

Optimization of CO₂ Laser Beam Cutting Process Parameters for Machining Of AISI 9255 Spring Steel

Renangi Sandeep¹, S Bala Anki Reddy², S Jaya Kishore³

^{1,2}Assistant Professor, Department of Mechanical Engineering, Siddhartha Institute of Science and Technology, Puttur, A.P., India – 517583

³Assistant Professor, Department of Mechanical Engineering, SVCE, Tirupathi, A.P., India – 517501

Abstract: The present work deals with the process parameters optimization of continuous wave CO₂ laser cutting of AISI 9255 spring steel. In the present study four process variables such as laser power, cutting speed, laser pressure and focal distance are considered and experimentation are carried out based on L₂₇ orthogonal array (OA). The cut quality responses such as surface roughness and kerf taper are measured for every experimental run. To optimize process parameters TOPSIS method is employed. The aim of optimization is to minimize surface roughness and kerf taper characteristics.

Keywords: CO₂ Laser beam cutting, spring steel, Kerf taper, TOPSIS, L₂₇ OA

I. INTRODUCTION

The laser was developed in 1960s due to its precision and high intensity has been widely used in the field of fine cutting of sheet metals. Lasers remain well known and a very flexible mechanism for producing various micro-structures in this modern era, particularly in upgrading of engineering materials. Laser Beam Machining (LBM) is one of the innovative non-conventional machining process that actuality contemporarily used for shaping virtually entire range of engineering materials wherever complex shapes in request precise, fast and force-free processing. In addition, marking, drilling, and welding applications, cutting is the most irregularly useful LBM process.

Laser beam cutting is a non-contact type; thermal energy based unconventional machining process in which an excessive intensity laser beam is concentrated at a spot and material gets melted or evaporated at that spot. The molten metal was removed from the melting pool by supplying the high pressure co-axial assisted gas as show in Fig. 1. The efficiency of the laser cutting process be influenced by mechanical properties of the material to be cut and then also based on the thermal and some extent optical properties.

