm x2.50k SE	Cavities with flash are occurred at the welded region	Due to higher rotational speed with lower feed rate, very high heat plastic deformation is occurred and the materials are sticking with the tool
*RS = 2150 rpm *TA = 90° *FR = 24 mm/min	CEG 15.0kV 12.0mm x2.50k SE	Defect free Welds are found	Proper heat generation and material flow



RS – Rotational Speed in rpm, *TA – Tool Tilt angle in degree, *FR – Feed rate in mm/min Fig. 3 SEM images on microstructure of FSW welded joints at weld centre

IV. CONCLUSION

During this investigation, an attempt is made to select a proper welding process from the effects of weld parameters on the microstructural behavior of MIG and FSW with cam profiled pin tool. From this investigation, the following conclusions are derived:

- A. The mean values of the welding process parameters are used to produce the best quality of weld with sufficient strength in microstructural analysis of MIG welding and very few process parameters setting gives the expected results and others having the defects.
- B. The microstructural analysis are made in FSW at stir zone and the welding process parameters of rotational speed 1250 2150 RPM, tilt angle 85-90° and Feed rate 24 30 mm/min are preferred for getting quality of weld with adequate strength in microstructural analysis and very few FSW process parameters setting gives the defects compared to other combinations of joints.
- *C.* By comparing all the welding processes, the friction stir welding gives better results than the MIG welding process in the microstructural analysis.

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