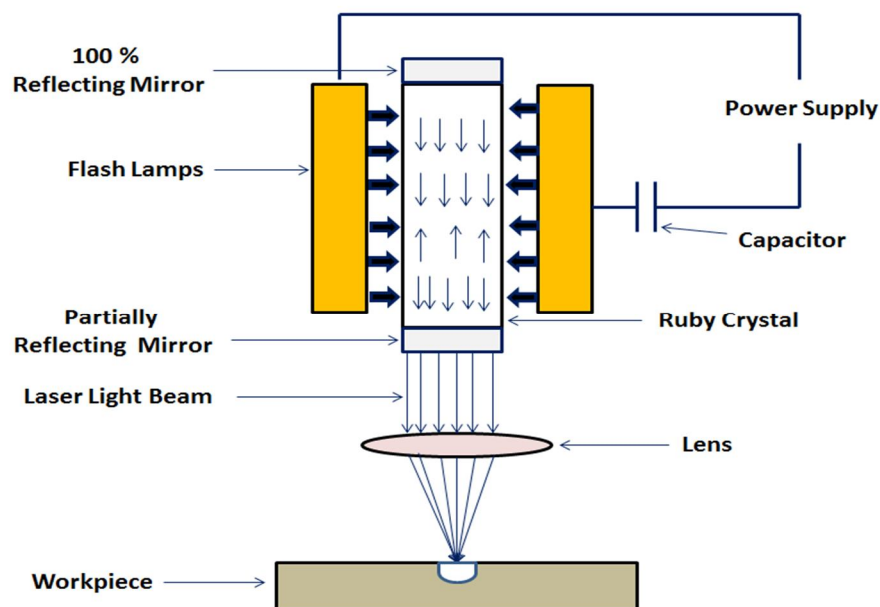


Fig. 1 Principle of Laser Beam Cutting Process

There are many researchers have been studied laser beam cutting process. Some of literatures are B S Yilbas [1] has studied the Striation formation due to the slow drifts and disturbances in various parameters during the laser cutting process. The effects of laser power, cutting speed and energy coupling factor on the kerf size are investigated. His work has shown that increasing laser power and energy coupling factor increase the kerf width size. Also, small changes in laser power, cutting speed and energy coupling factor modify the kerf width to a great extent. Dayana Espinal and Aravinda Kar [2] have developed A simple mathematical model to relate kerf depth to laser power, laser scanning speed and kerf width during laser cutting. Asano et al. [3] have shown that the range of processing conditions which allow cutting is determined by the energy input per unit area. The values of roughness of the cutting surface on both entry and exit sides of the plates can be reduced if the cutting speed is 1000 mm/min or higher. They change little at small values if the heat input per unit area is within a range under 20 J/mm². Cutting with small heat input always results in better finish of cut surface. Uslan.I [4] has investigated the influence of laser power and cutting speed variations on the kerf width size. A lump parameter analysis is introduced when predicting the kerf width size and an experiment is conducted to measure the kerf size and its variation during the cutting process. He has found that the workpiece surface influences significantly the kerf width size. He has also shown that the variation in the power intensity results in considerable variation in the kerf size during the cutting, which is more pronounced at lower intensities. Zhang et al [5] have proposed a synthetic evaluation method for laser cutting quality. B S Yilbas et al [6] using a CO₂ laser with variable pulse frequency and Oxygen, as assisting gas, at different pressures have investigated the cutting process. SEM and X ray diffraction are carried out to obtain micrographs and oxide compounds formed in the dross. They have found that the liquid layer thickness increases with increasing laser output power and reduces with increasing assisting gas velocity. The mechanics of dross formation has been studied by using the relation between kinetic energy of the melt film and the local temperature. Striation produced during the laser cutting affects the surface roughness, appearances and geometry of laser cut products. Lin Li, M. Sobih and P.L. Crouse [7] have given a theoretical model to predict the critical cutting speed at which striation-free cutting takes place. It is also observed that at cutting speeds above the critical cutting speed, striation reappears and surface roughness increases with the cutting speed.

In this present paper, two output responses are taken such as kerf taper and surface roughness have been optimized simultaneously during continues wave CO₂ laser beam cutting of AISI 9255 spring steel using approach of Topsis method. The control factors taken as laser power, gas pressure, focal distance and cutting speed. The plate material of AISI 9255 spring steel having thickness of 8 mm is taken into consideration. Firstly, Experiments have been performed on AISI 9255 spring steel work piece based upon Taguchi experimental design L₂₇ orthogonal array. The results obtained from Taguchi-based experiment have been used in Topsis for finding optimal solutions.

II. EXPERIMENTATION

The experiments are conducted on High power CO₂ Laser Machining centre model no Trumatic L6050, made by GSI group laser division, United Kingdom which is available with M/s. Meera Laser Solutions (I) PVT. LTD. Chennai, Tamilnadu. The maximum average power produced at laser is 3200W. In this research profile cutting of AISI 9255 spring steel is carried out at by varying the input parameters. The chemical composition of the material is given in Table I.

Table I: Chemical Composition Of Aisi 9255 Spring Steel

%	C	Cr	Si	Mn	P	V	S	Fe
Min	0.45	0.80	0	0.50	0	0	0	Balance
max	0.55	1.20	0.50	0.80	0.06	0.15	0.06	

A. Experimental setup

The CO₂ Laser Beam cutting equipment used for the present work is shown in Fig. 2 & Fig. 3. Fig. 2 shows the 3-axes CNC assisted Laser cutting unit, control unit and the fixture to locate the work piece. Fig. 2 shows the LBC machine showing Laser head in ready-to-start position. Fig. 3 shows the running position of the machine and the laser beam coming from the laser head can also be seen. The conditions at which the experiments were carried out are detailed in Table II. Based on the literature survey and the trial experiments, it was found that the process parameters such as Laser power, cutting speed, gas pressure, and focal distance have

significant effect on cut edge quality such as surface roughness and taper kerf. In the present work, surface roughness and taper kerf are considered as the decision variables and trial samples of square profile cutting with the dimensions of 10 x 10 mm are performed by varying one of the process variables to determine the working range of each process variable.



Fig 2: The CO2 laser-machining center (Trumatic L6050)

Fig. 3: CO₂ Laser Machining process

Table II: Experimental Conditions

Factors	Units	Levels		
		I	II	III
Power	KW	1.6	1.8	2.0
Cutting Speed	mm/sec	4000	4250	4500
Gas Pressure	Bar	2.0	2.5	3.0
Focal Distance	mm	1	1.1	1.2

B. Design of Experiments

Design of experiments (DOE) is used to find out the effect of different process response parameters on different control factors and for getting the relation between them. For giving the minimum no of experimental runs, we will get the required amount of information it will save the machine time and cost of the experiment. In taguchi method the experiments are performed as per the standard orthogonal arrays (OA). The selection of orthogonal array depends on the total degree of freedom (DOF). In the present investigation to check the DOFs in the experimental design for the three-level test, the four main factors take 8 ($4 \times (3-1)$) DOFs. For three second order interactions ($A \times B$, $A \times C$, $B \times C$) is 16 ($4 \times (3-1) \times (3-1)$) and the total DOFs required is 24 (8+16). Here the L₂₇ OA (DOF: 26) has been selected. The design of experiments is given in Table III to run the experiments.

III. EXPERIMENTAL RESULTS AND DISCUSSIONS

The experimental results for process responses such as kerf taper angle and surface roughness are presented in Table III.

Table iii. Experimetal run along with the output response values

S. No	Power (KW)	Cutting speed (mm/sec)	Gas Pressure (Bars)	Focal Distance (mm)	Kerf taper (degree)	Surface roughness (µm)
1	1.6	4000	2.0	1.0	0.303	5.851
2	1.6	4000	2.5	1.1	0.758	5.710
3	1.6	4000	3.0	1.2	0.761	4.398
4	1.6	4250	2.0	1.1	0.311	5.951
5	1.6	4250	2.5	1.2	0.521	3.317
6	1.6	4250	3.0	1.0	0.697	5.024
7	1.6	4500	2.0	1.2	0.306	5.340
8	1.6	4500	2.5	1.0	0.711	5.602
9	1.6	4500	3.0	1.1	0.820	6.083
10	1.8	4000	2.0	1.1	0.511	2.970
11	1.8	4000	2.5	1.2	0.660	2.756
12	1.8	4000	3.0	1.0	0.702	2.920
13	1.8	4250	2.0	1.2	0.6365	4.457
14	1.8	4250	2.5	1.0	0.465	2.582
15	1.8	4250	3.0	1.1	0.881	2.849
16	1.8	4500	2.0	1.0	0.725	4.156
17	1.8	4500	2.5	1.1	0.577	2.368
18	1.8	4500	3.0	1.2	0.625	2.125
19	2.0	4000	2.0	1.2	0.780	2.055
20	2.0	4000	2.5	1.0	0.819	2.455
21	2.0	4000	3.0	1.1	0.502	2.551
22	2.0	4250	2.0	1.0	0.711	1.309
23	2.0	4250	2.5	1.1	0.582	1.034
24	2.0	4250	3.0	1.2	0.565	1.584
25	2.0	4500	2.0	1.1	0.779	1.570
26	2.0	4500	2.5	1.2	0.661	3.709
27	2.0	4500	3.0	1.0	0.571	1.439

A. *Topsis method*

TOPSIS stands for technique for order preference by similarity to ideal solution. This method was developed by Hwang and Yoon in the year 1995. Technique for order preference by similarity to ideal solution (TOPSIS) is based on the idea that the chosen alternative should have the shortest distance from the positive ideal solution and on the other side the farthest distance of the negative ideal solution. The ideal solution is a hypothetical solution for which all attribute values correspond to the minimum attribute values in the data base. TOPSIS thus gives a solution that is not only closest to the hypothetically best but also farthest from the hypothetically worst. The steps followed for the TOPSIS in the present research work are given below.

1) Step 1: Decision matrix is normalized by using the following equation:

$$r_{ij} = \frac{a_{ij}}{\sqrt{\sum_{i=1}^m a_{ij}^2}} \text{ ----- Equ. (1)}$$

where $i = 1 \dots m$ and $j = 1 \dots n$. a_{ij} represents the actual value of the i^{th} value of j^{th} experimental run and r_{ij} represents the corresponding normalized value. The normalized values of kerf taper and surface roughness are presented in Table IV.

2) Step 2: Weight for each response is calculated. Here, equal weightage is given to all the responses. Therefore, $w_j = 0.50$. The weights for all the responses are given in Table V.

$$V_{ij} = W_i \times r_{ij} \text{ ----- Equ. (2)}$$

where $i = 1 \dots m$ and $j = 1 \dots n$. w_j represents the weight of the j^{th} attribute or criteria.

3) Step 3: In this step, the worst alternative (t_{wj}) and the best alternative (t_{bj}) are determined from the weighted normalized values (t_{ij}). These values are used to determine the separation measures. Table VI shows the Best and worst values of output parameters.

Table IV: Normalized Values Of Surface Roughness And Kerf Taper

S. No	Power (KW)	Cutting speed (mm/sec)	Gas Pressure (Bars)	Focal Distance (mm)	Normalized Values	
					Kerf taper	Surface roughness
1	1.6	4000	2.0	1.0	0.090	1.743
2	1.6	4000	2.5	1.1	0.226	1.701
3	1.6	4000	3.0	1.2	0.227	1.310
4	1.6	4250	2.0	1.1	0.093	1.773
5	1.6	4250	2.5	1.2	0.155	0.988
6	1.6	4250	3.0	1.0	0.208	1.497
7	1.6	4500	2.0	1.2	0.091	1.591
8	1.6	4500	2.5	1.0	0.212	1.669
9	1.6	4500	3.0	1.1	0.244	1.812
10	1.8	4000	2.0	1.1	0.152	0.885
11	1.8	4000	2.5	1.2	0.197	0.821
12	1.8	4000	3.0	1.0	0.209	0.870
13	1.8	4250	2.0	1.2	0.190	1.328
14	1.8	4250	2.5	1.0	0.139	0.769
15	1.8	4250	3.0	1.1	0.262	0.849
16	1.8	4500	2.0	1.0	0.216	1.238
17	1.8	4500	2.5	1.1	0.172	0.705
18	1.8	4500	3.0	1.2	0.186	0.633
19	2.0	4000	2.0	1.2	0.232	0.612
20	2.0	4000	2.5	1.0	0.244	0.731
21	2.0	4000	3.0	1.1	0.150	0.760
22	2.0	4250	2.0	1.0	0.212	0.390
23	2.0	4250	2.5	1.1	0.173	0.308
24	2.0	4250	3.0	1.2	0.168	0.472
25	2.0	4500	2.0	1.1	0.232	0.468
26	2.0	4500	2.5	1.2	0.197	1.105
27	2.0	4500	3.0	1.0	0.170	0.429

Table V: Weightage Values Of Surface Roughness And Kerf Taper

S. No	Power (KW)	Cutting speed (mm/sec)	Gas Pressure (Bars)	Focal Distance (mm)	Weighted Decision matrix	
					Kerf taper	Surface roughness
1	1.6	4000	2.0	1.0	0.0450	0.8715
2	1.6	4000	2.5	1.1	0.1130	0.8505
3	1.6	4000	3.0	1.2	0.1135	0.6550
4	1.6	4250	2.0	1.1	0.0465	0.8865
5	1.6	4250	2.5	1.2	0.0775	0.4940
6	1.6	4250	3.0	1.0	0.1040	0.7485
7	1.6	4500	2.0	1.2	0.0455	0.7955
8	1.6	4500	2.5	1.0	0.1060	0.8345
9	1.6	4500	3.0	1.1	0.1220	0.9060
10	1.8	4000	2.0	1.1	0.0760	0.4425
11	1.8	4000	2.5	1.2	0.0985	0.4105
12	1.8	4000	3.0	1.0	0.1045	0.4350
13	1.8	4250	2.0	1.2	0.0950	0.6640
14	1.8	4250	2.5	1.0	0.0695	0.3845
15	1.8	4250	3.0	1.1	0.1310	0.4245
16	1.8	4500	2.0	1.0	0.1080	0.6190
17	1.8	4500	2.5	1.1	0.0860	0.3525
18	1.8	4500	3.0	1.2	0.0930	0.3165
19	2.0	4000	2.0	1.2	0.1160	0.3060
20	2.0	4000	2.5	1.0	0.1220	0.3655
21	2.0	4000	3.0	1.1	0.0750	0.3800
22	2.0	4250	2.0	1.0	0.1060	0.1950
23	2.0	4250	2.5	1.1	0.0865	0.1540
24	2.0	4250	3.0	1.2	0.0840	0.2360
25	2.0	4500	2.0	1.1	0.1160	0.2340
26	2.0	4500	2.5	1.2	0.0985	0.5525
27	2.0	4500	3.0	1.0	0.0850	0.2145

Table VI Best And Worst Values Of Output Parameters

Output parameter	V _{bj}	V _{wj}
Kerf Taper	0.045	0.131
Surface roughness	0.154	0.906

4) Step 4: The separation of each alternative from positive ideal solution (PIS) and negative ideal solution (NIS) is calculated as

$$S_i^+ = \sqrt{\sum_{j=1}^n (V_{ij} - V_{bj})^2} \quad \text{----- Equ. (3)}$$

$$S_i^- = \sqrt{\sum_{j=1}^n (V_{ij} - V_{wj})^2} \quad \text{----- Equ. (4)}$$

where i = 1,2, 3, ... m, the separation measures for all experimental runs are given in Table VII.

TABLE VII SEPERATION MEASURE VALUES

S. No	Power (KW)	Cutting speed (mm/sec)	Gas Pressure (Bars)	Focal Distance (mm)	Separation measures	
					S_i^+	S_i^-
1	1.6	4000	2.0	1.0	0.718	0.093
2	1.6	4000	2.5	1.1	0.700	0.058
3	1.6	4000	3.0	1.2	0.506	0.252
4	1.6	4250	2.0	1.1	0.733	0.087
5	1.6	4250	2.5	1.2	0.342	0.415
6	1.6	4250	3.0	1.0	0.597	0.160
7	1.6	4500	2.0	1.2	0.642	0.140
8	1.6	4500	2.5	1.0	0.683	0.076
9	1.6	4500	3.0	1.1	0.756	0.009
10	1.8	4000	2.0	1.1	0.290	0.467
11	1.8	4000	2.5	1.2	0.262	0.497
12	1.8	4000	3.0	1.0	0.287	0.472
13	1.8	4250	2.0	1.2	0.512	0.245
14	1.8	4250	2.5	1.0	0.232	0.525
15	1.8	4250	3.0	1.1	0.284	0.482
16	1.8	4500	2.0	1.0	0.469	0.288
17	1.8	4500	2.5	1.1	0.203	0.555
18	1.8	4500	3.0	1.2	0.169	0.591
19	2.0	4000	2.0	1.2	0.168	0.600
20	2.0	4000	2.5	1.0	0.225	0.541
21	2.0	4000	3.0	1.1	0.228	0.529
22	2.0	4250	2.0	1.0	0.073	0.711
23	2.0	4250	2.5	1.1	0.042	0.753
24	2.0	4250	3.0	1.2	0.091	0.672
25	2.0	4500	2.0	1.1	0.107	0.672
26	2.0	4500	2.5	1.2	0.402	0.355
27	2.0	4500	3.0	1.0	0.073	0.693

5) Step 5. The closeness coefficient of each alternative (CC_i) is calculated as

$$CC_i = \frac{S_i^-}{S_i^+ + S_i^-} \text{ ----- Equ. (5)}$$

The closeness value to ideal solution values and corresponding values are given in Table VIII.

Table Viii Relational Closness Values And Their Ranks

S. No	Power (KW)	Cutting speed (mm/sec)	Gas Pressure (Bars)	Focal Distance (mm)	Relative Closeness Value	Ranks
1	1.6	4000	2.0	1.0	0.40508	27
2	1.6	4000	2.5	1.1	0.37908	11
3	1.6	4000	3.0	1.2	0.37864	9
4	1.6	4250	2.0	1.1	0.40961	26
5	1.6	4250	2.5	1.2	0.37850	4
6	1.6	4250	3.0	1.0	0.37861	8
7	1.6	4500	2.0	1.2	0.39061	23
8	1.6	4500	2.5	1.0	0.37949	14
9	1.6	4500	3.0	1.1	0.38247	17
10	1.8	4000	2.0	1.1	0.37845	1
11	1.8	4000	2.5	1.2	0.37929	12
12	1.8	4000	3.0	1.0	0.37948	13
13	1.8	4250	2.0	1.2	0.37855	6
14	1.8	4250	2.5	1.0	0.37846	2
15	1.8	4250	3.0	1.1	0.38267	18
16	1.8	4500	2.0	1.0	0.37858	7
17	1.8	4500	2.5	1.1	0.37901	10
18	1.8	4500	3.0	1.2	0.38008	15
19	2.0	4000	2.0	1.2	0.38398	21
20	2.0	4000	2.5	1.0	0.38283	20
21	2.0	4000	3.0	1.1	0.37848	3
22	2.0	4250	2.0	1.0	0.39247	24
23	2.0	4250	2.5	1.1	0.39741	25
24	2.0	4250	3.0	1.2	0.38122	16
25	2.0	4500	2.0	1.1	0.38957	22
26	2.0	4500	2.5	1.2	0.37853	5
27	2.0	4500	3.0	1.0	0.38278	19

IV. CONCLUSIONS

The scope of present paper was the optimization of process parameters in laser beam machining of AISI 9255 spring steel using TOPSIS Method. The process parameters examined in this investigation are cutting speed, laser power, gas pressure and focal distance. The following conclusions are made.

- A. The optimized process parameter setting is laser power 1.8 KW, cutting speed of 4000 mm/sec, gas pressure of 2.0 bars and 1.1 mm focal distance.
- B. The results obtained in the analysis are validated and the results based on turning process responses can be effectively improved.



- C. The proposed experimental and statistical approach is simple, useful, and a reliable methodology to optimize laser welding parameters efficiently. In future, this method can be used to optimize and improve other process parameters. Also, this method can be extended to study other machining processes.

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